

EPA REGION V ARCS PROGRAM

EPA Contract No. 68-W8-0093

Work Assignment No. 17-5L4J

SEC Donohue Project No. 20026

EPA Region 5 Records Ctr.



200062

13

VOLUME 2

**DRAFT REMEDIAL INVESTIGATION REPORT
APPENDIX A - BACKGROUND INFORMATION, AND
APPENDIX B - TECHNICAL MEMORANDA (PHASE I)**

**HIMCO DUMP
REMEDIAL INVESTIGATION/FEASIBILITY STUDY
ELKHART, INDIANA**

August
MAY 1992

Prepared for:

U.S. Environmental Protection Agency
Emergency and Remedial Response Branch
Region V
77 West Jackson Boulevard
Chicago, Illinois 60604

APPENDIX A
BACKGROUND INFORMATION

Fit Results
USGS Well Logs



ecology and environment, inc.

111 WEST JACKSON BLVD., CHICAGO, ILLINOIS 60604, TEL. 312-663-9415

International Specialists in the Environment

NARRATIVE SUMMARY

HIMCO DUMP

ELKHART, INDIANA

The Himco Dump site covers approximately 40 acres of former marsh land. The site is located at County Road 10 and the Napanee Extension in the Town of Elkhart, located in Elkhart County, Indiana. The site operated between 1960 and 1976 under the ownership of Mr. Charles Himes. A marshy area was excavated and general refuse, medical and pharmaceutical wastes were landfilled in the resulting hole. There is also a possibility that industrial waste was buried in the excavation.

The total amount of hazardous waste landfilled at the site is unknown. According to laboratory analysis of samples taken by Ecology and Environment FIT members during the site inspection of July 30, 1984, groundwater is contaminated with cobalt, selenium, beryllium, cadmium, copper, manganese, and other inorganic metals. The Rocky Mountain Analytical Laboratory performed the above analysis which corroborated earlier residential well sample analysis which showed high manganese levels. The site is located above a continuous portion of the local outwash aquifer system that is the sole source of drinking water for the community. A conservative estimate of 20,000 people may be affected by drinking water contaminated by the site.

In 1974, Mr. Himes was advised by the State Health Commissioner to drill deep wells for six local residences that were shown to have contaminated shallow wells.

In 1975, Mr. Himes signed a consent agreement (adopted by the Stream Pollution Control Board) that resulted in the closing of the landfill in September 1976. Much of the landfill was covered by sand. Several leachate streams were visible during the site inspection of July 30, 1984 by the E & E FIT.

In 1980, the USGS conducted a hydrogeologic study of the area and this helped influence the installation by U.S. EPA of two interceptor wells to divert contaminated groundwater away from the North Main Street Well Field located approximately 1 1/2 miles south east of the site. The interceptor wells have NPDES permits and discharge into nearby Christiana Creek.

222:1T

DETECTED METALS - 1984
Himco Dump
Elkhart, Indiana

Units: ug/l (pph)

Analytes	Field Blank	Upgradient Wells		E/17'	E/174'	H/24'	Dup H/24'	P/24'	Offsite Down Gradient		Surface Water		Sediment Units: mg/kg (ppm)	
		D/19'	D/174'						1/35'	1/172'	UG	DG	UG	DG
Aluminum	-	12,500	-	350,000	-	296	269	175	1,890	-	-	-	1,640	424
Arsenic	-	26	-	200	-	-	-	26	-	-	-	-	1.8	2.0
Barium	-	121	-	803	165	172	175	97	414	66	-	-	14	-
Beryllium	-	-	-	11	-	-	-	-	-	-	-	-	-	-
Cadmium	-	-	-	10	-	-	-	-	-	-	-	-	-	-
Chromium	-	370	-	461	-	16	12	-	-	-	-	-	3.9	1.3
Cobalt	-	-	-	132	-	-	-	-	-	-	-	-	2.7	-
Copper	-	73	-	555	-	-	-	-	-	-	-	-	3.9	-
Iron	-	67,400	1,230	146,000	1,580	12,300	14,800	11,400	5,520	507	246	210	4,380	1,550
Lead	-	73	-	401	-	7.7	9.0	6.7	-	-	-	-	5.8	1.6
Manganese	-	1,630	158	2,150	41	331	320	182	133	24	24	12	43	103
Mercury	-	0.21	-	1.4	-	-	-	-	-	-	-	-	-	-
Nickel	-	103	-	422	-	-	-	-	-	-	-	-	4.4	-
Selenium	-	-	2.0	14	-	-	-	4.7	-	-	-	-	-	-
Tin	-	-	-	-	32	-	-	-	-	55	-	-	1.1	1.2
Vanadium	-	-	-	326	-	-	-	-	-	-	-	-	-	-
Zinc	11	164	38	1,630	44	274	309	58	18	55	65	-	19	5

- = Not detected at or above contract required detection limit.

UG = Upgradient

DG = Downgradient

X/YY' = Well/sampling depth in feet.

ARCS/P/HIMCO/ABB

DETECTED ORGANICS - 1984

Himco Dump
Elkhart, Indiana

Units: ug/l (ppb)

Compound	Field Blank	Upgradient Wells		E/17'	E/174'	H/24'	Dup H/24'	P/24'	Offsite Down Gradient		Surface Water		Sediment Units: ug/kg (ppb)	
		D/12'	D/174'						1/35'	1/172'	UG	DG	UG	DG
Volatiles														
Acetone	32	39	39		164	60	100	230					492 C	66 C
Benzene	5 K	5 K	5		5 K	5 K	5 K	4	5 K		5 K	5 K		10 K
2-Butanone					106		79							
Chloroethane								13						
Chlorofluoromethane					43 J	57 J	37 J	18 J						
Dichlorodifluoromethane					61 J	79 J	56 J	14 J						
1,1-Dichloroethane								15						
Trans 1,2-Dichloroethane					8	9	7							
Diethylether								44 J					45 J	78 J
1,4-Dioxane								9 J						
Ethylbenzene									5 K					
2-Hexanone									5 K					
Methylene Chloride				5 K	5 K	5			5 K		15 C		319 C	249 C
Toluene	5 K			5 K	5 K	3	5 K	5 K	5 K	5 K			10 K	10 K
Trichloroethane					5 K		5 K	5 K						
Carbon Disulfide									1					
Semi-Volatiles														
1,2,4-Trichlorobenzene					10 K									
1,4-Dichlorobenzene					7 K									

K - Compound detected above instrument detection limit but below contract required detection limit.

J - Compound identified by computer library search, concentration estimated.

C - Associated lab blank contained detectable level, value reported has had blank level subtracted from it.

UG - Upgradient.

DG - Downgradient.

X/YY' - Well/sampling depth in feet.

DETECTED ORGANICS - 1984
Himco Dump
Elkhart, Indiana
(Continued)

Units: ug/l (ppb)

Compound	Field Blank	Upgradient Wells		E/17'	E/174'	M/24'	Dup M/24'	P/24'	Offsite Down Gradient		Surface Water		Sediment Units: ug/kg (ppb)	
		D/12'	D/174'						1/35'	1/172'	UG	DG	UG	DG
Naphthalene	10 K													
Di-N-Butylphthalate	10 K	10 K	10 K	10 K	15	10 K		10 K	10 K	10 K	10 K	10 K		
Acenaphthene					25 K									
2,4-Dinitrotoluene					20 K									
N-Nitrosodipropylamine					9									
Pyrene					13									
Phenol						62	76							
4-Methylphenol						197	235							
Bis(2-ethylhexyl) phthalate						10 K	266 C	20						
Diethylphthalate	10 K			10 K					10 K				150 K	
Caprolactam						274 J	145 J							
Sulfur						39 J	41 J						1180 J	
Dioctylester-hexanonedioic acid							1190 J							

Unknowns

Volatile fraction

5 J

Semi-Volatile fraction

1080 J 1390 J

PCB/Pesticides

None detected

K - Compound detected above instrument detection limit but below contract required detection limit.

J - Compound identified by computer library search, concentration estimated.

C - Associated lab blank contained detectable level, value reported has had blank level subtracted from it.

UG - Upgradient

DG - Downgradient

ARCS/P/HIMCO/AB7

77 - 376

I-1

DIVISION OF WATER
DEPARTMENT OF NATURAL RESOURCES, STATE OF INDIANA
STATE OFFICE BUILDING
INDIANAPOLIS, INDIANA 46204
Telephone 633-5267 Area Code 317.

WATER WELL RECORD

WELL LOCATION

(Fill in completely - Refer to instruction sheet)

County in which well was drilled Elkhart Civil Township Cleveland
Driving directions to the well location: Include County Road Names, Numbers, Subdivision Name, lot number, distinctive landmarks, etc. Twp. 38E N. 4E Sec. 36
About 1/2 mi. N. of Lawrence St. on Co. Rd. 20 E about 1/2 mi. N. of Rte. - 1. Well

NAME OF WELL OWNER and/or BUILDING CONTRACTOR

Well Owner U. S. Ecological Survey Address 1810 N. Meridian, Indianapolis, Ind.

Building Contractor _____ Address _____

Name of Well Drilling Contractor: Critman Drilling, Inc.

Address 717 E. Malfalfa Road, Yokum, Indiana

Name of Drilling Equipment Operator: Rich G., Lowell C., Dan E., Frank C.

WELL INFORMATION

Depth of well: 496 Date well was completed: Oct. 6, 1977

Diameter of casing or drive pipe: 5" PVC Total Length: 490

Diameter of liner (if used): 4 1/2" Length: 3' long Total Length: _____

Diameter of Screen: 4 1/2" Length: 3' long Slot Size: .015 SS NW bottom screen
.040 SS NW top screen

Type of Well: Drilled ☒ Gravel Pack ☐ Driven ☐ Other _____

Use of Well: For Home ☐ Test For Industry ☐ For Public Supply ☐ Stock ☐

Method of Drilling: Cable Tools ☐ Rotary ☒ Rev. Rotary ☐ Jet ☐ Bucket Rig ☐

Static water level in completed well (Distance from ground to water level) 6.5 feet

Bailer Test: Hours Tested _____ Rate _____ g.p.m. Drawdown _____ ft. (Drawdown is the difference between static level and water level at end of test)

Pumping Test: Hours Tested 1hr Rate 60 g.p.m. Drawdown _____ ft.

Signature Critman Drilling, Inc.

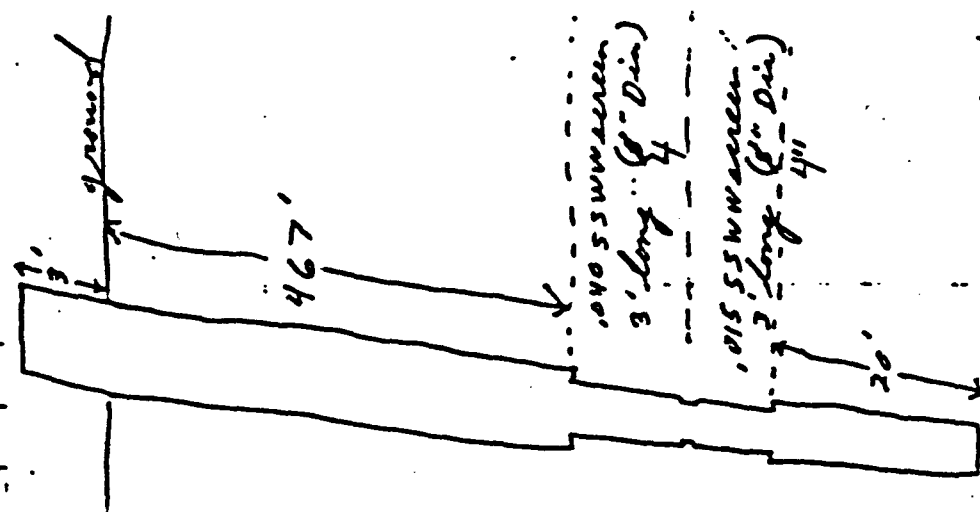
Date October 27, 1977

WATER WELL LOG

FORMATIONS (Color, type of material, hardness, etc.)	From	To
fine to med. sand & gravel	0	30
med. to coarse sand & gravel	30	48
fine to med. sand w/ some gravel	48	160
fine to med. gravel w/ some sand - finer at bottom	160	240
red. gravel w/ some sand	240	275
fine to med. gravel w/ sand	275	300
med. gravel w/ some sand	300	318
fine to med. gravel	318	375
fine gravel & sand	375	465
red. gravel & broken stone	465	475
fine to med. gravel & broken stone	475	489
blue shale	489	492
brown siltstone	492	496
16 hrs.		
NOTE: 18 fts. 200 PSI (20')		
6 fts. 160 PSI (20')		
1 ft. 160 PSI plain end		

COUNTY San Diego TWP. 22N RGE. 4E SEC. 36
 Topo Map _____
 Field Located By 1/1/77 Date 1/1/77
 Courthouse Location By _____ Date _____
 Location accepted w/o verification by _____

FOR ADMINISTRATIVE USE ONLY
 (Well driller does not fill out)
 1300 Ft W of EL _____
 Ft N of SL _____
 Ft E of WL _____
 5 Ft S of NL _____
 Ground Elevation 762
 Depth to bedrock 489
 Bedrock elevation 273
 Aquifer elevation _____
 Lot Number _____



COMPOSITE LITHOLOGIC LOG

(DATA FROM DRILLER'S AND GAMMA LOGS)

[illegible]

77 - 376

C-1

DIVISION OF WATER
DEPARTMENT OF NATURAL RESOURCES, STATE OF INDIANA
STATE OFFICE BUILDING
INDIANAPOLIS, INDIANA 46204
Telephone 633-5267 Area Code 317

WATER WELL RECORD

WELL LOCATION

(Fill in completely - Refer to instruction sheet)

County in which well was drilled Elkhart Civil Township Cleveland
Driving directions to the well location: Include County Road Names, Numbers, Subdivision Name, lot number, distinctive landmarks, etc. Twp. 38N R. 4E Sec. 36
About 1/2 Mi. W. of Nappanee St. on Co. Rd. 10 about 1/8 Mi. N. of E. - N. Well

NAME OF WELL OWNER and/or BUILDING CONTRACTOR

Well Owner U. S. Geological Survey Address 1819 N. Meridian, Indianapolis, Ind.

Building Contractor _____ Address _____

Name of Well Drilling Contractor: Ortman Drilling, Inc.

Address 717 S. Malfalfa Road, Kokomo, Indiana

Name of Drilling Equipment Operator: Rick O., Frank G., Lowell C., Dan E.

WELL INFORMATION

Depth of well: 355 Date well was completed: Oct. 4, 1977

Diameter of casing or drive pipe: 5" PVC Total Length: 337 1/2

Diameter of liner (if used): _____ Total Length: _____

Diameter of Screen: 2" Length: 5' long Slot Size: .018 SS WW

Type of Well: Drilled ☒ Gravel Pack ☐ Driven ☐ Other ☐

Use of Well: For Home ☐ Test ☐ For Industry ☐ For Public Supply ☐ Stock ☐

Method of Drilling: Cable Tools ☐ Rotary ☒ Rev. Rotary ☐ Jet ☐ Bucket Rig ☐

Static water level in completed well (Distance from ground to water level) 6.7 feet

Bailer Test: Hours Tested _____ Rate _____ g.p.m. Drawdown _____ ft. (Drawdown is the difference between static level and water level at end of test)

Pumping Test: Hours Tested 4 hr Rate 35 g.p.m. Drawdown _____ ft.

Signature William L. Willey, Secretary

Date October 27, 1977

FOR ADMINISTRATIVE USE ONLY

(Well driller does not fill out)

COUNTY Elkhart TWP. 34N RGE. 7E SEC. 36 Subdivision NameTopo Map OscodaField Located By U.S.G.S. Date 10/1/00

Courthouse Location By _____ Date _____

Location accepted w/o verification by _____

Ft W of ELGround Elevation 759_____
Ft N of SL

Depth to bedrock _____

26.50
Ft E of WL

Bedrock elevation _____

10.50
Ft S of NL

Aquifer elevation _____

Lot Number _____

WATER WELL LOG

FORMATIONS (Color, type of material, hardness, etc.)	From	To
med. to coarse sand & gravel	0	55
fine to med. sand & fine gravel - very sandy	55	135
95 - 100 streaks of gray clay		
sand brown clay	135	143
med. sand w/some gravel	143	147
sandy brown clay	147	149
med. sand w/some gravel	149	151
sandy brown clay	151	153
sand & gravel	153	154
brown-gray clay	154	156
sand & gravel	156	159
brownish gray clay	159	160
sand & gravel	160	161
brownish gray clay	161	180
medium sand & gravel	180	195
fine to med. sand & gravel (sandy)	195	210
fine to med. sand & gravel (sandy) & some brownish gray clay mixed	210	228
brownish gray clay	228	230
fine to med. sand & some gravel	230	235
med. sand & gravel w/some broken shale	235	255
fine sand	255	305
fine to med. sand & fine gravel	305	343
fine sand	343	355
bottom of screen 340 ft.		
10 hrs.		
NOTE: 8 jts. 200 PSI (20)		
8 jts. 160 PSI (20+)		
1 ft. 160 PSI plain		
(casing cut threaded at 116 ft.		

WELL LOCATION

(Fill in completely - Refer to instructions above)

Elkhart

County of Elkhart, Indiana

Being directions to the well location: Indiana, etc.

About 1/2 mi. N. of Co. Rd. 10 on Napoleon St. on W. side of Rd.

U. S. GEOLOGICAL SURVEY

WRD - INDIANA

NAME OF WELL OWNER COMPOSITE LITHOLOGIC LOG OR

(DATA FROM DRILLER'S AND GAMMA LOGS)

PROJECT: ELKHART

COUNTY: ELKHART

WELL # C-1

INTERPRETATION BY: A. Martin

DATE: 4/20/79

FORMATION

FROM

TO

Sand & Gravel 1475 0 147

Sandy Clay 147 149

Sand & Gravel 25 149 151

Sandy Clay 151 153

Sand & Gravel 153 154

Clay 154 155

Sand & Gravel 35 156 159

Clay 159 160

Sand & Gravel 160 161

Clay 161 170

Sand & Gravel 48 180 228

Clay 228 230

Sand & Gravel 125 230 355

D-2

COUNTY

4

D-2

COUNTY

D-2

COUNTY

(DATA FROM DRILLER'S AND GAMMA LOGS)

COUNTY: ELKHART

INTERPRETATION BY: A. M. ...

DATE: 4/30/79

[illegible]

77 - 376

E-Test Hole

DIVISION OF WATER
DEPARTMENT OF NATURAL RESOURCES, STATE OF INDIANA
STATE OFFICE BUILDING
INDIANAPOLIS, INDIANA 46204
Telephone 633-5267 Area Code 317

WATER WELL RECORD

WELL LOCATION

(Fill in completely - Refer to instruction sheet)

County in which well was drilled Elkhart Civil Township Cleveland
Driving directions to the well location: Include County Road Names, Numbers, Subdivision Name, lot number, distinctive landmarks, etc. Twp. 38N R. 4E Sec. 36
About 800' W. of Nanphee St. on N. side of Co. Rd. 10 - South Side

NAME OF WELL OWNER and/or BUILDING CONTRACTOR

Well Owner U. S. Geological Survey Address 1819 N. Meridian, Indianapolis, Ind.
Building Contractor _____ Address _____
Name of Well Drilling Contractor: Ortman Drilling, Inc.
Address 717 S. Malfalfa Road, Kokomo, Indiana
Name of Drilling Equipment Operator: Rick C., Frank G., Lowell C., Dan E.

WELL INFORMATION

Depth of well: 315 Date well was completed: Oct. 10, 1977
Diameter of casing or drive pipe: none Total Length: _____
Diameter of liner (if used): _____ Total Length: _____
Diameter of Screen: none Length: _____ Slot Size: _____
Type of Well: Drilled ☒ Gravel Pack ☐ Driven ☐ Other _____
Use of Well: For Home ☐ Test For Industry ☐ For Public Supply ☐ Stock ☐
Method of Drilling: Cable Tools ☐ Rotary ☒ Rev. Rotary ☐ Jet ☐ Bucket Rig ☐
Static water level in completed well (Distance from ground to water level) none feet
Bailer Test: Hours Tested _____ Rate _____ g.p.m. Drawdown _____ ft.
Pumping Test: Hours Tested _____ Rate _____ g.p.m. Drawdown _____ ft.

(Drawdown is the difference between static level and water level at end of test)

Signature William J. [illegible]
Date October 27, 1977

77 - 376

F - 5

DIVISION OF WATER
DEPARTMENT OF NATURAL RESOURCES, STATE OF INDIANA
STATE OFFICE BUILDING
INDIANAPOLIS, INDIANA 46204
Telephone 633-5267 Area Code 317

WATER WELL RECORD

WELL LOCATION

(Fill in completely - Refer to instruction sheet)

County in which well was drilled Elkhart Civil Township Osolo
Driving directions to the well location: Include County Road Names, Numbers, Subdivision Name, lot number, distinctive landmarks, etc. Twp. 36N R. 5E Sec. 30
On N. sd. of Tr. Rt. 19 where Rd. starts to curve to S. E. Well

NAME OF WELL OWNER and/or BUILDING CONTRACTOR

Well Owner U. S. Geological Survey Address 1819 N. Meridian, Indianapolis, Ind.

Building Contractor _____ Address _____

Name of Well Drilling Contractor: Crtman Drilling, Inc.

Address 717 S. Malfalfa Road, Kokomo, Indiana

Name of Drilling Equipment Operator: Rick O., Frank G., Lowell C., Dan E.

WELL INFORMATION

Depth of well: 225 Date well was completed: Oct. 11, 1977

Diameter of casing or drive pipe: 5" PVC Total Length: 126

Diameter of liner (if used): _____ Total Length: _____

Diameter of Screen: 2" Length: 5' long Slot Size: .018 SS WW
2 Screens 12' overall 195' to bottom of screen

Type of Well: Drilled ☒ Gravel Pack ☐ Driven ☐ Other _____

Use of Well: For Home ☐ Test For Industry ☐ For Public Supply ☐ Stock ☐

Method of Drilling: Cable Tools ☐ Rotary ☒ Rev. Rotary ☐ Jet ☐ Bucket Rig ☐

Static water level in completed well (Distance from ground to water level) 15.4 feet

Bailer Test: Hours Tested _____ Rate _____ g.p.m. Drawdown _____ ft. (Drawdown is the difference between static level and water level at end of test)

Pumping Test: Hours Tested Air Rate 30 g.p.m. Drawdown _____ ft.

Signature Crtman Drilling, Inc.

Date October 26, 1977

WATER WELL LOG

[illegible]

U. S. GEOLOGICAL SURVEY
WRD - INDIANA
COMPOSITE LITHOLOGIC LOG

(DATA FROM DRILLER'S AND GAMMA LOGS).....

PROJECT: ELKHART		COUNTY: ELKHART	
WELL # F-5		INTERPRETATION BY: A. M. ...	
DATE: 4/12/79			
FORMATION		FROM	TO
Sand & Gravel	37 1/2	0	37
Clay		31	79
Dark Sand	14 1/2	79	93
Clay		93	100
Light Sand	28 1/2	100	128
Sandy Clay		128	135
Sand & Gravel	23 1/2	135	157
Clay		158	166
Sand	1	166	167
Clay		167	182
Sand & Gravel	13 1/2	182	195
Clay w/ streaks of sand		195	212
Clay		212	220
Shale		220	220

DIVISION OF WATER
DEPARTMENT OF NATURAL RESOURCES, STATE OF INDIANA
STATE OFFICE BUILDING
INDIANAPOLIS, INDIANA 46204
Telephone 633-5267 Area Code 317

WATER WELL RECORD

WELL LOCATION

(Fill in completely - Refer to instruction sheet)

County in which well was drilled Elkhart Civil Township Osolo
Driving directions to the well location: Include County Road Names, Numbers, Subdivision Name, lot number, distinctive landmarks, etc. Twp. 3EN R. 5E Sec. 31
W. of Bristol St. on Edwardsburg Ave. 1 block, th. W. about 150' on N. rd. N. Well

NAME OF WELL OWNER and/or BUILDING CONTRACTOR

Well Owner U. S. Geological Survey Address 1619 N. Meridian, Indianapolis, Ind.

Building Contractor _____ Address _____

Name of Well Drilling Contractor: Ortman Drilling, Inc.

Address 717 S. Malfalfa Road, Kokomo, Indiana

Name of Drilling Equipment Operator: Rick O., Frank G., Lowell C., Dan E.

WELL INFORMATION

Depth of well: 224 Date well was completed: Oct. 17, 1977

Diameter of casing or drive pipe: 5" PVC Total Length: 160

Diameter of liner (if used): _____ Total Length: _____

Diameter of Screen: 2" Length: 5' long Slot Size: .018 SS WW
2 Screens 12' overall

Type of Well: Drilled ☒ Gravel Pack ☐ Driven ☐ Other 169' to bottom of scr

Use of Well: For Home ☐ Test For Industry ☐ For Public Supply ☐ Stock ☐

Method of Drilling: Cable Tools ☐ Rotary ☒ Rev. Rotary ☐ Jet ☐ Bucket Rig ☐

Static water level in completed well (Distance from ground to water level) 8.3 feet

Bailer Test: Hours Tested _____ Rate _____ g.p.m. Drawdown _____ ft.

Pumping Test: Hours Tested Air Rate 75 g.p.m. Drawdown _____ ft.

(Drawdown is the difference between static level and water level at end of test)

Signature Ortman Drilling, Inc.
Date October 26, 1977

13/12/55

Aquifer elevation _____ **Lot Number** _____

1 ft. 160 PSI plain end

77 - 276

I-1

DIVISION OF WATER
DEPARTMENT OF NATURAL RESOURCES, STATE OF INDIANA
STATE OFFICE BUILDING
INDIANAPOLIS, INDIANA 46204
Telephone 633-5267 Area Code 317

WATER WELL RECORD

WELL LOCATION

(Fill in completely - Refer to instruction sheet)

County in which well was drilled Elkhart Civil Township Cleveland
Driving directions to the well location: Include County Road Names, Numbers, Subdivision Name, lot number, distinctive landmarks, etc. Twp. 38N R. 4E Sec. 36
1 Block N. of Mishavaka St. on Kappanee St., th. W. 1/2 Block on S. sd. W. Well

NAME OF WELL OWNER and/or BUILDING CONTRACTOR

Well Owner U. S. Geological Survey Address 1819 N. Meridian, Indianapolis, Ind.
Building Contractor _____ Address _____
Name of Well Drilling Contractor: Ortman Drilling, Inc.
717 S. Malfalfa Road, Kokomo, Indiana
Address _____
Name of Drilling Equipment Operator: Frank C., Lowell C.

WELL INFORMATION

Depth of well: 195 Date well was completed: Oct. 13, 1977
Diameter of casing or drive pipe: 5" PFC Total Length: 163
Diameter of liner (if used): _____ Total Length: _____
Diameter of Screen: 2" Length: 5' Slot Size: .030 SS WW
2 Screens - 12' overall 172' to bottom of screen
Type of Well: Drilled ☒ Gravel Pack ☐ Driven ☐ Other _____
Use of Well: For Home ☐ Test ☐ For Industry ☐ For Public Supply ☐ Stock ☐
Method of Drilling: Cable Tools ☐ Rotary ☒ Rev. Rotary ☐ Jet ☐ Bucket Rig ☐
Static water level in completed well (Distance from ground to water level) 9 feet
Bailer Test: Hours Tested _____ Rate _____ g.p.m. Drawdown _____ ft. (Drawdown is the difference between static level and water level at end of test)
Pumping Test: Hours Tested Air Rate 100 g.p.m. Drawdown _____ ft.

Signature Ortman Drilling, Inc.
Date October 26, 1977

12.2.

COUNTY San Diego

TWP:

LARGE.

SE

— 42 —

42

SEC

36

Subdivision Name

Topo Map

Field Located

By

Date

Courthouse Location By

Date _____

Location accepted w/o verification by

Fi W of EL

Ground Elevation

752

Fit N of SL.

Depth to bedrock

193

Fit E of WL.

Bedrock elevation

559

Fit S of NL.

Aquifer elevation

Lot Number

WATER WELL LOG

[illegible]

U. S. GEOLOGICAL SURVEY

WRD - INDIANA

COMPOSITE LITHOLOGIC LOG

(DATA FROM DRILLER'S AND GAMMA LOGS)

PROJECT: ELKHART	COUNTY: ELKHART	
WELL # I-3	INTERPRETATION BY: A. H.	
DATE: 4/12/77		
FORMATION	FROM	TO
Sand & Gravel 32 1/2	0	33
Clay	33	43
Sandy Clay	43	54
Clay	54	88
Sand 3 3/4	89	92
Sandy Clay	92	124
Sand & Gravel 50 3/4	124	174
Clay	174	84
Gravel 9 1/2	184	193
Shale	193	195

DIVISION OF WATER
DEPARTMENT OF NATURAL RESOURCES, STATE OF INDIANA
STATE OFFICE BUILDING
INDIANAPOLIS, INDIANA 46204
Telephone 633-5267 Area Code 317

WATER WELL RECORD

WELL LOCATION

(Fill in completely - Refer to instruction sheet)

County in which well was drilled Elkhart Civil Township Osolo ?
Driving directions to the well location: Include County Road -Names, Numbers, Subdivision Name, lot number, distinctive landmarks, etc. Twp. 38N R. 5E Sec. 32 E
Southwest Corner of Oak St. & McNaughton St.

NAME OF WELL OWNER and/or BUILDING CONTRACTOR

Well Owner U. S. Geological Survey Address 1819 N. Meridian, Indianapolis, Ind.

Building Contractor _____ Address _____

Name of Well Drilling Contractor: Crtman Drilling, Inc.

Address 717 S. Malfalfa Road, Kokomo, Indiana

Name of Drilling Equipment Operator: Pick C., Frank C., Lowell C., Dan F.

WELL INFORMATION

Depth of well: 175 Date well was completed: Oct. 12, 1977

Diameter of casing or drive pipe: 5" Total Length: 149

Diameter of liner (if used): _____ Total Length: _____

Diameter of Screen: 2" Length: 5' Slot Size: .040 S: WW

Type of Well: Drilled ☒ Gravel Pack ☐ Driven ☐ Other 152' to bottom of screen

Use of Well: For Home ☐ Test ☐ For Industry ☐ For Public Supply ☐ Stock ☐

Method of Drilling: Cable Tools ☐ Rotary ☒ Rev. Rotary ☐ Jet ☐ Bucket Rig ☐

Static water level in completed well (Distance from ground to water level) 13.9 feet

Bailer Test: Hours Tested _____ Rate _____ g.p.m. Drawdown _____ ft. (Drawdown is the difference between static level and water level at end of test)

Pumping Test: Hours Tested 1hr Rate 20 g.p.m. Drawdown _____ ft.

Signature C. Crtman Drilling, Inc.

Date October 26, 1977

(Well driller does not fill out)

12/12/20

TWP:

TWP. 58 N. 1

URGE

172

24

 $\frac{1}{4}$

SEC

51

Subdivision Name

22-50

 Ft W of EL

Ground Elevation

254

By

1975

Date

155

 Ft N of SL.

Depth to bedrock

165

Courthouse Location By

Date

File of WL

Bedrock elevation

589

Location accepted w/o verification by

Fl S of NL.

Aquifer elevation

Lot Number

[illegible]

U. S. GEOLOGICAL SURVEY

WRD - INDIANA

COMPOSITE LITHOLOGIC LOG

(DATA FROM DRILLER'S AND GAMMA LOGS)

PROJECT: ELKHART	COUNTY: ELKHART	WELL # 1-3	INTERPRETATION BY: A.M.M.	DATE: 4/10/73
FORMATION				
	From	To		
Sand & Gravel	42	0		
Clay	56	42		
Dir. Sand	59	56		
Clay	112	59		
Dir. Sand	121	112		
Sandy Clay	136	121		
Sand & Gravel	141	136		
Sand & Clay	144	141		
Sand & Gravel	155	144		
Clay	165	155		
Shale	175	165		

DIVISION OF WATER
DEPARTMENT OF NATURAL RESOURCES, STATE OF INDIANA
STATE OFFICE BUILDING
INDIANAPOLIS, INDIANA 46204
Telephone 633-5267 Area Code 317

100
M

WATER WELL RECORD

WELL LOCATION

(Fill in completely - Refer to instruction sheet)

County in which well was drilled Elkhart Civil Township _____
Driving directions to the well location: Include County Road Names, Numbers, Subdivision Name, lot number, distinctive landmarks, etc.

NAME OF WELL OWNER and/or BUILDING CONTRACTOR

Well Owner James A. Rogers Address 1000 N. Jefferson St. Elkhart, Ind. 46516

Building Contractor _____ Address _____

Name of Well Drilling Contractor: James A. Rogers

Address _____

Name of Drilling Equipment Operator: James A. Rogers

WELL INFORMATION

Depth of well: 28.63 Date well was completed: 5/3/79

Diameter of casing or drive pipe: 2" Galv Total Length: 53'

Diameter of liner (if used): _____ Total Length: _____

Diameter of Screen: 2" Length: 5' Slot Size: 18

Type of Well: Drilled ☒ Gravel Pack ☐ Driven ☐ Other _____

Use of Well: OPERATION For Home ☐ For Industry ☐ For Public Supply ☐ Stock ☐

Method of Drilling: ROVERS Cable Tools ☐ Rotary ☐ Rev. Rotary ☐ Jet ☐ Bucket Rig ☐

Static water level in completed well (Distance from ground to water level) 29 feet

Bailer Test: Hours Tested _____ Rate _____ g.p.m. Drawdown _____ ft.

Pumping Test: Hours Tested _____ Rate _____ g.p.m. Drawdown _____ ft.

(Drawdown is the difference between static level and water level at end of test)

Signature _____

Date _____

WATER WELL LOG

FORMATIONS (Color, type of material, hardness, etc.)	From	To
WHITE FINE SAND - 10' THICK	0	10
GREY SAND	10	16
BLACK GLYPH TUBE OF SAND	16	25
DOY BROWN FINE SAND & MED GRAVEL	25	32
BRICKS, COALS & LIMESTONE IN SAND	32	43
GREY FINE SAND & MED GRAVEL	43	
BTH	105	
AUGERS FILLED W/ FINE SAND		
PUSHED #13 SCREEN + GALVANIZED		
PIPE IN OPEN HOLE TO 103'		
SEALED W/ BENTONITE		
TD = 75' - 3' SAND IN WELL		
COULD NOT DEVELOP W/ PUMP		
USED AIR COMPRESSOR TO DEVELOP		
WELL		
TD = 103.2 + 0.43 = 103.65		
W/L ≈ 9'		

FOR ADMINISTRATIVE USE ONLY
(Well driller does not fill out)

COUNTY ECCLART TWP. 38N RGE. 4E NW X SE X NE SEC. 36
Topo Map OSCONA
Field Located By LLGGS Date 5/3/29
Courthouse Location By _____ Date _____
Location accepted w/o verification by _____

 900 Ft W of EL. Ground Elevation 767

_____ Ft N of SL. Depth to bedrock _____

_____ Ft E of WL. Bedrock elevation _____

1700 Ft S of NL. Aquifer elevation _____

Lot Number _____
Subdivision Name _____

DIVISION OF WATER
DEPARTMENT OF NATURAL RESOURCES, STATE OF INDIANA
STATE OFFICE BUILDING
INDIANAPOLIS, INDIANA 46204
Telephone 633-5267 Area Code 317.

STATE
N

WATER WELL RECORD

WELL LOCATION

(Fill in completely - Refer to instruction sheet)

County in which well was drilled ESSEX Civil Township _____
Driving directions to the well location: Include County Road Names, Numbers, Subdivision Name, lot number, distinctive landmarks, etc.

NAME OF WELL OWNER and/or BUILDING CONTRACTOR

Well Owner WILSON Address 1215 N. HENRY

Building Contractor _____ Address _____

Name of Well Drilling Contractor: SAME

Address _____

Name of Drilling Equipment Operator: WILSON / T. WILSON

WELL INFORMATION

Depth of well: 22.95 Date well was completed: 4/30/79

Diameter of casing or drive pipe: 2" Drive Total Length: 25'

Diameter of liner (if used): _____ Total Length: _____

Diameter of Screen: 2" Length: 5' Slot Size: 40

Type of Well: Drilled ☒ Gravel Pack ☐ Driven ☐ Other _____

Use of Well: OBSERVATION For Home ☐ For Industry ☐ For Public Supply ☐ Stock ☐

Method of Drilling: AUGER Cable Tools ☐ Rotary ☐ Rev. Rotary ☐ Jet ☐ Bucket Rig ☐

Static water level in completed well (Distance from ground to water level) 8.41 feet

Bailer Test: Hours Tested _____ Rate _____ g.p.m. Drawdown _____ ft.

Pumping Test: Hours Tested _____ Rate _____ g.p.m. Drawdown _____ ft.

(Drawdown is the difference between static level and water level at end of test)

Signature _____

Date _____

FOR ADMINISTRATIVE USE ONLY

(Well driller does not fill out)

COUNTY Elbert #N TWP. 38N RGE. 4E SE 1/4 SW 1/4 NE SEC. 36 Subdivision NameTopo Map Oscola1900 Ft W of EL.Ground Elevation 763Field Located By USGS Date 4/30/79

Ft N of SL.

Depth to bedrock

Courthouse Location By _____ Date _____

Ft E of WL.

Bedrock elevation

Location accepted w/o verification by _____

2200 Ft S of NL.

Aquifer elevation

Lot Number

WATER WELL LOG

FORMATIONS (Color, type of material, hardness, etc.)	From	To
Med br sand + clay	0	3
Med br sand	3	4
Med br sand & fine gravel	7	17
Water table \approx 8'		
very med sand & fine gravel	17	32
1/4 coarse gravel		
93TH 32'		
5' SS 40' 1/2' gravel		
Drilled \approx 20 gpm		
1 1/2" 900 - 150 = 841		
7/D 24.52 + 43 = 3495		
Set in meter box		

9

DIVISION OF WATER
DEPARTMENT OF NATURAL RESOURCES, STATE OF INDIANA
STATE OFFICE BUILDING
INDIANAPOLIS, INDIANA 46204
Telephone 633-5267 Area Code 317

WATER WELL RECORD

WELL LOCATION

(Fill in completely - Refer to instruction sheet)

County in which well was drilled _____ Civil Township _____

Driving directions to the well location: Include County Road Names, Numbers, Subdivision Name, lot number, distinctive landmarks, etc.

NAME OF WELL OWNER and/or BUILDING CONTRACTOR

Well Owner John J. Brown Address 1234 E. 10th St.

Building Contractor _____ Address _____

Name of Well Drilling Contractor: W. J. Brown

Address _____

Name of Drilling Equipment Operator: James H. Brown

WELL INFORMATION

Depth of well: _____ Date well was completed: 10-1-68

Diameter of casing or drive pipe: 2" Plastic Total Length: _____

Diameter of liner (if used): _____ Total Length: _____

Diameter of Screen: 2" Length: 10' Slot Size: 40

Type of Well: Drilled ☒ Gravel Pack ☐ Driven ☐ Other _____

Use of Well: Observation For Home ☐ For Industry ☐ For Public Supply ☐ Stock ☐

Method of Drilling: Auger Cable Tools ☐ Rotary ☐ Rev. Rotary ☐ Jet ☐ Bucket Rig ☐

Static water level in completed well (Distance from ground to water level) _____ feet

Bailer Test: Hours Tested _____ Rate _____ g.p.m. Drawdown _____ ft.

Pumping Test: Hours Tested _____ Rate _____ g.p.m. Drawdown _____ ft.

(Drawdown is the difference between static level and water level at end of test)

Signature _____

Date _____

FOR ADMINISTRATIVE USE ONLY
(Well driller does not fill out)

COUNTY ECKHART TWP. 38N RGE. 4E SE & NE & SE SEC 36 Subdivision Name _____

Topo Map Osceola 600 Ft W of EL. Ground Elevation 756 _____

Field Located By 11265 Date 4/26/79 1900 Ft N of SL. Depth to bedrock _____

Courthouse Location By _____ Date _____ _____ Ft E of WL. Bedrock elevation _____

Location accepted w/o verification by _____ _____ Ft S of NL. Aquifer elevation _____ Lot Number _____

WATER WELL LOG

[illegible]

APPENDIX B

TECHNICAL MEMORANDA (Phase I Field Work)

TM 1	Soil Boring and Monitoring Well Installation
TM 2	Well Development of EPA Wells
TM 3	Staff Gauge Installation
TM 4	Geotechnical Borings
TM 5	Geotechnical Data Evaluation
TM 6	Private Well Sampling and Basement Air Screening
TM 7	Landfill Cap Soil Sampling
TM 8	Groundwater Sampling
TM 9	Surface Water and Sediment Sampling
TM 10	Test Pit Excavation and Geophysical Exploration Program
TM 11	Slug Testing and Analysis
TM 12	Waste Mass Gas Sampling
TM 13	Installation of Water Table Wells and Landfill Cap Sampling
TM 14	Wetlands Assessment and Identification
TM 15	Wetland Soil Sampling
TM 16	Water Level Measurements
TM 17	Health and Safety

ORIGINAL

TECHNICAL MEMORANDUM NUMBER 1

DATE: January 16, 1991

TO: Vanessa Harris, Site Manager

CC: Marcia Kuehl - RI Lead
Roman Gau - Project Manager
Mike Crosser - TSQAM

FROM: Tom Puchalski

SUBJECT: EPA ARCS Region V Contract No. 68-W8-0093
EPA Work Assignment No. 17-5L4J
Donohue Project No. 20026.023
Himco Dump RI/FS

MONITORING WELL INSTALLATION

Introduction

Four deep groundwater monitoring wells were installed as described in Exhibit A, Field Sampling Plan Addendum to Volume 2, Field Sampling Plan, Himco Dump Remedial Investigation/Feasibility Study, Elkhart, Indiana. Drilling activities for these well installations began on November 27, 1990, and were completed December 15, 1990. These piezometers were installed to provide groundwater samples for chemical analysis and water elevations to be used in groundwater flow analysis. Steve Padovani and Tom Puchalski of Donohue & Associates, Inc., inspected the drilling and well installation activities, completed qualitative logs based upon visual inspection of cuttings liberated during air rotary drilling, performed and documented air monitoring using a photoionization detector and gaspender, and completed well installation documentation forms and activity logs. Drilling and well installations were completed by John Mathes and Associates, Inc. (Columbia, Illinois), with a TH 60, Ingersol Rand air rotary rig.

Methods

Drilling and well installation methods were performed as described in Exhibit A, Field Sampling Plan Addendum to Volume 2, Field Sampling Plan, Himco Dump Remedial Investigation/Feasibility Study, Elkhart, Indiana, Section 4.2.

Air rotary drilling was used to advance boreholes prior to the installation of piezometers. A 7-7/8-inch tricone bit was advanced ahead of 8-inch driven steel casing. No samples were retained from these four borings for piezometer installations, but the Donohue geologist completed an approximate log as drilling progressed based upon visual inspection of drill cuttings.

Piezometers were finished at the following depths: P101B, 98 feet; P101C, 165 feet, P102B, 65.4 feet; and P102C, 159.5 feet. Their locations are provided in Figure 1.

A typical piezometer installation began with steam cleaning of the 2-inch diameter stainless steel well casing and plastic 1-inch diameter tremie pipe. Following steam cleaning, the 5-foot screen (Dietrich 2-inch I.D., flush-threaded, 0.010-inch slot, Schedule 5, Type 304 stainless) and riser (Dietrich 2-inch I.D., flush-threaded, Schedule 5, Type 304 stainless) were wrapped with teflon tape at the joints and threaded together before being lowered into the borehole. Enough 10-foot stainless steel sections were threaded together to allow a 2.5-foot riser stickup to extend above the ground surface. Excess stickup was cut off with a pipe cutter. In P102B, the annular space between the well screen and the borehole wall were backfilled with number 10-20 silica sand (Colorado Silica Sand, Colorado Silica Sand, Inc., Colorado Springs, Colorado) to 3.4 feet above the top of the well screen. P101B, P101C, and P102C were installed with natural formation sand which collapsed onto the well screen from 2 to 4 feet above the top of the well screen.

The placement of the filter pack was followed by the installation of a 2.5- to 3-foot thick bentonite slurry seal. From the bentonite seal to approximately 3 feet from ground surface, the annular space was backfilled with a cement/bentonite grout. A concrete collar was used to cement the protective casing (steel 4-inch diameter) in place. Vented, threaded PVC caps were installed at the top of the 2-inch risers. Protective casings were supplied with locking lids. Boring logs are provided in Appendix A. Well installation diagrams are provided in Appendix B.

Deviations

Intermediate piezometer P102B was installed at 65.4 feet rather than 100 feet since a silt and silty clay layer approximately 34 feet thick was logged beginning at approximately 65 to 70 feet while the boring for P102C was drilled. P102B was installed directly above this confining unit.

P102C was intended to be installed at 175 feet, however, a fine dense sand unit encountered at about 120 feet slowed down the rate of casing advance to less than 20 feet per hour. Very little water was being produced from this zone. Because driving casing became slowed to the point of futility, the well was installed at 159.5 feet by drilling beyond the 140-foot bottom of the 8-inch casing.

P101C was also intended to be installed at 175 feet, however, a large hole developed beneath the back of the rig by settling of sand during casing pounding. This problem, in addition to sand heaving up into the 8-inch casing, forced the installation to occur at 165 feet.

A natural formation sand was used in place of the specified filter pack sand in P102C, P101B, and P101C since sand immediately collapsed the borehole as the drill bit was removed. The 2-inch casing was installed beyond the bottom of the 8-inch casing by jetting water with a tremie pipe while allowing the weight of the 2-inch casing to sink it down to the previously drilled depth. Most of the jetted water circulated back up the 8-inch casing and was not lost to the formation.

Head pressures and loose formation sand also account for natural sand which blew up within the 8-inch casing before the bentonite slurry seal could be installed to the base of the 8-inch casing. Up to 2 feet of sand flowed up into the 8-inch casing prior to seal installation. Specific depths of seal placement are provided for each well in Appendix B.

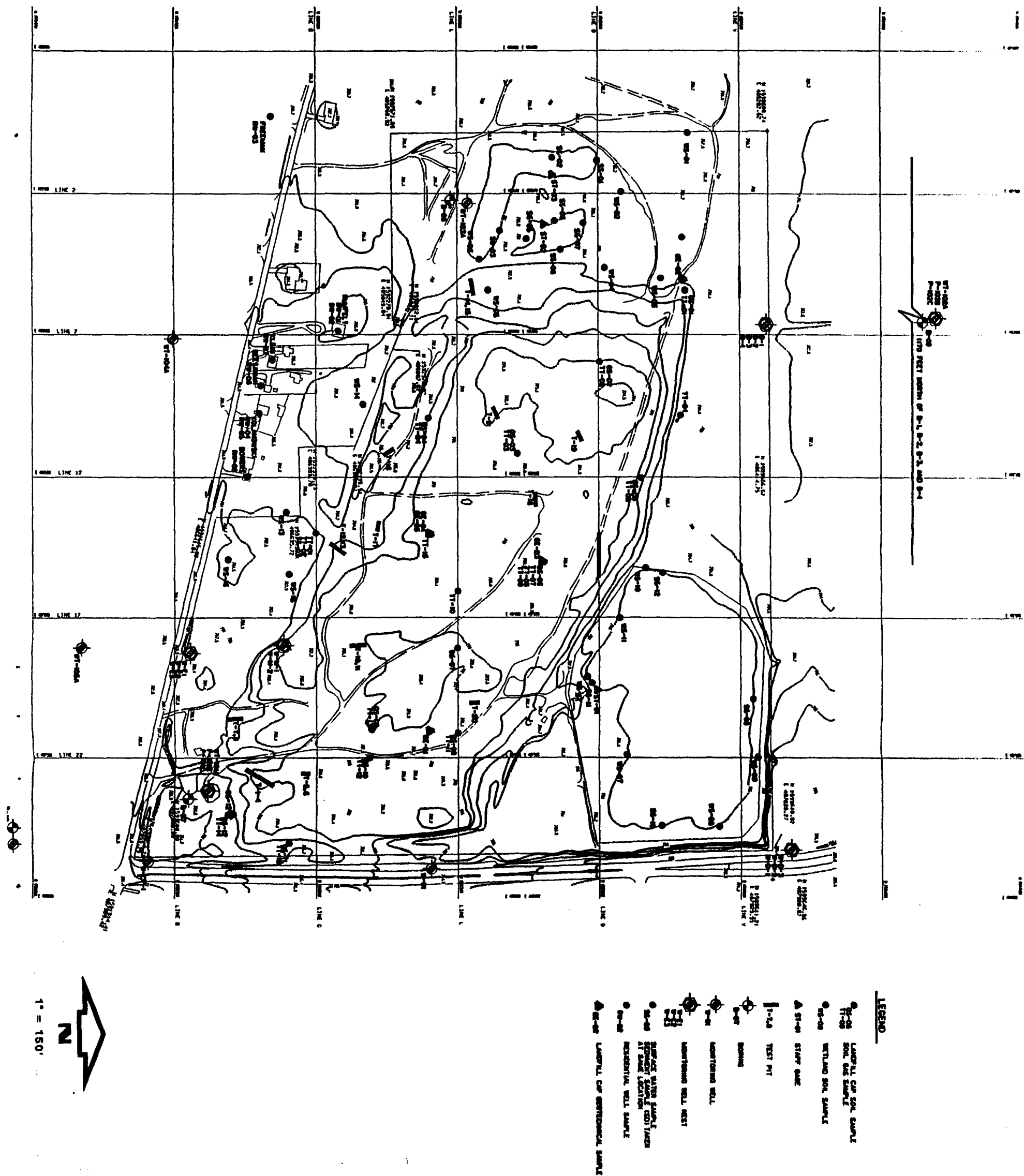
Summary of Results

No samples were retained for this task. The stratigraphy at these locations is provided by boring logs for water table well locations and geotech borings.

The most significant challenge to overcome during these well installations was due to sand heaving up into the 8-inch casing while well installations were being done. The rate of sand heaving was fast enough so that by the time the drill stem was broken and pulled from the boring, up to 70 feet of sand had heaved up into the 8-inch casing. This sand had to be removed prior to well installation.

The sand was cleared from the casing at P102C by jetting water down into the 8-inch casing as the 2-inch casing was installed. Sand and water circulated up and out of the 8-inch casing which allowed the 2-inch casing to drop. Once the sand was removed from the 8-inch casing, further jetting below the 8-inch casing allowed the 2-inch casing to drop below the 8-inch casing and, therefore, expose the 2-inch casing to the formation. This method was required to expose the screen below the 8-inch casing because attempts to pull the casing up were not successful. Shallower installations at P101B and P102B, however, were installed by pulling the 8-inch casing up while the 2-inch casing remained stationary. The installation at P101C required additional effort since the 8-inch casing could not be pulled up, and jetting was not successful beyond the bottom of the 8-inch casing. After two attempts at jetting the well in place, the boring was overdrilled 10 feet and then jetted. This third attempt was successful.

A/R/HIMCO/AH4



MAY 1991

FIGURE 1 SITE LOCATION MAP (TECHNICAL MEMO)

**HIMCO DUMP
SUPERFUND SITE
ELKHART, INDIANA**

20026

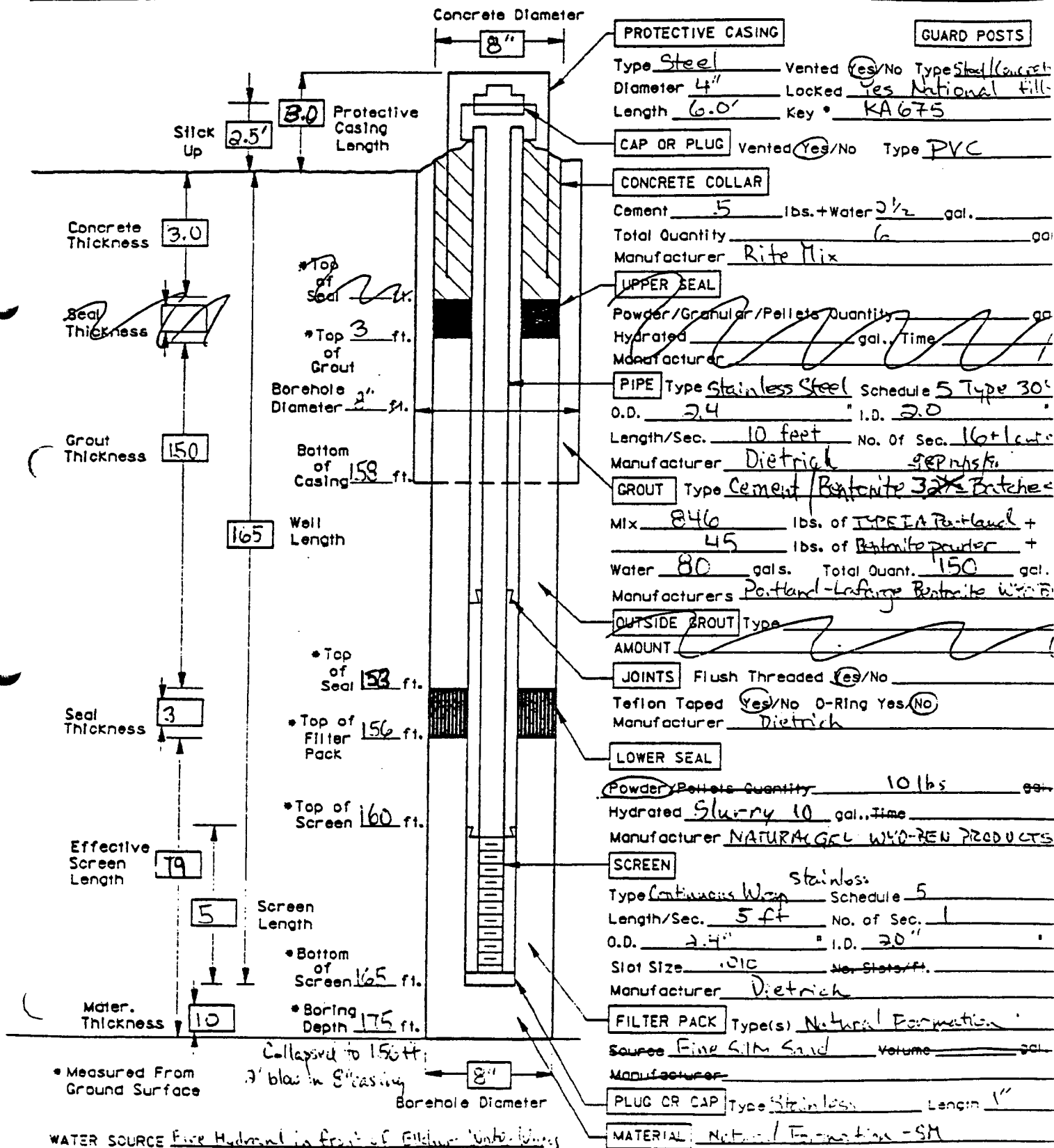
Donohue ENGINEERS
ARCHITECTS
SCIENTISTS

APPENDIX A
APPROXIMATE BORING LOGS

Donohue

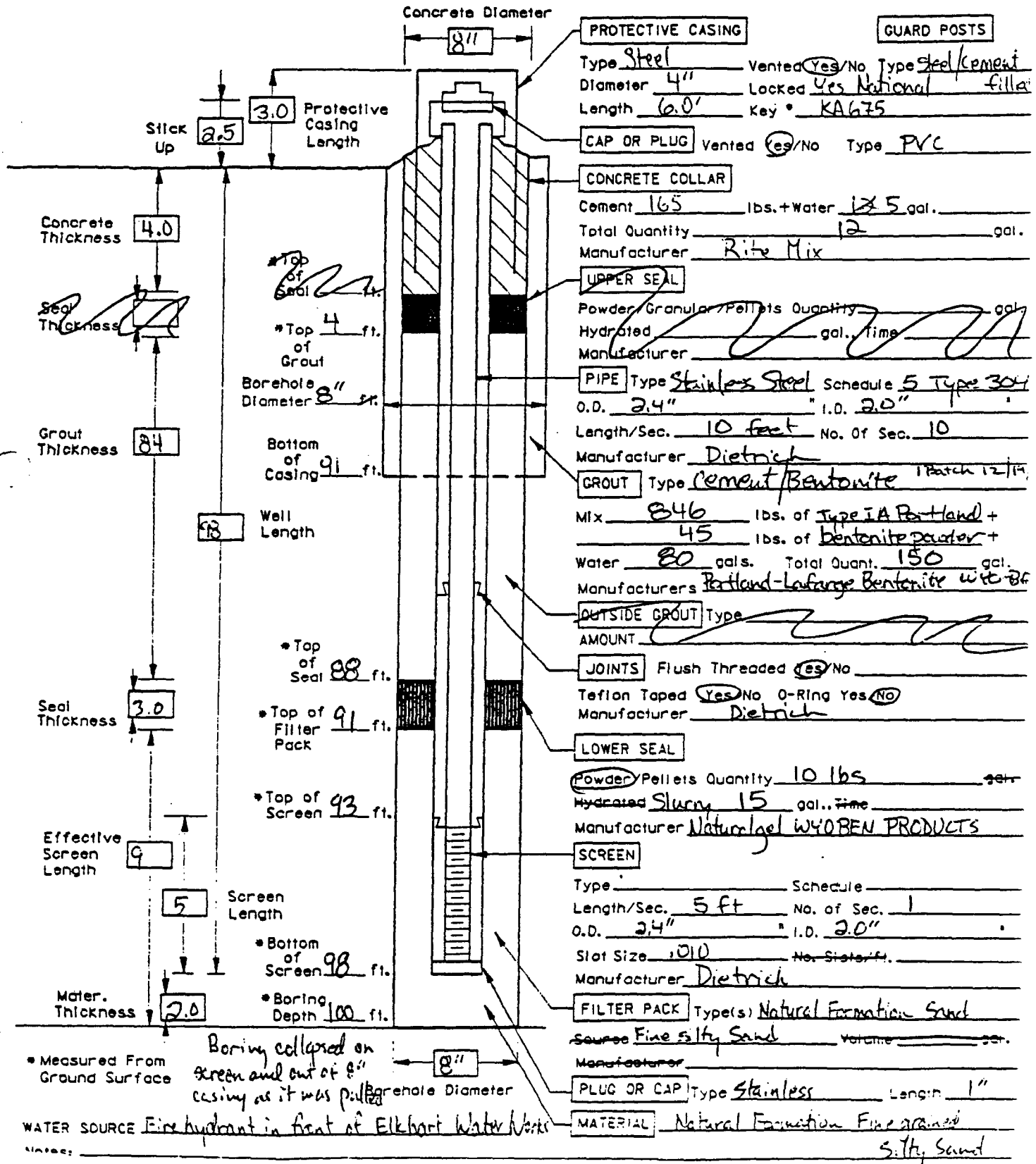
DOUBLE CASING WELL/PIEZOMETER INSTALLATION DIAGRAM

Form 1

Site: HIMCO DUMPDate: 12/12/90Inspected By: Tom PuckettProject No. 30006.023Well No. PIC1CEngineers & Architects
COMPUTER AIDED DESIGN/DRAFTINGDriller/Contractor MAX T. INNIN, DON BREWINGTON/MATHES

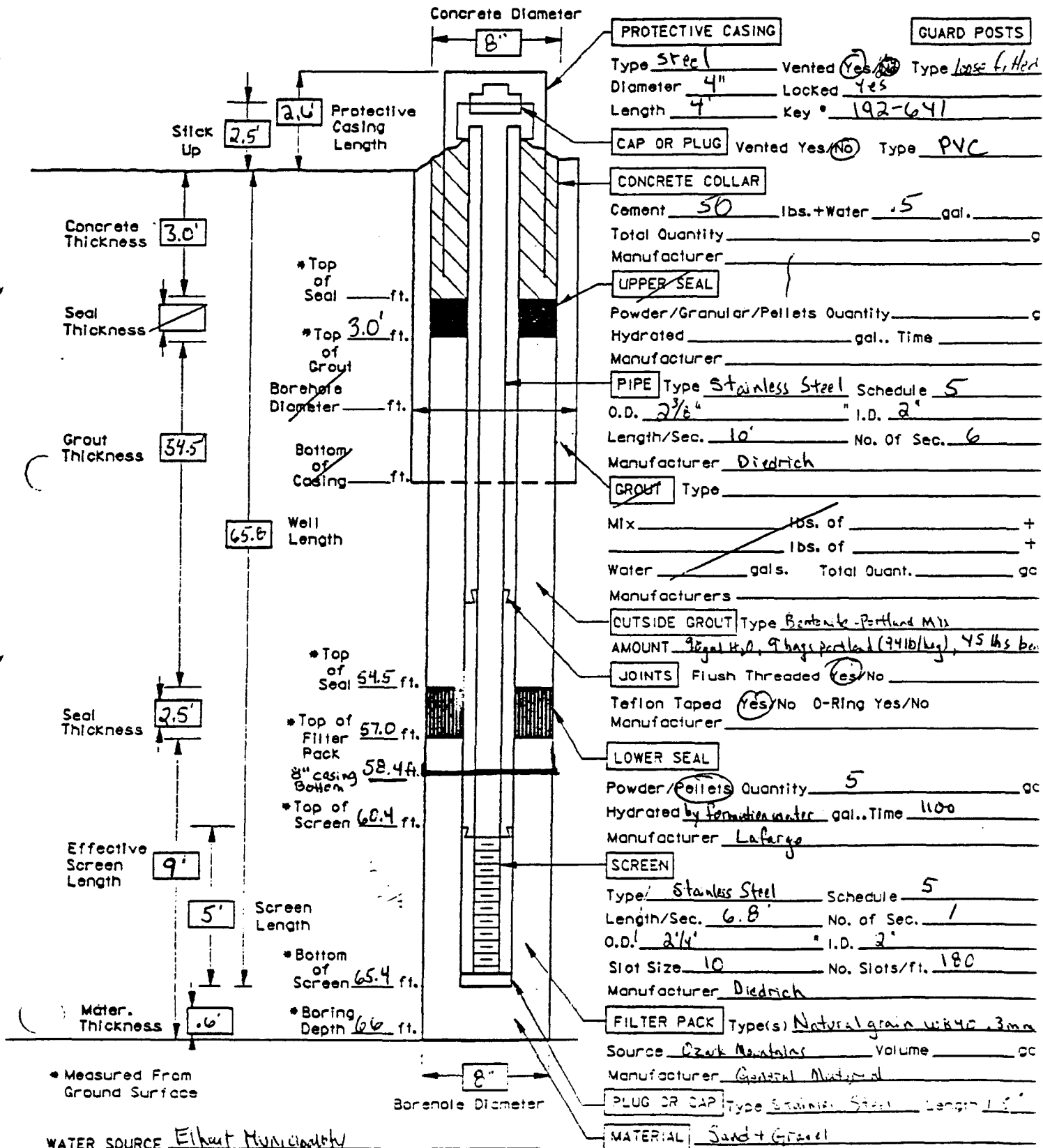
Donohue**DOUBLE CASING WELL/PIEZOMETER INSTALLATION DIAGRAM**

Form 104

Site: Himee DumpDate: 12/14/90Inspected By: Tom PuchalskiProject No. 20026.023Well No. P101BEngineers & Architects
COMPUTER AIDED DESIGN/DRAFTINGDriller/Contractor Max Tinnin Don Brexington / Mathes

Donohue**DOUBLE CASING WELL/PIEZOMETER INSTALLATION DIAGRAM**

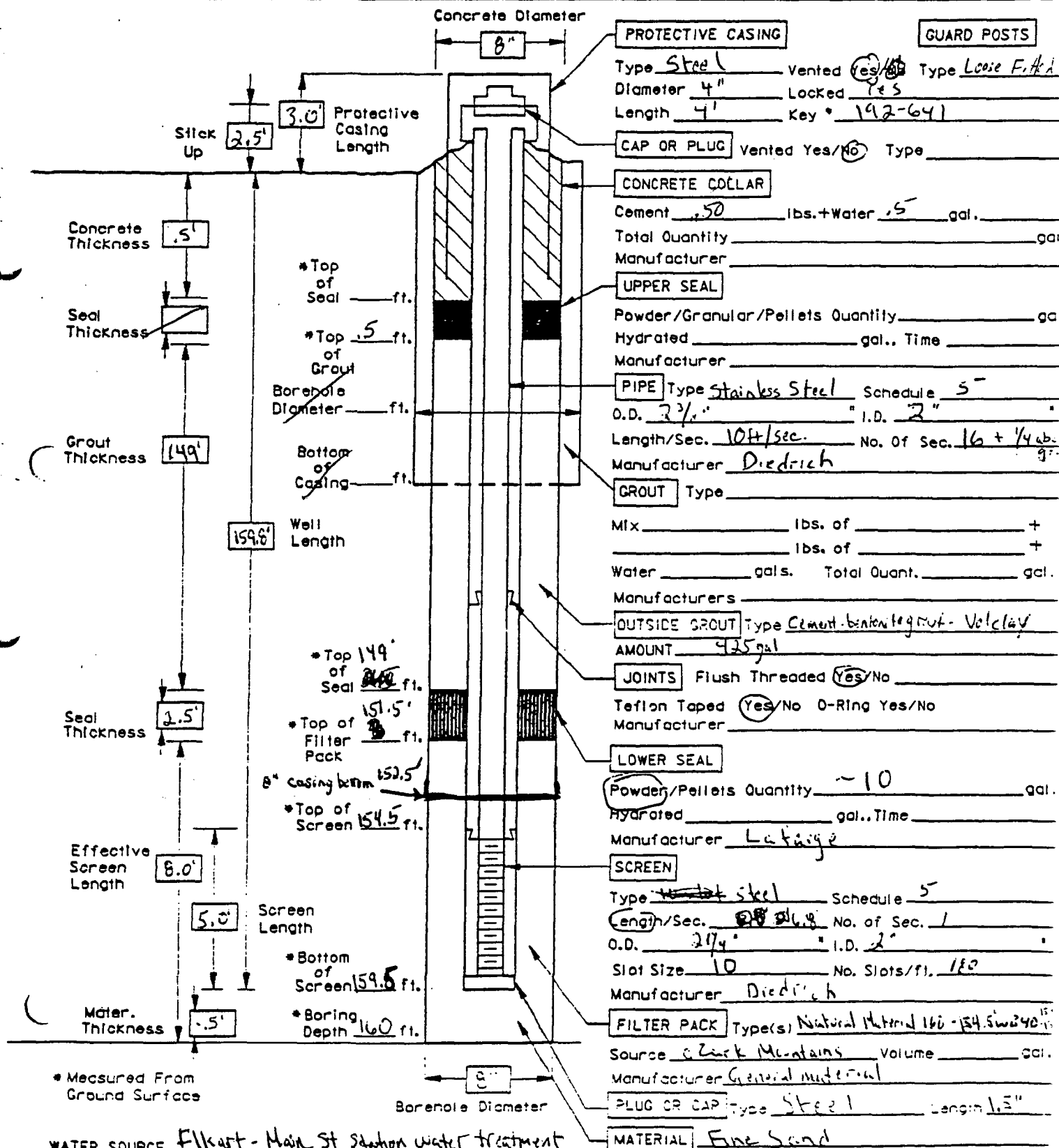
Form

Engineers & Architects
COMPUTER AIDED DESIGN/DRAFTINGSite: Himco DumpDate: 12/2/90Inspected By: S. PadavaniProject No. 20026Well No. P102BDriller/Contractor Max Tinnin/MedhesWATER SOURCE Elkhart Municipality

Donohue

DOUBLE CASING WELL/PIEZOMETER INSTALLATION DIAGRAM

Form 10

Site: Himco DumpDate: 12/1/90Inspected By: S. PaderaniProject No. 20026Well No. P102CEngineers & Architects
COMPUTER AIDED DESIGN/DRAFTINGDriller/Contractor Max Tinner / Mathes

Engineers & Architects

SOIL BORING NO.

SITE: Himco Dump PROJECT NO. 30030.033

PICIB

DRILLING METHOD: 7" Blade bit
Air rotary 8" drive casing

WATER LEVEL READINGS			
DATE	TIME	DEPTH	CASING

GROUND SURFACE ELEV.: _____
COORDINATES: _____

LOG BY: TOM PUCITA-LSKI

DRILLER: John Moynes & Max Tinnin

WEATHER: 30: Clearing up. Occ. Breeze to

PHYSICAL SETTING: Grass field

NORTH: _____

NORTH: _____

EAST: _____

DATE START: 12/13/90

DATE COMPLETE: _____

WELL INSTALLATION: _____

DEPTH IN FEET	SOIL DEPOSITIONAL ENVIRONMENT	USCS	SOIL DESCRIPTION AND DRILLING COMMENTS	SAMPLING DATA				AIR MONITORING					
				B	N	A	R	SAMPLE		TIME	PID	O ₂	CO
								TYPE	INTERVAL			LEL	U.S.
0		SM											
0		SH	10 YR 4/1 Dark Grey Medium Grained Silty Sandy, wet							1600	5	01.3	00.7
0		GP	Poorly graded Gravel 85% 1" dia. shaly, 100% black lignite, 30% organic dark grey sand, saturated							1645	0	01.3	00.7
0		SM	10 YR 4/1 Dark Grey Silty Sand, medium grained, saturated							1730	0	01.3	00.7
0		GW	Well graded GRAVEL 85% 1/2-3" sand & shaly, sil. 15% medium grained sand 10 YR 2/1 Grey SILTY SAND 60% fine gr. sand, 40% SILT wet							1109	0	01.3	00.7
0		SH											
0		SM	10 YR 5/2 Brownish Brown SILTY SAND 70% fine gr. sand 30% SILT, saturated							1320	0	01.3	00.7
This is an approximate log based upon cuttings blown out of the boring during air rotary drilling.													

Donohue

BORING LOG

SOIL BORING NO.

Engineers & Architects
COMPUTER AIDED DESIGN/DRAFTINGSITE: Himco Dump PROJECT NO. 20026

(P1020)

DRILLING METHOD: Air Rotary

WATER LEVEL READINGS

DATE TIME DEPTH CASING

GROUND SURFACE ELEV.: _____

COORDINATES: _____

NORTH: _____

EAST: _____

LOG BY: S. PadovaniDRILLER: Max Turner - MathosWEATHER: Cold

PHYSICAL SETTING: _____

DATE START: 11/24/90DATE COMPLETE: 11/30/90WELL INSTALLATION: 11/30/90

DEPTH IN FEET	SOIL DEPOSITIONAL ENVIRONMENT	USCS	SOIL DESCRIPTION AND DRILLING COMMENTS	SAMPLING DATA				AIR MONITORING				
				B	N	A	R	SAMPLE		TIME	PIO	O ₂ LEL
								TYPE	INTERVAL			
10			Brown medium to coarse grained sand with gravel						1440	.2	20.8/0	
20			Poorly sorted grey sand + Gravel						1530	.2	20.8/2	
30												
40			Poorly sorted sand + Gravel						1615	-	20.7/3	
50												
60			Poorly sorted sand w/ Gravel						1740	.2	21.0/3	
70			medium grained sand w/ clay chunks									
80			fine Silty fine grained sand									
90			Sandy silt									
100			Sandy silt / silt						1000	.2	21.0/0	
110			Silty clay / clay <u>DRY!!!</u>									
120			Clay (tight)						1130	.2	21.0/0	
130			Brownish well sorted medium grained sand. Some Trace gravel pieces to 1 1/2"									
140			Brownish well sorted fine grained Sand						1230	.2	21.0/0	
150			VERY TIGHT FORMATION - Not much water									
160		Takes 1 1/4 hours to bring 30 feet							0	0	0	
170			BEING DRILLING									

Donohue

BORING LOG

SOIL BORING NO.

Engineers & Architects
COMPUTER AIDED DESIGN/DRAFTING

SITE: Hanco Dump PROJECT NO. 20026

91022

DRILLING METHOD: Rotary

WATER LEVEL READINGS

GROUND SURFACE ELEV.: _____

DATE _____ TIME _____ DEPTH _____ CASING _____

COORDINATES: _____

NORTH: _____

EAST: _____

LOG BY: S. Padovani

DRILLER: Max Tien - Mathes

WEATHER: Cold

PHYSICAL SETTING: _____

DATE START: 11/24/90

DATE COMPLETE: 11/30/90

WELL INSTALLATION: 11/30/90

DEPTH IN FEET	SOIL DEPOSITIONAL ENVIRONMENT	USCS	SOIL DESCRIPTION AND DRILLING COMMENTS	SAMPLING DATA				AIR MONITORING		
				B	N	A	R	TIME	PIO	O ₂ / LEL
150			Brownish well sorted fine <u>fine</u> ground sand ↓ Tight!!! Very little water					1500	.2	20.8%
160			Pounding the casing has become futile - Tom P., the drillers, and I agreed to set well screen at this depth							
170			COMMENTS: 8" steel casing Down to 152.5'							
			: These soil descriptions and depths are approximate!							
			BLIND DRILLING							
			* 500 gallons of water put down well to hold formation back at 160'. However, most of this water exits out of the top of the 8" casing and does not enter the formation. G.P. 12/16/90							

SOIL BORING NO.

Engineers & Architects

SITE: Himco Dump PROJECT NO. 20026

9102B

DRILLING METHOD: Air rotary w/
2" casing driver

[illegible]

GROUND SURFACE ELEV.: _____

COORDINATES: _____

NORTH: _____

EAST: _____

LOG BY: S. Padayachi

DRILLER: Max Thron

WEATHER: Cloudy, Cool 40°F

PHYSICAL SETTING: _____ WELL INSTALLATION: 12/1/90

DATE START: 11/30/40

DATE COMPLETE: 12/1/40

WELL INSTALLATION: 12/1/90

[illegible]

Engineers & Architects

SOIL BORING NO.

SITE: Hime Damp PROJECT NO. 22026.023

Pratic

WEATHER: Clear 40s SE wind 10-15 mph

NUMBER OF OFFERS 6 per Call

DATE COMPLETE: 12/14/90
WELL INSTALLATION: 2/10/90

[illegible]

TECHNICAL MEMORANDUM - NO. 2

ORIGINAL

DATE: January 23, 1991
TO: Vanessa Harris - Site Manager
CC: Marcia Kuehl - RI Lead
Roman Gau - Project Manager
Mike Crosser - TSQAM
FROM: Tom Puchalski
SUBJECT: EPA ARCS Region V Contract No. 68-W8-0093
EPA Work Assignment No. 175L4J
Donohue Project No. 20026.024
Himco Dump

WELL DEVELOPMENT

Introduction

All newly installed groundwater monitoring wells at the Himco Dump site in Elkhart, Indiana, were developed a minimum of 24 hours after their installation. Water table wells were developed on November 13 and 14, 1990, and piezometers were developed December 15 and 16, 1990. Developed water table wells include WT101A, WT102A, WT103A, WT104A, WT105A, and WT106A. Developed piezometers include P101B, P101C, P102B, and P102C. The locations of these wells are provided in Figure 1 of this memorandum. Water table wells were developed by John Mathes & Associates, Inc., and Eric Slusser of Donohue & Associates, Inc. Piezometers were developed by Max Tinnin and Don Brewington of John Mathes & Associates, Inc., and Tom Puchalski of Donohue & Associates, Inc. Wells were developed to remove sediment from the well and to allow the maximum amount of groundwater to enter the well for groundwater sampling. Well development helps assure that a representative groundwater sample is obtained.

Methods

Well development was carried out as specified in the Final Field Sampling Plan, Himco Dump Remedial Investigation/Feasibility Study Elkhart, Indiana, Section 4.2.2.3.

The development method for water table wells was different from the development method for piezometers. Water table wells were pumped by hand using a Brainard Killman hand pump.

Piezometers were developed using compressed air provided by the TH60 drill rig. An air purging device developed by John Mathes & Associates, Inc., was used. This device consists of a compressed air line attached to a tube directed down into the well which takes an 180-degree bend upward into the base of a 1-1/2-inch I.D. plastic water hose. The air lifts the sand and water up through the plastic hose. This method was used for these deep

wells because a high volume of water and sand was required to be removed in a short amount of time.

Pumps with sufficient pumping rates are not available for 2-inch wells. The air developer served to remove the sand from the well and purge the groundwater in a reasonable amount of time.

Pumping of the well continued until at least five well volumes were removed and the purge water was silt free, the water temperature was stabilized to $\pm 0.5^{\circ}\text{C}$, pH was stabilized to ± 0.1 units, and conductivity was stabilized to ± 10 percent.

Measurements of pH, conductivity, color, temperature, and turbidity were recorded at least once after each of the five well volumes were purged.

Deviations

High pressure hot water washing of the Brainard Killman hand pump and the air development pump was used for decontamination between wells instead of soap and water, isopropanol, and deionized water as was described in Section 4.2.2.4 of the sampling plan. The lengths of PVC connections and lengths of the exit hose and air compressor hose were not easily cleaned by hand. The high pressure hot water wash provided a quicker and more thorough method of decontamination for this equipment.

The sampling plan specified using a submersible pump for well development. The air development device used by Mathes for the development of the piezometers was used in place of a submersible pump. No submersible pump is available which could pump out the sand and purge the groundwater as quickly from a 2-inch well as did the air development tool.

Summary of Results

Copies of completed field forms are provided in Appendix A. The development methods successfully cleared the sand and silt from the installed groundwater monitoring wells and removed the required purge volumes so that a representative groundwater sample could be collected after the wells had stabilized for a minimum of two weeks. All groundwater wells provided sufficient groundwater volume to conduct groundwater sampling.

TP/ds

A/R/HIMCO/AA9

APPENDIX A
WELL DEVELOPMENT DATA

Well Development

Project No. 20026.023 Site Hines Dune

Method of Development Pumped X Bailed _____ Blown _____ Surge Block _____

Equipment _____ Airlift _____ N2 Lift _____ In. Bailer _____ Length 5 Ft. Material _____

Pump PVC Manufacturer Bransid Kilmer Diameter 1 1/4" x 10 5' section

Description of site (weather, temp, soil conditions) Cool, sunny mid 40s

[illegible]

Additional Notes: 2" well $\pi r^2 = 7.4 \text{ y} = 0.163$ $WC = 9.09$ $9.09 \times 0.163 = 1.48$

8" sand pack $2.611 \times 9.05 = 23.73 \times .3 = 7.12$

7.12 - 1.48 = 5.64 Sand pack 3'6" - 2" well

 ~~$5.64 + 1.48 = 7.12$ with vol gal~~~~7.44~~ $1.41 + 6.69 = 8.10$ | well vol

22.25

Entered on computer

Signature

Date 11/14/80

Donohue

Well Development

Engineers & Architects

Project No. 20026.023 Site Himesa Dump

Method of Development Pumped X Bailed _____ Blown _____ Surge Block _____

Equipment _____ Airlift _____ N2 Lift _____ In. Bailer 1 1/4" Length 5 Ft. Material _____

Pump PVC Manufacturer Bramid Kilmer Diameter 1 1/4" 10 5' section

Description of site (weather, temp, soil conditions) Warmer Sunny 40's - 46°

[illegible]

Additional Notes: $W = H_2O$ 2" well .163 8" 2.661

W. W. W. W. W.

$W = 8.32$

$$S = \boxed{6.18} [(4 \times 13) - 11] \times .3$$

H height of Col.

$$T = W + 5$$

D. ~~duen~~. bo. ehole dize.

$$2'' \text{ HX D} = 163 \times 8.32 = 1.36 \text{ | wall vol - 2'' pin}$$

r total vol of well

$$q^* = \left[\frac{(2611 \times 2.34) - (1.34)}{21.72 - 1.34} \right] \times 3 = \text{Sand pack}$$

+ Sand pack.

$$\boxed{20.36} \gamma.3 = 6.11 + 1.36 = 7.47 = 1 \text{ well v.l.}$$

B. Buchle d. n.

Entered on computer

Signature

but will find

Date / /

524

As noted above,

Donohue

Well Development

Engineers & Architects

Project No. 20026.023 Site Himco Dux

Method of Development Pumped X Bailed _____ Blown _____ Surge Block _____

Equipment _____ **Airlift** _____ **N2 Lift** _____ **In. Bailer** _____ **Length** _____ **Ft. Material** _____

Pump PVC Manufacturer Brainerd k.l.m. Diameter 1 1/4" 5' section

Description of site (weather, temp, soil conditions) Wet Sunny 45°

11-13-97

set-r
4:50

5:06

مذہب

[illegible]

Additional Notes: $W = H D = 1.03$ 1" well $H = 6.32$ water col-mm

$$S = [(HyD) - W] \cdot 3 = [(2.611 \times 6.32) - 1.03] \cdot 3 =$$

$$T = 2 + 3$$

$$(16.50 - 1.03) \cdot 3$$

$$(15.47) \cdot 3 = 4.64 + 1.03 = 5.67 = 1 \text{ well val}$$

Entered on computer

Signature

E. D. Shu

Date 11 / 14 / 92

Donohue

Well Development

Engineers & Architects

Project No. 20026.023 Site Hine, Dyer

Method of Development Pumped X Bailed _____ Blown _____ Surge Block _____

Equipment	Airlift	N2 Lift	In. Bailer	Length	Ft. Material
------------------	----------------	----------------	-------------------	---------------	---------------------

Pump 1VC Manufacturer Brainerd Kilmer Diameter 1 1/4" 10 5' section

Description of site (weather, temp, soil conditions) Sunny Cool 40s

[illegible]

Additional Notes: 2" well .163 8" 2.611 H = 12.34 ft H = Water column
W = HD 0.163 x 12.34 = 2.01 gal. W 2" well volume
S = [(H x D) = W] 0.3 [(2.611 x 12.34) - (2.01) = (30.21) (.3) = 9.063 gal. S 8" well volume
T = W + S 32.22 9.063 T sand pack and well vol.

$$T = 9.06 \text{ bbl} + 2.01 = 11.07 \text{ gallons} = \text{1 well vol including sand pit and pipe}$$

Entered on computer

Signature

Date 11/14/90

Donohue

Well Development

Engineers & Architects

Project No. 20226.023 Site Hines Dump

Method of Development Pumped X Bailed _____ Blown _____ Surge Block _____

Equipment _____ Airlift _____ N2 Lift _____ In. Bailer 1 1/4" Length 5 Ft. Material _____

Pump AVC Manufacturer Bosch Rexroth Diameter 1 1/4" ID

Description of site (weather, temp, soil conditions) Cool sunny 40s - 50s by noon

[illegible]

Additional Notes: 2" .163 8" 2.611

' H = height of water = 7.11 ft

$$W = H_0 = .163 \times 7.1 = 1.16$$

S sand pack vol.

~~3 books done~~

$$S = [(H \times B) - W] \cdot .3 = [18.56 - 1.16] \cdot .3 = 5.22 \text{ m}$$

Well Volume

total well & sand prod = $W+S = 5.22 + 1.16 = 6.38 \text{ gal}$

T Sand pocket and well

Entered on computer

Signature

E. D. Allen

Date 11/14/90

Donohue

Well Development

Engineers & Architects

Project No. 20026.023 Site Hinco Dump

Method of Development Pumped X Bailed _____ Blown _____ Surge Block _____

Equipment _____ Airlift _____ N2 Lift _____ In. Bailer _____ Length _____ Ft. Material _____

Pump PVC Manufacturer Barnard Kilman Diameter 1 1/4" ID 5' sec.

Description of site (weather, temp, soil conditions) Cloudy, sunny, low 50's

[illegible]

Additional Notes: 2" 0.163 5' 2.611

$$i = 7.19\%$$
$$H = \frac{\text{thick}}{\text{thin}} \text{ of water column}$$

$$W = H \times D = .163 \times 7.19 = 1.17$$

$S = 5^{\text{th}}$ pack volume.

$$S = \sqrt{(1 + \frac{1}{B}) = 1.3} = (18.77 - 1.17) \cdot 3 = (17.60) \cdot 3 = 5.28$$

~~Do~~ - diaries ~~be~~ well

$$\underline{T = W + S \quad 5.28 + 1.17 = 6.45 \text{ gal.} - 1 \text{ well vol}$$

B diameter burrhole

well known

T- Sand rock and well

Entered on computer

Signature

Ein 2. An

Date 11 / 14 / 97

Donohue

Well Development 12/15/96

Engineers & Architects

Project No. 20026.033 Site Himco Dump

Method of Development Pumped ✓ Bailed _____ Blown _____ Surge Block _____

Equipment ✓ Airlift ~~W~~ N2 Lift In. Bailer Length 100 Ft. Material ASTM D2233 Plastic

Pump	Air rig	Manufacturer	Natco	Diameter	3/4"	Exit Hose
------	---------	--------------	-------	----------	------	-----------

Description of site (weather, temp, soil conditions) 44°F, south wind 10-15 mph, partly sunny, wet soil

[illegible]

Additional Notes: Initial air surge blew sand from screen

Entered on computer _____ Signature _____ Date ____ / ____ / ____

Donohue

Well Development 12/15/90

Engineers & Architects

Project No. 20026.003 Site Himeo Dump

Method of Development Pumped ✓ Bailed _____ Blown _____ Surge Block _____

Equipment ✓ Airlift ✓ N2 Lift In. Bailer Length 100 Ft. Material ASTM D3233

Pump ^{Air supplied} by rig Manufacturer Mathes Diameter 3/4" crit hose ^{Plastic Hose}

Description of site (weather, temp, soil conditions) 43°F, south wind 14 mph, partly sunny, soil wet

[illegible]

Additional Notes: Initial air surge blew sand from screen.

Entered on computer _____ Signature _____ Date ____ / ____ / ____

Donohue

Well Development 12/15/90

Engineers & Architects

Project No. 20076.023 Site Himco Dump

Method of Development Pumped ☒ Bailed ☐ Blown ☐ Surge Block ☐

Equipment ☒ Airlift _____ N2 Lift _____ In. Bailer _____ Length 100 Ft. Material Plastic Exit Hose

Pump Air Rig Manufacturer Mathes Diameter 3/4"

Description of site (weather, temp, soil conditions) 40°F, south wind 10-20 mph, overcast, wet soil

[illegible]

Additional Notes: Initial air surge blew sand from screen

Entered on computer _____ Signature _____ Date ____ / ____ / ____

Donohue

Well Development 12/16/90

Engineers & Architects

Project No. 20026.023 Site Himco Dump

Method of Development Pumped ☒ Bailed ☐ Blown ☐ Surge Block ☐

Equipment ☒ Airlift _____ N2 Lift _____ In. Bailer _____ Length 100 Ft. Material Plastic Exit Hose

Pump Air Rig Source Manufacturer Mathes devised pump Diameter 3/4"

TH60 Ingersol Rand
Description of site (weather, temp, soil conditions) 40°F, calm, overcast, foggy, drizzle, wet soil

[illegible]

Additional Notes: Initial air surge blew sand out of screen.

ORIGINAL

TECHNICAL MEMORANDUM - NO. 3

DATE: January 21, 1991

TO: Vanessa Harris, Site Manager

CC: Marcia Kuehl, RI Lead
Roman Gau, Project Manager
Mike Crosser, TSQAM

FROM: Tom Puchalski

SUBJECT: EPA ARCS Region V Contract No. 68-W8-0093
EPA Work Assignment No. 175L4J
Donohue Project No. 20026.024
Himco Dump

STAFF GAUGES

Introduction

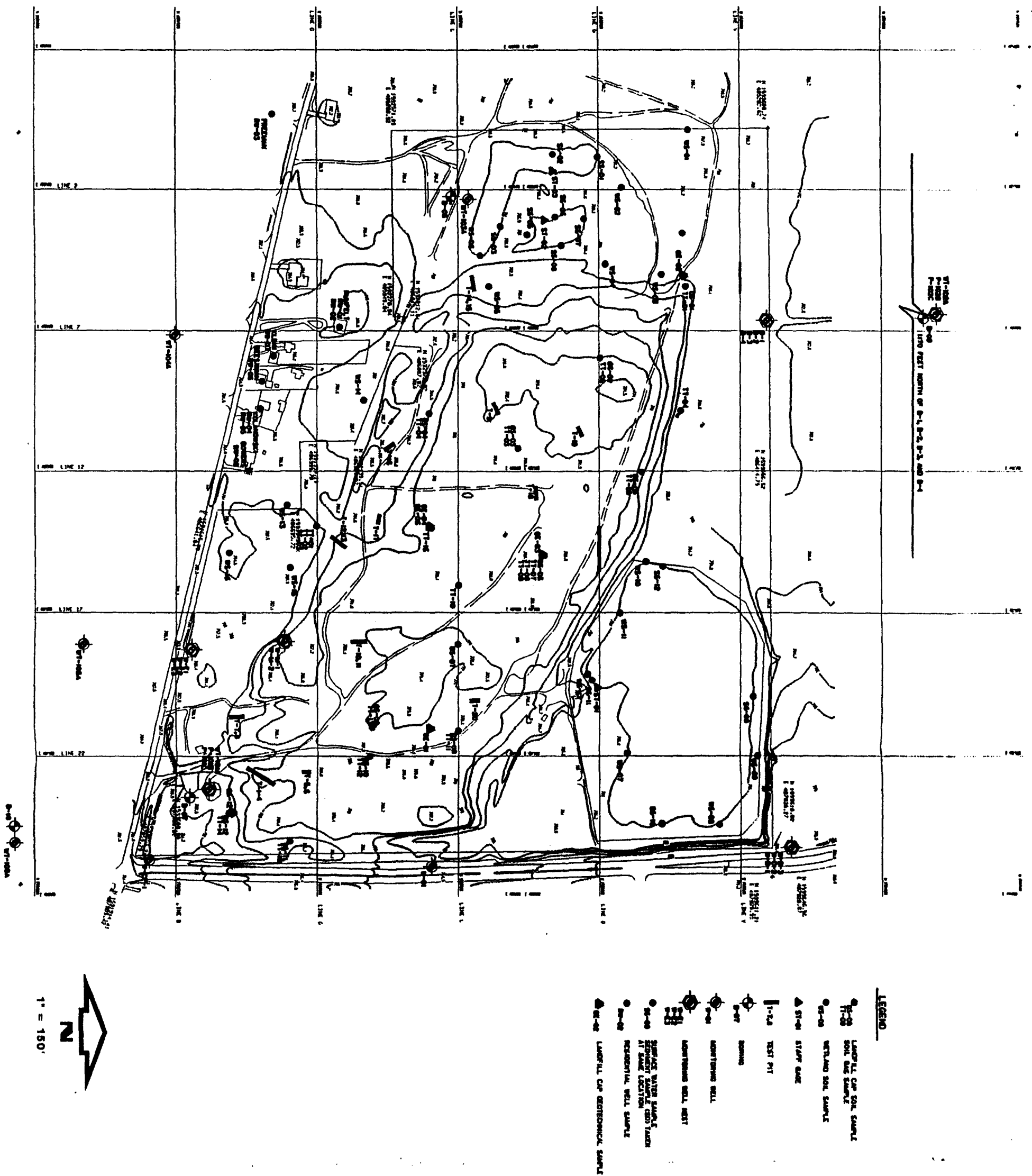
Three staff gauges were installed at the Himco Dump Site; one was installed in the gravel pit pond at the northeast area of the site, one was installed at the "L"-shaped fish pond at the southwest corner of the site, and one was installed at the smallest pond on-site located east of the "L"-shaped fish pond (Figure 1). The posts for anchoring the gauges were installed on October 24, 1990, by Eric Slusser and Tom Puchalski of Donohue & Associates, Inc. The gauges were installed onto the posts by Anya Kirykiewicz and Steve Spiewak on December 14, 1990.

The staff gauges were installed in order to gather surface water elevation data. The measurements were taken on the same days as groundwater elevations from monitoring wells so that interconnection of groundwater and surface water can be evaluated.

Methods

The installation of staff gauges proceeded as described in Section 4.3 Surface Water Hydraulic Monitoring of the Final Field Sampling Plan, Himco Dump RI/FS, Elkhart, IN. The actual material used for the anchor posts for staff gauges deviated from what was described in the sampling plan. Two-inch I.D. electrical conduit in 8- or 10-foot lengths were used in place of the coupled galvanized steel described in the plan.

Anchor posts were driven into the bottom sediments of the ponds with a post driver. Hip waders were used to allow the installation in water approximately 2 feet deep about 3 to 5 feet from the shoreline. About 4 feet of the posts remained above water after driving in-place to allow the attachment of a sheet metal rule marked to 0.01-foot.



MAY 1991

FIGURE 1 SITE LOCATION MAP (TECHNICAL MEMO)

**HIMCO DUMP
SUPERFUND SITE
ELKHART, INDIANA**

20028

Donohue ENGINEERS
ARCHITECTS
SCIENTISTS

The sheet metal rules were attached to the anchor posts by bolts which pass through the rule and into the posts. Holes were drilled in the posts to accommodate the bolts by using an electric drill at each staff gauge location. A gasoline powered electric generator was used to power the drill. The sheet metal rules were anchored with the top of the rule flush with the top of the anchor post. The elevations of the tops of the anchor posts were surveyed by Lang Feeney of South Bend, Indiana, on December 16, 1990.

Deviations

The locations deviate slightly from those shown in Figure 4-1 of the sampling plan. While the ponds shown in Figure 4-1 all have gauges installed, Figure 1 of this memorandum more accurately locates the actual staff gauge locations within each pond. The locations were modified to account for shoreline and bottom sediment conditions which were most favorable for the staff gauge installations. The conditions include consolidated bottom sediments, which provide a sturdy anchoring of the post, and the absence of shoreline brush which makes accessing and reading the gauges difficult.

Summary of Results

A table of the observed surface water levels and groundwater monitoring well water level elevations are included in Appendix A. Measurements of the level of ice during months when the surface water was frozen do not accurately reflect the free water surface elevation and should not be used to evaluate surface water to groundwater connection.

TP/ke

A/R/HIMCO/AA6

APPENDIX A
WATER LEVEL MEASUREMENTS AND ELEVATIONS

DONOHUE

WATER ELEVATION

Feb. 1, 1991

PROJECT NO. 20026

SITE Himco Dump

WELL NUMBER	ELEVATION OF TOP OF PIPE	DEPTH TO WATER	WATER ELEVATION	DEPTH TO BOTTOM	WELL INTEGRITY				COMMENTS
					LOCKED	CAPPED	CRACKED	OBSTRUCT	
B-1		6.25			X	X			1052 No protective casing
B-2		6.15		13.88		X			1055
B-3		7.44		130.34	X	X			1059
B-4		6.45		175.16	X	X			1110
CP-1		3.82		20.19		X			1013 2/2/91 No protective casing
E-2		9.82		16.54		X			1612
E-3		11.11		175.65	X	X			1614
F-1		2.67		31.28		X			1755
F-2		14.08		147.83	X	X			1438
F-3		16.98			X	X			1453
G-1		12.48		52.02	X	X			1413
G-3		22.08		169.89	X	X			1424
I-1		9.48		172.97	X	X			1540
I-2		8.78		15.67		X			1544
I-3		9.14		32.15	X	X			1872
J-1		12.03		43.64	X	X			1514
J-2		10.29		17.81		X	X		1524 2/2/91 SP 2/2/91
J-3		18.63		153.39	X	X			1520
M-1		15.61		103.24		X			10452 2/6/1
M-2		14.84		24.76		X			1050
N-1		8.81		24.22		X			0947 Flush
O-1		5.0		23.47		X			1820
O-1		8.34		29.77		X			0921
WT101A		9.96		18.70	X	X			1145
PI01B		9.89		100.47	X	X			1152
PI01C		9.78		106.53	X	X			1159
WT106A		2.87		18.50	X	X			1558
WT105A		9.0		18.56	X	X			1625
WT104A		18.75		18.69	X	X			1635
WT103A		5.28		18.47	X	X			1001 2/2/91
WT102A		10.17		18.18	X	X			0851 2/2/91

DESCRIPTION OF SITE

F 1 16.17 DTW = 11.38 NTR = 71.75

SOIL CONDITIONS

O-1: Flush w/ground water = me for rever to side casing filler

WEATHER

hion, ice, water cap no snow on

TEMPERATURE

ENTERED ON COMPUTER

SIGNATURE

DATE

WATER ELEVATION

PROJECT NO. 10026 SITE Himec Dump

[illegible]

DESCRIPTION OF SITE _____

SOIL CONDITIONS _____

WEATHER _____ TEMPERATURE _____

ENTERED ON COMPUTER _____ SIGNATURE _____ DATE _____

DONOHUE

WATER ELEVATION

PROJECT NO. 20026

SITE HIMCO DUMP - INITIAL WELL INVENTORY

WELL NUMBER	ELEVATION OF TOP OF PIPE	DEPTH TO WATER	WATER ELEVATION	DEPTH TO BOTTOM	WELL INTEGRITY				COMMENTS
					LOCKED	CAPPED	CRACKED	CONSTRUCT	
E-1	72.11	12.15'		91.38'	X	X			11/6/90 - 1st water level and 1st water well
E-2		11.62'		11.93'		X			11/6/90 - 1st water level and 1st water well
E-3		12.99'		115.52'	X	X			11/6/90 - 5' 2" ID
N-1		9.55'		22.25'		X			11/6/90 - NOT LOCATED
B-4		11.55'		175.12'	X	X			11/6/90 - NO PROTECTIVE CASING, TURNING EAST
B-3		7.34'		130.23'	X	X			11/6/90 - NO PROTECTIVE CASING, 5" ID
B-2		6.04'		12.91'		X			11/6/90 - NO PROTECTIVE CASING, 2" ID
B-1		11.33'			X	X			11/6/90 - NO PROTECTIVE CASING, 2" ID
CP-1	UNABLE TO OPEN					X			11/6/90 - NO PROTECTIVE CASING, 2" ID
11-1		10.12'		103.34'		X			11/6/90 - 1st water level and 1st water well
11-2		16.35'		21.27'		X			11/6/90 - 1st water level and 1st water well
L-1		12.58'		62.53'	X	X			11/6/90 - NO PROTECTIVE CASING, VENTED 5" ID, SILTY
L-2		10.46'		186.0'	X	X			11/6/90 - NO PROTECTIVE CASING, VENTED 5" ID, SILTY
L-4		11.73'		19.91'		X			11/6/90 - NO PROTECTIVE CASING, 2" ID, 12" PLUGGED
I-3		9.28'		22.20'	X	X			11/6/90 - NO PROTECTIVE CASING, VENTED CAP 5" ID, CASING
I-1		10.67'		172.82'	X	X			11/6/90 - NO PROTECTIVE CASING, VENTED CAP, 5" ID, CASING
I-2		9.05'		15.64'	NO	X			11/6/90 - NO PROTECTIVE CASING, VENTED CAP, 2" ID, PVC
Q-1		5.87'		23.69'	NO	X			11/6/90 - UNLOCKED FLUSH MOUNT WELL BOX NEXT TO HYDRANT, RECORDS FROM PAIN
J-1		11.65'		42.70'	X	X	X		11/6/90 - NO PROTECTIVE CASING, VENTED CAP, 5" ID, PVC
J-3		22.18'		153.62'	X	X			" "
J-2		9.76'		17.80'	NO	X			11/6/90 - UNLOCKED, 2" ID PVC WELL VENTED CAP
F-2		17.06'		147.85'	X	X			11/6/90 - NO PROTECTIVE CASING, VENTED CAP, 5" ID, PVC
F-3		20.34'		180.20'	X	X			" "
F-1		9.5'		31.25'	NO	X			11/6/90 - NO PROTECTOR, VENTED CAP, 5" ID, PVC
G-1		13.75'		46.87'	X	X			11/6/90 - NO PROTECTOR, VENTED CAP, 5" ID, PVC CASING
G-3		27.68'		—	X	X			" " UNABLE TO LOCATE TOTAL DEPTH
P-1		8.90'		25.24'	NO	NO			11/6/90 - FLUSH MOUNT WELL BOX, WELL 2" ID AT AN ANGLE
O-1		10.19'		29.77'	X	X			11/6/90 - FLUSH MOUNT WELL BOX, WELL 2" ID PVC

DESCRIPTION OF SITE

SOIL CONDITIONS

WEATHER

TEMPERATURE

ENTERED ON COMPUTER

SIGNATURE

DATE

TECHNICAL MEMORANDUM - NO. 4

ORIGINAL

DATE: January 22, 1991

TO: Vanessa Harris, Site Manager

CC: Marcia Kuehl, RI Lead
Roman Gau, Project Manager
Mike Crosser, TSQAM

FROM: Tom Puchalski

SUBJECT: EPA ARCS Region V Contract No. 68-W8-0093
EPA Work Assignment No. 17-5L4J
Donohue Project No. 20026.024
Himco Dump RI/FS

GEOTECH BORINGS

Introduction

Four deep (175-foot) geotech borings were drilled and sampled as described in Exhibit A, Field Sampling Plan Addendum to Volume 2, Field Sampling Plan, Himco Dump Remedial Investigation/Feasibility Study, Elkhart, Indiana. Drilling activities for these borings began on December 17, 1990, and were completed January 9, 1991. These four borings were completed to investigate the site stratigraphy and to collect samples for geotechnical analysis at the Himco Dump Site, Elkhart, Indiana. The boring locations are provided in Figure 1 of this memorandum. Drilling and sampling activities were completed by Max Tinnin and Don Brewington of John Mathes and Associates, Inc. (Columbia, Illinois) with a TH60, Ingersol Rand air/mud rotary rig. Tom Puchalski of Donohue & Associates, Inc., inspected the drilling and sampling, completed time logs, logged all samples, collected select samples for geotechnical analysis, and performed air monitoring using a photoionization detector and gaspender.

Methods

Drilling and sampling were performed as described in Exhibit A, Field Sampling Plan Addendum to Volume 2, Field Sampling Plan, Himco Dump Remedial Investigation/Feasibility Study, Elkhart, Indiana, Section 4.2.

Each geotech boring began with using air rotary and a 7-7/8-inch tricone bit. The boring was blind-drilled to 18 feet. Eight-inch casing was then pounded down into the borehole to 8 or 9 feet. The 8-inch steel casing was then temporarily sealed in-place using granular bentonite. A 3-foot diameter steel casing was installed at the surface with a 6-inch diameter PVC tube extending to a 500-gallon mud tub. After the drilling mud was mixed in the tub, mud rotary drilling began. A 5-7/8-inch blade bit was used for the remainder of Borings 7, 8, and 9. Once this bit was worn out, a 7-7/8-inch blade bit replacement was used to drill Boring 10. Split-spoon sampling was accomplished with a 2-inch O.D., 2-foot long split-spoon sampler passed down through the inside of the drill stem. The split-spoon sampler was driven by a 140-pound down-hole hammer which was operated by a winch at the surface.

The Donohue geologist performed atmospheric monitoring at 5-foot intervals using a photoionization detector and gaspender. The geologist also logged all the samples using the Unified Soil Classification System (U.S.C.S.) based on visual inspection. A Munsell Color Chart was used to describe all soil colors.

The borings were drilled to the following depths: BRG-7, 174.5 feet; BRG-8, 166 feet; BRG-9, 173.5 feet; and BRG-10, 174 feet.

All borings were abandoned by backfilling with cement/bentonite grout emplaced by tremie pipe.

Deviations

The sampling plan specified using a 3-7/8-inch bit, however, either a 5-7/8 or 7-7/8-inch bit was used. The larger bits were required because split-spoon sampling was performed through the inside of the blade bit. Using a larger bit had no effect on the sampling of geotechnical borings.

Although several attempts were made to push shelly tubes, none were successful.

Boring 8 was finished at 166 feet instead of 175 feet because a till aquitard greater than 4 feet thick was encountered. In order to avoid passing through this aquitard at this downgradient location, the hole was stopped after two split-spoons sampled the unit.

Summary of Results

Boring logs, including atmospheric monitoring results, are provided in Appendix A.

Of the 20 geotechnical and 20 TOC samples sent to the laboratory, 15 geotechnical and 15 TOC samples were collected from the four deep geotech borings. Although three shelly tube samples were also designated to be collected from these four borings, attempts to retrieve these samples were unsuccessful.

Several complications caused delays in the drilling schedule. Some of the difficulties were weather-related. The operation of the drill rig was dependent upon the air system being free of water. Condensation would generally build up overnight which caused pressure losses in the air system. Isopropanol dripped into the lines would eventually clear up this problem. Mud or water freezing in the circulation hoses or in the mud pump also caused delays in the morning while a propane torch was used to thaw frozen parts.

One day of drilling was lost to an equipment failure. One of the main hydraulic hoses ruptured on the drill rig requiring replacement.

TP/ds

A/R/HIMCO/AA7

APPENDIX A
BORING LOGS

Donohue

BORING LOG

SOIL BORING NO.

Engineers & Architects
COMPUTER AIDED DESIGN/DRAFTING

SITE: HIMCO DUMP PROJECT NO. 20026.023

BRG-07

DRILLING METHOD: 5 1/8" bit
mud rotary, down hole 140lb
hammer on 2" split spoon

WATER LEVEL READINGS
DATE TIME DEPTH CASING

GROUND SURFACE ELEV.: _____

COORDINATES: _____

NORTH: _____

EAST: _____

LOG BY: TOM PUCHALSKI

DRILLER: MAX TINNIN - MATHES

WEATHER: South wind 15 mph, overcast

Flat grass field
PHYSICAL SETTING: _____

DATE START: 12/16/90

DATE COMPLETE: 12/18/90

WELL INSTALLATION: NONE

DEPTH IN FEET	SOIL DEPOSITIONAL ENVIRONMENT	USCS	SOIL DESCRIPTION AND DRILLING COMMENTS	SAMPLING DATA				AIR MONITORING					
				B	N	A	R	SAMPLE TYPE INTERVAL		TIME	PID	O ₂ LEL	CO H ₂ S
32													
34	GM		10YR 5/1 GRAY SILTY GRAVEL, 70% > 2" dia grl, 20% co-md snd, 10% silt, saturated OUTWASH	30				3'55	33-35	838	0	21.2 0.07	0
36													
38	GM		10YR 5/1 Gray SILTY GRAVEL, 85% 1/2 - 2" dia gravel-sbrd, 20% co-md snd, 10% silt, sat OUTWASH	15				2'55	38-40	848	0	21.2 0.07	0
40													
42													
44	GM		POOR RECOVERY, 1/4 - 1/2" sbrd grl, some > 2" 10% silty sand OUTWASH	14				2'55	43-45	858	0	21.2 0.06	0
46			Begin losing mud at surface due to poor seal at 8" casing / soil inter face. Reseal with bentonite. Set up sand filter cone.							50 gallons mud lost down hole			
48	SP		10YR 5/1 Gray SAND, fine grained, sat OUTWASH	35				2'55	48-50	1059	0	21.2 0.07	0
50										GEO 48-49		GTO7-03	
52													
54	SP		10YR 5/1 Gray SAND, fn grn, sat, trace 1/2" dia sbrd grl, scattered throughout, saturated OUTWASH	33				2'55	53-55	1106 ↓	0	21.2 0.09	0
56													
58	GP		Poorly Graded GRAVEL, 3/4 - 1 inch diameter, most sbrd, some sbrd	24				2'55	58-60	1137	0	21.2 0.07	0

Donohue

BORING LOG

SOIL BORING NO.

Engineers & Architects

SITE: HIMCO DUMP PROJECT NO. 30036.033

BRG-C7

DRILLING METHOD: 3 1/2" tri-cone, blade

WATER LEVEL READINGS

GROUND SURFACE ELEV.: _____

mud rotary down hole 140 lb

DATE _____ TIME _____ DEPTH _____ CASING _____

COORDINATES:

hammer, 5" ss

NORTH: _____

LOG BY: TEP

EAST: _____

DRILLER: MT, DB - JMA

DATE START: 12/16/90

WEATHER: Southwind 15 mph, overcast

Flat grassy field.

DATE COMPLETE: 12/18/90

WELL INSTALLATION: NOPE

DEPTH IN FEET	SOIL DEPOSITIONAL ENVIRONMENT	USCS	SOIL DESCRIPTION AND DRILLING COMMENTS	SAMPLING DATA				AIR MONITORING					
				B	N	A	R	SAMPLE TYPE INTERVAL		TIME	PID	O ₂ LEL	CO H ₂ S
62													
64		SP	10YR 5/1 Gray SAND, fine grained, well sorted, saturated OUTWASH	30				3"SS	63-65	1145	0	0.3 C	0 C
66													
68		SP	10YR 6/2 Light Brownish Gray SAND, fine grn well sorted, saturated, one > 3" dia. cobble. OUTWASH	50				3"SS	68-70	1324	RAIN - Cont take air readings.		
70													
72			10YR 5/1 Gray SAND, well sorted, fine grained, saturated OUTWASH	40				3"SS	73-75	1334			
74		SP											
76													
78		SP	10YR 5/1 Gray SAND, fine grained, trace 1/4" silty clay clasts 10YR 6/1 Light gray, saturated OUTWASH	54				3"SS	78-80	1346			
80													
82													
84		SM	10YR 5/1 Gray SILTY SAND, fine grn, trace 1/4" silty clay 10YR 6/1 Lt gray, sat 20% silt OUTWASH	61				3"SS	83-85	1352			
86													
88		SM	AS ABOVE + 1 > 3" dia. cobble broken in spoon	48				3"SS	88-90	1414			
90													

SOIL BORING NO.

Engineers & Architects

SITE: HUNCO DUMP PROJECT NO. 30036.033

BRG 07

DRILLING METHOD: 5 7/8" bit blake WATER LEVEL READINGS

GROUND SURFACE ELEV.: _____

mud rotary, down hole 140 lb
hammer, 2" ss

DATE	TIME	DEPTH	CASING
------	------	-------	--------

COORDINATES: _____

LOG BY: TIP

NORTH: _____

EAST: .

DRILLER: MT, DB / Mathes

DATE START: 12/16/90

DATE COMPLETE: 12 18 90

WEATHER: Raining, south wind 10 mph

PHYSICAL SETTING: Cross field

WELL INSTALLATION: NONE

[illegible]

Donohue

BORING LOG

SOIL BORING NO.

Engineers & Architects
COMPUTER AIDED DESIGN/DRAFTING

SITE: HIMCO DUMP PROJECT NO. 20026.023

BEG 07

DRILLING METHOD: 5 1/2" ~~Electric~~ block & mud rotary, down hole 140 lb hammer, 2" SS

WATER LEVEL READINGS

DATE	TIME	DEPTH	CASING

GROUND SURFACE ELEV.:

COORDINATES:

NORTH:

EAST:

LOG BY: TOM PUCHALSKI

DRILLER: MT/DB - Mathes

WEATHER: Rain, 40s, south wind 7 mph

PHYSICAL SETTING: Grass Field

DATE START: 12/16/90

DATE COMPLETE: 12/18/90

WELL INSTALLATION: NONE

DEPTH IN FEET	SOIL DEPOSITIONAL ENVIRONMENT	USCS	SOIL DESCRIPTION AND DRILLING COMMENTS	SAMPLING DATA				AIR MONITORING			
				B	N	A	R	TIME	PID	O ₂ LEL	CO H ₂ S
122											
124		SP	3.5 Y 5/2 Grayish Brn SAND, well sorted, low ch, saturated, fine grained OUTWASH	50				2"SS 123-125	1531	0	21.3 / 0 / 0
126											
128		SP	AS ABOVE + trace coarse sand - white subangular grains OUTWASH	52				3"SS 128-130	1528		
130											
132											
134		SP	2.5 Y 5/2 Grayish Brn SAND, fine grained low ch, sat trace coarse sand strong OUTWASH	50				3"SS 133-135	1539		
136											
138		SP	As Above OUTWASH	50				3"SS 138-140	1555		
140											
142											
144		SP	As Above OUTWASH	54				3"SS 143-145	1600		
146											
148		SP	As Above	48				3"SS 148-150	1610		

Donohue

BORING LOG

SOIL BORING NO.

Engineers & Architects
COMPUTER AIDED DESIGN/DRAFTING

SITE: HIMCO DUMP PROJECT NO. 70026.023

BPG08

DRILLING METHOD: 5" E" brush & air
to 20 feet, 5 1/2" blade bit & mud
interval 20-175 feet

WATER LEVEL READINGS

DATE	TIME	DEPTH	CASING

GROUND SURFACE ELEV.:

COORDINATES:

NORTH:

EAST:

LOG BY: TOM PUCHALSKI

DRILLER: Max Timm/Don Brewington - Mottos

DATE START: 12/19/90

DATE COMPLETE:

WEATHER: Clear, 33°F, South wind 5 mph

PHYSICAL SETTING: 60 ft south of WELL INSTALLATION:

DEPTH IN FEET	SOIL DEPOSITIONAL ENVIRONMENT	USCS	SOIL DESCRIPTION AND DRILLING COMMENTS	103 SAMPLING DATA				AIR MONITORING			
				B	N	A	R	TIME	PID	O ₂ LEL	CO H ₂ S
2			Blind drill with air rotary								
4			see log for WT 103A for first 20 feet								
6			8" casing to 9 feet								
8			↓								
10											
12											
14											
16									1043	0	21.3 0 0
18			↓								
20			10 1/2" 5/1 Gray Gravelly Sand, 40% shaly med grn sand, 30% coarse sand, 30% shaly & shaly, small gravel, saturated	31	15	15	15	18-20	1020	0	21.3 0 0
22			OUTWASH								
24			GP(?) RECOVERED ONE 3" COBBLE IN SPECIM TIP	15	15	15	15	23-25	1031	0	21.0 0 0
26											
28			10 1/2" 5/1 Gray GRAVELLY SAND, 40% shaly coarse grn sand, 30% med grn, 30% shaly & coarse med-grn med 1/2" med 3" saturated	33	15	15	15	28-30	1042	0	21.3 0 0

Donohue

BORING LOG

SOIL BORING NO.

Engineers & Architects
COMPUTER AIDED DESIGN/DRAFTING

SITE: HIMCO DUMP PROJECT NO. 20036.023

BPG08

DRILLING METHOD: See pg 1

WATER LEVEL READINGS

GROUND SURFACE ELEV.: _____

DATE _____ TIME _____ DEPTH _____ CASING _____

COORDINATES: _____

NORTH: _____

EAST: _____

LOG BY: TEP

DRILLER: See pg 1

DATE START: 12/19/90

DATE COMPLETE: _____

WEATHER: 3nac, 18°F, west wind 2mph

PHYSICAL SETTING: See pg 1

WELL INSTALLATION: NONE

DEPTH IN FEET	SOIL DEPOSITIONAL ENVIRONMENT	USCS	SOIL DESCRIPTION AND DRILLING COMMENTS	SAMPLING DATA				AIR MONITORING			
				B	N	A	R	SAMPLE TYPE INTERVAL	TIME	PID	O ₂ LEL
60			start 1145 1/3/91								
62											
64	GW		WELL GRADED GRAVEL > 3" broken in tip - green mafic volcanic - basalt, most 3/4" sbrd					"SS 63-65"	1342 0	0.3	0/0
66			OUTWASH					TOC08-01 63-63.5			
68	SP		10R 6/2LT brownish grey SAND, well sorted fine grained, non plas, low coh, sat					"SS 68-70"	1353 0	0.3	0/0
70			OUTWASH					TOC08-02 68-68.5			
72											
74	SP		10R 5/2 Grayish Brown SAND, well sorted fine grained, non plas, low coh, sat trace curvilinear white inclusions - silice plagioclase or chert(?)					"SS 73-75"	1400 0	0.3	0/0
76			OUTWASH					TOC08-03 73-73.5			
78	SP		As above					"SS 78-80"	1410 0	0.3	0/0
80			OUTWASH					TOC08-04 78-78.5			
82											
84	SP		Same as above					"SS 83-85"	1420 0	0.3	0/0
86			OUTWASH					TOC08-05 83-83.5			
88			8.5" zone of silty clay layers								
90	SM		10R 5P Grayish Brn SILTY SAND, 20% silt 80% low coh, non plas, sat fine grain sand, stratified silty clay layers at 88.5" smooth					"SS 88-90"	1434 0	0.3	0/0
92								TOC08-06 88-88.5			

Donohue

BORING LOG

SOIL BORING NO.

Engineers & Architects
COMPUTER AIDED DESIGN/DRAFTING

SITE: HIMCO DUMP PROJECT NO. 20026-023

BRG 08

DRILLING METHOD: See pg. one

WATER LEVEL READINGS

GROUND SURFACE ELEV.: _____

DATE _____ TIME _____ DEPTH _____ CASING _____

COORDINATES: _____

NORTH: _____

EAST: _____

LOG BY: TEP

DRILLER: See Pg one

DATE START: 12/19/90

WEATHER: See page three

PHYSICAL SETTING: See pg. 1

DATE COMPLETE: _____

WELL INSTALLATION: None

DEPTH IN FEET	SOIL DEPOSITIONAL ENVIRONMENT	USCS	SOIL DESCRIPTION AND DRILLING COMMENTS	SAMPLING DATA				AIR MONITORING					
				B	N	A	R	SAMPLE TYPE	INTERVAL	TIME	PI0	O ₂ LEL	C ₁ LEL
90													
92													
94		SP	10 YR 5/2 Grayish Brown SAND, fine grained, well sorted, non coh, sat	41				2'SS	93-95	1451	0	31	0/0
96			OUTWASH						GT08-03	93-93.5			
98			NO RECOVERY	50				2'SS	98-100	1500	0	21.0	0/0
100													
102													
104		SP	10 YR 5/2 Grayish Brown SAND, coarse mixed with hard and fine grained, sat fine grained, low coh, non plas, sat	50				2'SS	103-105	1510	0	19.0	0/0
106			OUTWASH										
108		SP	As above but all outwash fine grained	50				2'SS	108-110	1519	0	20.1	0/0
110													
112													
114		SP	As Above - OUTWASH	50				2'SS	113-115	1526	0	21.7	0/0
116													
118		SP	As Above OUTWASH	50				2'SS	118-120	1543	0	19.9	0/0

Donohue

BORING LOG

SOIL BORING NO.

Engineers & Architects
COMPUTER AIDED DESIGN/DRAFTING

SITE: HINCA DUMP PROJECT NO. 20026.023

BRG08

DRILLING METHOD: See pg one

WATER LEVEL READINGS

GROUND SURFACE ELEV.: _____

DATE _____ TIME _____ DEPTH _____ CASING _____

COORDINATES: _____

NORTH: _____

EAST: _____

LOG BY: TEP

DRILLER: See pg one

DATE START: 12/19/90

WEATHER: See pg three

PHYSICAL SETTING: See pg one

DATE COMPLETE: _____

WELL INSTALLATION: NONE

DEPTH IN FEET	SOIL DEPOSITIONAL ENVIRONMENT	USCS	SOIL DESCRIPTION AND DRILLING COMMENTS	SAMPLING DATA				AIR MONITORING			
				B	N	A	R	TIME	PID	O ₂ LEL	CO ₂ LEL
120											
122											
124		SP	10YR 5/2 Grayish Brown SAND, finegrained, non plas, low coh, sat Very fine grained - almost silt stratification occasional, trace organic debris in stratification < 1% OUTWASH	50				2"SS 123-125	1555	0	19.9 0/0
126											
128		SP	10YR 5/2 Grayish Brown SAND, well sorted, fine grained, low coh, non plas, sat OUTWASH	50				3"SS 128-130	1605	0	20.1 0/0
130											
132											
134		SP	As above	50				3"SS 133-135	1631	0	21.0 0/0
136											
138											
140		GW	Well graded Gravel with sand, most gravel > 2" (broken in spoon) - some 1" sand fine grained, saturated OUTWASH	50				3"SS 138-140	1641	0	19.9 0/0
142		GP	Poorly graded GRAVEL, most 1/4" sized, 15% fin grn sand, OUTWASH	50				3"SS 143-145	1653	0	20.0 0/0
144								GT08-C4	143-143.5		
146											
148		GP	Poorly graded Gravel As above	50				3"SS 148-150	1701	0	22 0/0

SOIL BORING NO.

Engineers & Architects
COMPUTER AIDED DESIGN/DRAFTING

SITE: HINCO DUMP PROJECT NO. 20036.023

BRG-C9

DRILLING METHOD: 7 1/8 tricone & air
to a 18 foot 5 7/8 blade bit &

WATER LEVEL READINGS

GROUND SURFACE ELEV.:

DATE	TIME	DEPTH	CASING
------	------	-------	--------

COORDINATES:

mud rotary - remainder of drive

NORTH:

LOG BY: TOM PUCHALSKI

EAST:

DRILLER: Max Tinnin / Don Brewington / Mathes

DATE START: January 5, 1991

WEATHER: Snow, 32°F, west wind 5 mph

60 ft south of 102 west at wind
PHYSICAL SETTING: *above*

DATE COMPLETE:

WELL INSTALLATION: NO E

DEPTH IN FEET	SOIL DEPOSITIONAL ENVIRONMENT	USCS	SOIL DESCRIPTION AND DRILLING COMMENTS	SAMPLING DATA				AIR MONITORING					
				B	N	A	R	SAMPLE		TIME	PID	O ₂ LEL	
								TYPE	INTERVAL				
2			Blind drill with air to 18 feet										
4			See log for WT102A for first										
6			18 feet.										
8													
10													
12													
14													
16													
18			START 1400 11/5/91										
20	SP		10 YR 5/3 BROWN, SAND, poorly sorted, coarse grained, sat, trace gvl, trace med sand	18	3	55	18-20	1400	0	21	0	0	0
22			OUTWASH					TOC 09-07	18-19				
24	SP		10 YR 5/3 Brown SAND, fn grained, sat, nonplv	25	2	55	23-25	1404	0	20.5	0	0	0
26			OUTWASH					TOC 09-07	23-23.5				
28	SP		10 YR 5/3 Brown SAND 20% Fine 70% med, 10% coarse, sat	35	2	55	28-30	1414	0	20.3	0	0	0
30								TOC 09-07	28-28.5				

Donohue

BORING LOG

SOIL BORING NO.

Engineers & Architects
COMPUTER AIDED DESIGN/DRAFTING

SITE: HUMCO DUMP PROJECT NO. 20026.023

BRG09

DRILLING METHOD: _____

WATER LEVEL READINGS

GROUND SURFACE ELEV.: _____

DATE _____ TIME _____ DEPTH _____ CASING _____

COORDINATES: _____

NORTH: _____

EAST: _____

LOG BY: _____

DATE START: 1/5/91

DRILLER: _____

DATE COMPLETE: _____

WEATHER: _____

PHYSICAL SETTING: _____

WELL INSTALLATION: NONE

DEPTH IN FEET	SOIL DEPOSITIONAL ENVIRONMENT	USCS	SOIL DESCRIPTION AND DRILLING COMMENTS	SAMPLING DATA				AIR MONITORING						
				B	N	A	R	SAMPLE TYPE INTERVAL		TIME	PID	O ₂ LEL	CO % HS	
30														
32														
34		SP	10 YR 5/3 Brown SAND, fine grained, sat trace small shang gvl. OUTWASH	25				2"SS	33-35	1420	0	31.2	0	0
36														
38		GP	Poorly graded GRAVEL, trace fine sand, most gvl > 2" diam, broken in spec. OUTWASH	25				2"SS	38-40	1425	0	31.0	0	0
40														
42														
44		GP	Poorly graded GRAVEL, most shd, some shang 3/4", basalt, dolomite, chert OUTWASH NE SAND	36				2"SS	43-45	1433	0	30.3	0	0
46		e												
48		GP	Poorly graded GRAVEL, 2" 1" shang 10% fn grn sand, sat OUTWASH	40				2"SS	48-50	1441	0	31.1	0	0
50														
52														
54		SP	10 YR 5/3 Brown SAND, poorly graded, fn grn, trace 1" gvl shang, qtzite, sat OUTWASH	16				2"SS	53-55	1449	0	30.7	0	0
56														
58		SP	10 YR 5/3 Grayish Brown SAND, 20% 1" shang gvl, sat OUTWASH	25				2"SS	58-60	1450	0	30.7	0	0

Donohue

BORING LOG

SOIL BORING NO. 023

Engineers & Architects
COMPUTER AIDED DESIGN/DRAFTING

SITE: HIMCO DUMP PROJECT NO. 20026.023

02309

DRILLING METHOD: See page 1

WATER LEVEL READINGS
DATE TIME DEPTH CASING

GROUND SURFACE ELEV.:
COORDINATES:

LOG BY: TOM PUCHALSKI

DRILLER: JMA

WEATHER: See page 1

PHYSICAL SETTING: Page 1

NORTH:

EAST:

DATE START: 1/5/91

DATE COMPLETE:

WELL INSTALLATION:

DEPTH IN FEET	SOIL DEPOSITIONAL ENVIRONMENT	USCS	SOIL DESCRIPTION AND DRILLING COMMENTS	SAMPLING DATA				AIR MONITORING		
				B	N	A	R	TIME	PID	O ₂ LEL
60										
62										
64	SP		10 YR 5/2 Grayish Brown SAND, noncoh, non plas, fine grained, sat	40				2"SS 63-65 1527 0 20.3 0 0		
66			OUTWASH					GT09-02 63-63.5		
68										
70	SP		As above	28				2"SS 68-70 1537 0 21.3 0 0		
72			OUTWASH					GT09-03 68-68.5		
74	SP		As above	8"SP				2"SS 73-75 1544 0 21.3 0 0		
76										
78	SW		10 YR 5/2 Grayish Brown GRAVELLY SAND, noncoh, non plas, sat 10/60/30 Fin/med/coarse 40% gravel	8"SP				2"SS 78-80 1554 0 21.3 0 0		
80			strongly							
82			Driller feels change							
84	SP		5Y 5/1 Gray SAND, fine grained-close to silt low coh, non plas, sat	7"SS				2"SS 83-85 1610 0 21.3 0 0		
86			OUTWASH							
88										
90	SP		5Y 4/3 Olive grey SAND as above	6"SP				2"SS 88-90 1625 0 21.3 0 0		

Donohue

BORING LOG

SOIL BORING NO. BRG 09

Engineers & Architects
COMPUTER AIDED DESIGN/DRAFTING

SITE: HIMCO DUMP PROJECT NO. 20026.022

DRILLING METHOD: Sp WATER LEVEL READINGS: DATE TIME DEPTH CASING GROUND SURFACE ELEV.:
LOG BY: COORDINATES: NORTH: EAST:
DRILLER: DATE START: DATE COMPLETE:
WEATHER: Overcast, 21°F PHYSICAL SETTING: WELL INSTALLATION:

DEPTH IN FEET	SOIL DEPOSITIONAL ENVIRONMENT	USCS	SOIL DESCRIPTION AND DRILLING COMMENTS	SAMPLING DATA				AIR MONITORING							
				B	N	A	R	SAMPLE TYPE	INTERVAL	TIME	PID	O ₂ LEL			
90		C	5Y 4/3 Olive Gray SILTY CLAY, stratified 1/8" apart, most, low plus												
92			LACUSTRINE												
94		CL	Attempt Shelby Tube 95-97 1745 - No Recovery in Tube	30				2'SS	93-95	1644	0	21.3	0	0	0
96			START 950 1/6/91												
98		CL	NO RECOVERY CL in sparsely SILTY CLAY LACUSTRINE	35				2'SS	98-100	953	0	21.3	0	0	0
100															
102															
104		CL	5Y 4/1 Dark Gray SILTY CLAY, med pks, med coh, non stratified, wet	12				2'SS	103-105	1005	0	21.1	0	0	0
106			LACUSTRINE												
108		SP	5Y 4/2 Olive gray SAND, 80% fn grained, 20% medium grt, subangular, sat	45				2'SS	106-110	1012	0	21.1	0	0	0
110			CUTWASH												
112															
114		CL	5Y 4/1 Dark Gray SILTY CLAY, med pks, med coh, non stratified, wet changes color to 2.5Y 5/2 Grayish Brown SILTY clay	17				2'SS	113-115	1023	0	21.2	0	0	0
116			CUTWASH												
118		ML	2.5Y 5/2 Grayish Brown SILT, trace fn sand in laminae, trace clay, wet	35				2'SS	118-120	1034	0	21.3	0	0	0

PHYSICAL SETTING: See dx 1

Donohue

BORING LOG

SOIL BORING NO.

Engineers & Architects
COMPUTER AIDED DESIGN/DRAFTING

SITE: HIMCO DUMP PROJECT NO. 20026.023

BRG 10

DRILLING METHOD: 7 1/8 tricone with air rotary to 18 feet, 7 1/8 double bit & mud rotary to end of boring
LOG BY: TOM PUCHALSKI
DRILLER: John Mathes & Assoc Inc
WEATHER: 19°F, clear, NE wind Drizzle

WATER LEVEL READINGS

DATE	TIME	DEPTH	CASING

GROUND SURFACE ELEV.:

COORDINATES:

NORTH:

EAST:

DATE START: Jun 7, 1991

DATE COMPLETE:

60 feet west of WT106A

PHYSICAL SETTING: grass at woods well INSTALLATION: NONE

DEPTH IN FEET	SOIL DEPOSITIONAL ENVIRONMENT	USCS	SOIL DESCRIPTION AND DRILLING COMMENTS	edge SAMPLING DATA				AIR MONITORING					
				B	N	A	R	SAMPLE TYPE INTERVAL		TIME	PIO	O ₂ LEL	CO H ₂ C
0			Blind drill to 18 feet with 7 7/8" tricone & air rotary. See log for WT104A for first 18 feet.										
2													
4													
6													
8													
10													
12													
14													
16													
18			Start 1000 11/8/91										
20		SP	104R 5/2 Grayish Brown GRAVELLY SAND, 70% med to coarse grained subrounded sand, 30% to 2" subangular gravel, non cohesive, non plastic, saturated Free > 20 grains OUTWASH	15	8"SS	18-20	1011	C	20.4	0	0	0	
						TOC 10-01	1F-1.5						
22													
24		SP	104R 5/2 Grayish Brown SAND, Fine grained, non coh, non plas, saturated OUTWASH	21	8"SS	23-25	1038	C	20.1	0	0	0	
						TOC 10-02	23-23.5						
26													
28		SP	104R 4/2 Dark Grayish Brown SAND, Fines, non coh, trace med grn. silt, sat OUTWASH	21	8"SS	28-30	1156	C	20.8	0	0	0	
						TOC 10-03	28-28.5						

Donohue

BORING LOG

SOIL BORING NO.

Engineers & Architects
COMPUTER AIDED DESIGN/DRAFTING

SITE: HIMCO DUMP PROJECT NO. 20026.023

BRG10

DRILLING METHOD:

WATER LEVEL READINGS

GROUND SURFACE ELEV.:

LOG BY:

DATE

TIME

DEPTH

CASING

COORDINATES:

NORTH:

EAST:

DRILLER:

DATE START: Jan 7, 1991

DATE COMPLETE:

WEATHER:

PHYSICAL SETTING: Page one

WELL INSTALLATION: NONE

DEPTH IN FEET	SOIL DEPOSITIONAL ENVIRONMENT	USCS	SOIL DESCRIPTION AND DRILLING COMMENTS	SAMPLING DATA				AIR MONITORING					
				B	N	A	R	SAMPLE		TIME	PIO	O ₂ LEL	CO %S
		TYPE	INTERVAL										
30													
32													
34			NO RECOVERY 3" Subangular cobbles in mat	18			J'SS	33-35	1215	0	21.1	0	0
36													
38		GP	GRAVEL, most 2" - broken shrd, some 1" - 3/4", basalt, dolomite predominance,	40			J'SS	38-40	1345	0	21.1	0	0
40			OUTWASH				GTIC	01 38-39					
42													
44		GP	GRAVEL As above	42			J'SS	43-45	1434	0	21.1	0	0
46			OUTWASH										
48		CL	ST 4/1 Dark Grey SILTY CLAY, low plasticity, low cohesion, saturated	48			J'SS	48-50	1443	0	21.1	0	0
50			LACUSTRINE				GTIC	02 48-50					
52		SP	ST 4/1 Dark Grey SAND, well sorted, fine grained, non coh., saturated	52			J'SS	53-55	1450	0	21.1	0	0
54			very fine grained - non coh. silt size OUTWASH				GTIC	05 53-54					
56													
58		SP	As above	60			J'SS	58-60	1500	0	21.1	0	0
			OUTWASH										

Donohue

BORING LOG

SOIL BORING NO.

Engineers & Architects
COMPUTER AIDED DESIGN/DRAFTING

SITE: HIMCO DUMP PROJECT NO. 20076-023

BRG10

DRILLING METHOD: Sp 12 WATER LEVEL READINGS GROUND SURFACE ELEV.:
DATE TIME DEPTH CASING COORDINATES:
LOG BY: Sp 02 NORTH:
DRILLER: EAST:
WEATHER: Overcast, SE wind 12, 30F DATE START: Jan 7, 1991
DATE COMPLETE:
PHYSICAL SETTING: Page 1 WELL INSTALLATION: NONE

DEPTH IN FEET	SOIL DEPOSITIONAL ENVIRONMENT	USCS	SOIL DESCRIPTION AND DRILLING COMMENTS	SAMPLING DATA				AIR MONITORING			
				B	N	A	R	TIME	PID	O ₂ LEL	CO H ₂ S
60											
62											
64		SP	54 4/1 Dark Grey SAND, fine grained, well sorted, lowish, non pls, saturated very fine grained - near silt size	30				2"SS 63-65	1507	0	21.0 / 0 / 0
66			OUTWASH								
68			NO RECOVERY	30				2"SS 68-70	1528	0	21.0 / 0 / 0
70											
72											
74		SP	54 5/2 Olive Gray, SAND, fine grained, lowish, saturated	41				2"SS 73-75	1540	0	21.0 / 0 / 0
76			OUTWASH					GT 10-03 73-74			
78		SP	3.5 5/2 Grayish Brown SAND, fine grained, lowish, non plastic, saturated	40				2"SS 78-80	1548	0	21.0 / 0 / 0
80			OUTWASH								
82											
84		SP	Same as above	39				2"SS 83-85	1557	0	21.0 / 0 / 0
86			OUTWASH								
88											
90		SP	As above	40				2"SS 88-90	1603	0	21.0 / 0 / 0
92			OUTWASH								

Donohue

BORING LOG

SOIL BORING NO.

Engineers & Architects
COMPUTER AIDED DESIGN/DRAFTING

SITE: HIMCO DUMP PROJECT NO. 20026.023

BRG10

DRILLING METHOD: See Page One
LOG BY: Page One
DRILLER: Page One
WEATHER: Page Three
WATER LEVEL READINGS
DATE TIME DEPTH CASING
GROUND SURFACE ELEV.:
COORDINATES:
NORTH:
EAST:
DATE START: Jan 7, 1991
DATE COMPLETE:
WELL INSTALLATION: NONE
PHYSICAL SETTING:

DEPTH IN FEET	SOIL DEPOSITIONAL ENVIRONMENT	USCS	SOIL DESCRIPTION AND DRILLING COMMENTS	SAMPLING DATA				AIR MONITORING				
				B	N	A	R	SAMPLE		TIME	PID	O ₂ LEL
						TYPE	INTERVAL					
90												
92												
94	SP		2.5' 5/2 Grayish Brown SAND, fine grained, non coh, non plastic, saturated	40		2"SS	93-95	1645	0	21.0	0	0
96			CUTWASH									
98	SP		Same as above	40		2"SS	98-100	1645	0	21.0	0	0
100												
102												
104	SP		2.5' 5/2 Grayish Brown SAND, fine grained, trace med grn, non coh, saturated	50		2"SS	103-105	1630	0	21.0	0	0
106			CUTWASH									
108	SP		2.5' 5/2 Grayish Brown SAND, fine grained trace coarse grained sand plus white graininess,	50		2"SS	108-110	1645	0	21.0	0	0
110			non coh, sat									
112			CUTWASH									
114	SP		Same as above	43		2"SS	113-115	1655	0	21.0	0	0
116			CUTWASH									
118	CL		10' 1/2 5/1 Gray SILTY CLAY, med plas, med coh	40		2"SS	118-120	1700	0	21.0	0	0

SOIL BORING NO.

PRG10

GROUND SURFACE ELEV.: _____

COORDINATES: _____

NORTH: _____

EAST:

LOG BY: JCS

DRILLER: _____

DATE START: Jan 7, 1991

DATE COMPLETE: Jan 9, 1991

WEATHER: 32°F. mist + snow. NE wind 5 mph.

PHYSICAL SETTING: Page One

DATE COMPLETE: SEP 1961
WELL INSTALLATION: NONE

DEPTH IN FEET	SOIL DEPOSITIONAL ENVIRONMENT	USCS	SOIL DESCRIPTION AND DRILLING COMMENTS	SAMPLING DATA				AIR MONITORING					
				B	N	A	R	SAMPLE TYPE INTERVAL		TIME	PID	O ₂ LEL	CO H ₂
100													
104		SP	Start 1/9/91 910 10YR 5/3 Brown SAND, well sorted, fine grained, noncoh, non plus, saturated OUTWASH	35	/	/	/	2"SS	133-135	920	0	21.7	0
106													
108		SP	As above OUTWASH	35	/	/	/	2"SS	138-140	934	0	21.0	0
110													
114		SP	As above OUTWASH	35	/	/	/	2"SS	137-139	939	0	21.0	0
116													
118		SP	As above + trace angular white mineral-fine grn OUTWASH	35	/	/	/	2"SS	138-140	950	0	21.0	0
144		SP	10YR 5/3 Brown SAND, well sorted, 80% fine grained, 20% medium grn, non coh, non plus, saturated OUTWASH	30	/	/	/	2"SS	143-145	956	0	21.0	0
148													
148		SP	10YR 5/3 Brown SAND, fine grn, noncoh, non plus Sub alternating with 1" to 1/4" thick layers of 10YR 5/1 Green silt clay bands. Wet OUTWASH	31	/	/	/	2"SS	148-150	1006	0	21.0	0

Donohue

BORING LOG

SOIL BORING NO.

Engineers & Architects
COMPUTER AIDED DESIGN/DRAFTING

SITE: HIMCO DUMP PROJECT NO. 20026.023

BRG10

DRILLING METHOD: See Page One WATER LEVEL READINGS: _____ GROUND SURFACE ELEV.: _____
DATE: _____ TIME: _____ DEPTH: _____ CASING: _____ COORDINATES: _____
NORTH: _____ EAST: _____
LOG BY: Page One DATE START: Jan 7, 1991
DRILLER: _____ DATE COMPLETE: Jan 9, 1991
WEATHER: Page Five PHYSICAL SETTING: Page One WELL INSTALLATION: NONE

DEPTH IN FEET	SOIL DEPOSITIONAL ENVIRONMENT	USCS	SOIL DESCRIPTION AND DRILLING COMMENTS	SAMPLING DATA				AIR MONITORING			
				B	N	A	R	TIME	PID	LEL	H ₂ S
150											
152											
154		SP	5Y 5/2 Olive Gray SAND, fine grained - near silt size, stratified, low coh, non plus, saturated LACUSTRINE	21	1	1	1	153-155	1012	0	0
156											
158		CL	2.5 YR 5/2 Grayish Brown SILTY CLAY, med plus, med coh, sat	15	1	1	1	158-160	1021	0	0
160		SM	2.5 YR 5/2 Grayish Brown SILTY SAND, fine grained, low coh, non plus, saturated LACUSTRINE					GEOTECH GT 04	158-159.5		
162											
164		SM	2.5 YR 5/2 Grayish Brown, SILTY SAND, low coh, fine grained, 20% silt, 80% sand, low coh, non plus, saturated LACUSTRINE	26	1	1	1	163-165	1032	0	0
166											
168		CL	10YR 4/1 Dark Gray SILTY CLAY, med plus, med coh, stratified, moist LACUSTRINE	26	1	1	1	168-170	1040	0	0
170											
172											
174		ML	10YR 4/1 Dark Gray SILT, non plus, med coh, non stratified, moist LACUSTRINE	10	1	1	1	173-175	1046	0	0
176											
			SCB Split spoon to 174 drill 7 1/4 to 173 1/4 1991 1050 - Gray Fimbriata								

TECHNICAL MEMORANDUM NUMBER 5

ORIGINAL

DATE: April 1, 1991
TO: Marcia Kuehl
CC: Bob Isenberg
FROM: John Cicone
SUBJECT: EPA ARCS Region V Contract No. 68-W8-0093
EPA Work Assignment No. 17-5L4J
Donohue Project No. 20026.025
Himco Landfill RI/FS

GEOTECHNICAL DATA EVALUATION

Introduction

The objective of this data evaluation is to determine if the data provided from laboratory consolidation and triaxial shear tests, Atterberg limits, grain size and permeability is sufficient enough for use in Remedial Investigation (RI) and Feasibility Study (FS) reports for the Himco Landfill.

Analytical Results

The following table shows the tests for which data was provided and a summary of the results:

<u>LABORATORY TEST</u>	<u>RESULTS</u>
Unconsolidated Undrained (uu) Triaxial Shear	Cohesion (c) = 7 psi = 1008 psf friction angle (ϕ) = 33 degrees
Atterberg Limits	See Table 1 (attached)
Grain Size	30 curves total
Consolidation	Unable to obtain results with given data (see Geotechnical Data Interpretation)

Geotechnical Data Interpretation

Data provided for the unconsolidated undrained (uu) triaxial shear testing was sufficient to obtain cohesion and friction angle values. The attached figure shows the Mohr-Coulomb failure envelope plotted by the laboratory and the tangent line drawn by Donohue to obtain cohesion (c) and friction angle (ϕ) values. Test results indicate cohesion and friction angle for the test sample are approximately 7 psi and 33 degrees, respectively.

Data provided for grain size and Atterberg limits was complete and require no additional interpretation.,

Data was provided for a consolidation test. The consolidation coefficient, c_v , which is used to determine how long consolidation will take, can normally be determined from this test. However, c_v cannot be obtained with the data provided. All of the data curves seem to indicate the specimens had not reached 100% consolidation when the test was stopped. Two possible conclusions can be drawn from this termination. The first is that the test was stopped too early resulting in an incomplete curve and c_v cannot be calculated. The second is that the material may have undergone a very rapid consolidation and c_v could only be obtained with some difficulty and accuracy would be limited. The grain size curve for the consolidation test sample indicated a clayey silt, which does not normally have a rapid consolidation. Therefore, the second possibility seems less likely; however, definite conclusions cannot be made with available information.

Data was also provided for the consolidation test to allow for calculation of the compression index, C_c . This value is used to determine the magnitude of consolidation settlement. This value cannot be obtained because the x-axis is labeled improperly as ELAPSED TIME (min) when it should be labeled as a load or pressure (see attached figure).

Summary

The triaxial shear, Atterberg limit and grain size data were sufficient to obtain strength parameters, and to establish soil classifications of the on-site soil.

No permeability test data was provided with the laboratory results and should be obtained if drainage of material beyond site boundaries is a concern.

Consolidation test information was insufficient to calculate c_v and C_c . The laboratory should be contacted to determine why testing was stopped and to relabel the appropriate graph. Further, the laboratory should, as a matter of common practice, provide the c_v and C_c values.

Attachments - Atterberg Limits Results
- Triaxial Shear Test Results
- Compression Index Curve

A/R/HIMCO/AH6

CONSOLIDATION TEST RESULTS
(ASTM D2435)

PROJECT: SAS 5993E SML / TETC NO.: 91-212-310B
CLIENT PROJECT NO.: 5993E CLIENT: VIAR COMPANY
REPORT DATE: Feb. 18, 1991 SUMMARIZED BY: S. Sayawataana

SAMPLE NO.: HD K 14-01 DEPTH: N/A ft.
INITIAL DRY DENSITY: 91.0 pcf. INITIAL MOISTURE CONTENT: 34.0 pct.
INITIAL VOID RATIO: 0.816
SPECIFIC GRAVITY: 2.65 (assumed)

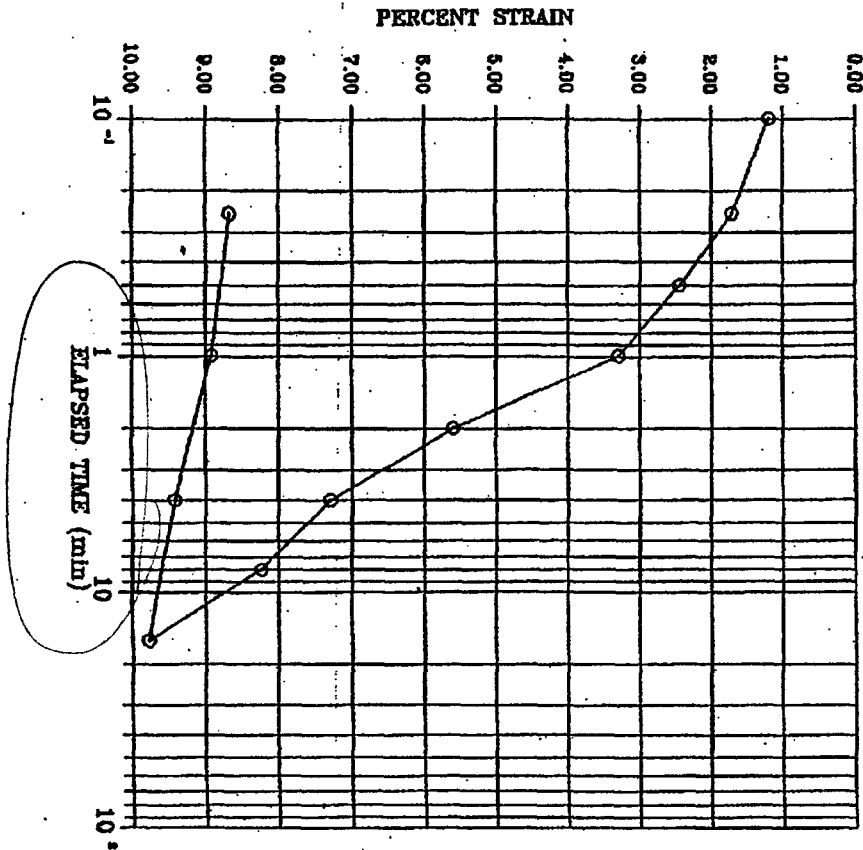


TABLE 1
SUMMARY
OF
LABORATORY TEST RESULTS

PROJECT: SAS 5993E

TBTC NO.: 91-220-3108

PROJECT NO.: SAS 5993E

CLIENT: VIAR COMPANY

REPORT DATE Feb. 19, 1991

SUMMARIZED BY: S. Sayrawatsana

LABORATORY MANAGER: (Arul) K. Arulmoli

BORING & SAMPLE NO.	ATTERBERG LIMITS (ASTM D 4318)		
	LIQUID LIMIT (%)	PLASTIC LIMIT (%)	PLASTICITY INDEX (%)
HDGT-07-06-01	21	12	9
HDGT-07-07-01	17	13	4
HDGT-08-05-01	16	11	5
HDGT-09-06-01	14	11	3
HDGT-09-07-01	23	14	9
HDGT-10-04-01	21	13	8
HDGT-10-05-01	24	17	7

TABLE 1

SUMMARY

OF

LABORATORY TEST RESULTS

PROJECT : SAS 5993E

TETC NO. : 91-220-3108

PROJECT NO. : SAS 5993E

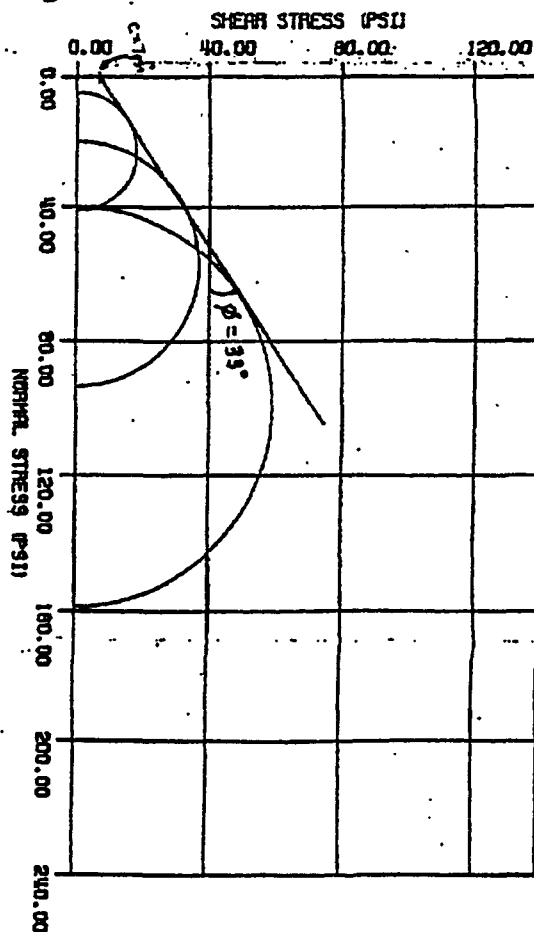
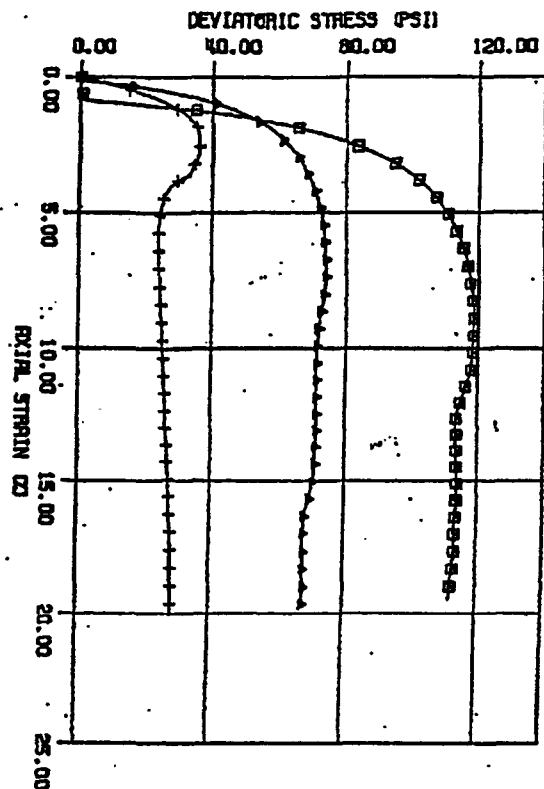
CLIENT : VIAR COMPANY

REPORT DATE Feb. 19, 1991

SUMMARIZED BY: S. Sayaratana

LABORATORY MANAGER : (Arul) K. Arulmoli

BORING & SAMPLE NO.	ATTERBERG LIMITS (ASTM D 4318)		
	LIQUID LIMIT (%)	PLASTIC LIMIT (%)	PLASTICITY INDEX (%)
HDGT-07-06-01	21	12	9
HDGT-07-07-01	17	13	4
HDGT-08-05-01	16	11	5
HDGT-09-06-01	14	11	3
HDGT-09-07-01	29	14	9
HDGT-10-04-01	21	13	8
HDGT-10-05-01	24	17	7

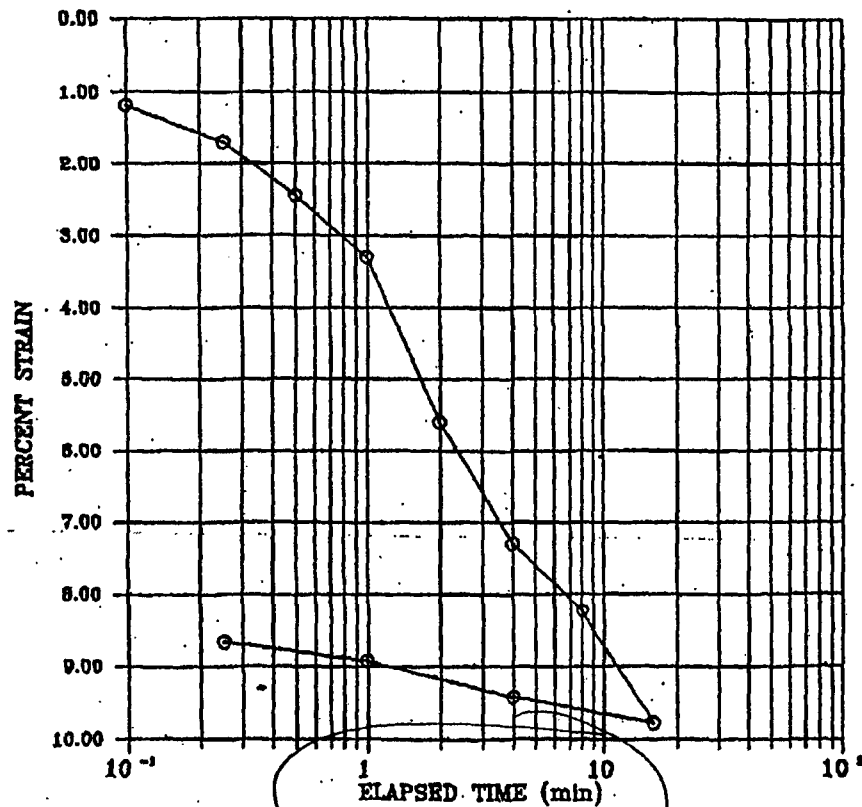


STRESS	DEVIATORIC	AXIAL	TEST	DEV. STRESS	MOHRS	PR. DEF.	PR. DEF.	PR. DEF.	PR. DEF.
NO.	NO.	NO.	NO.	NO.	NO.	NO.	NO.	NO.	NO.
5-00001	5-00001	5-00001	UU	5-00001	5-00001	5-00001	5-00001	5-00001	5-00001
5-00002	5-00002	5-00002	UU	5-00002	5-00002	5-00002	5-00002	5-00002	5-00002
5-00003	5-00003	5-00003	UU	5-00003	5-00003	5-00003	5-00003	5-00003	5-00003

CONSOLIDATION TEST RESULTS
(ASTM D2435)

PROJECT: SAS 5993E SML / TETC NO. : 91-212-3108
CLIENT PROJECT NO.: 5993E CLIENT : VIAR COMPANY
REPORT DATE : Feb. 18, 1991 SUMMARIZED BY : S. Sayawatana

SAMPLE NO. : HD K 14-01 DEPTH : N/A ft.
INITIAL DRY DENSITY : 91.0 pcf. INITIAL MOISTURE CONTENT : 34.0 pct.
INITIAL VOID RATIO : 0.816
SPECIFIC GRAVITY : 2.55 (assumed)



TECHNICAL MEMORANDUM - NO. 6

ORIGINAL

DATE: APRIL 29, 1991

TO: Vanessa Harris - Site Manager

CC: Marcia Kuehl - RI Lead
Roman Gau - Project Manager
Mike Crosser - TSQAM

FROM: Tom Puchalski

SUBJECT: EPA Arcs Region V Contract No. 68-W8-0093
EPA Work Assignment No. 17-5L4J
Donohue Project No. 20026.024
Himco Dump Phase I

PRIVATE WELL SAMPLING AND BASEMENT AIR SCREENING

Introduction

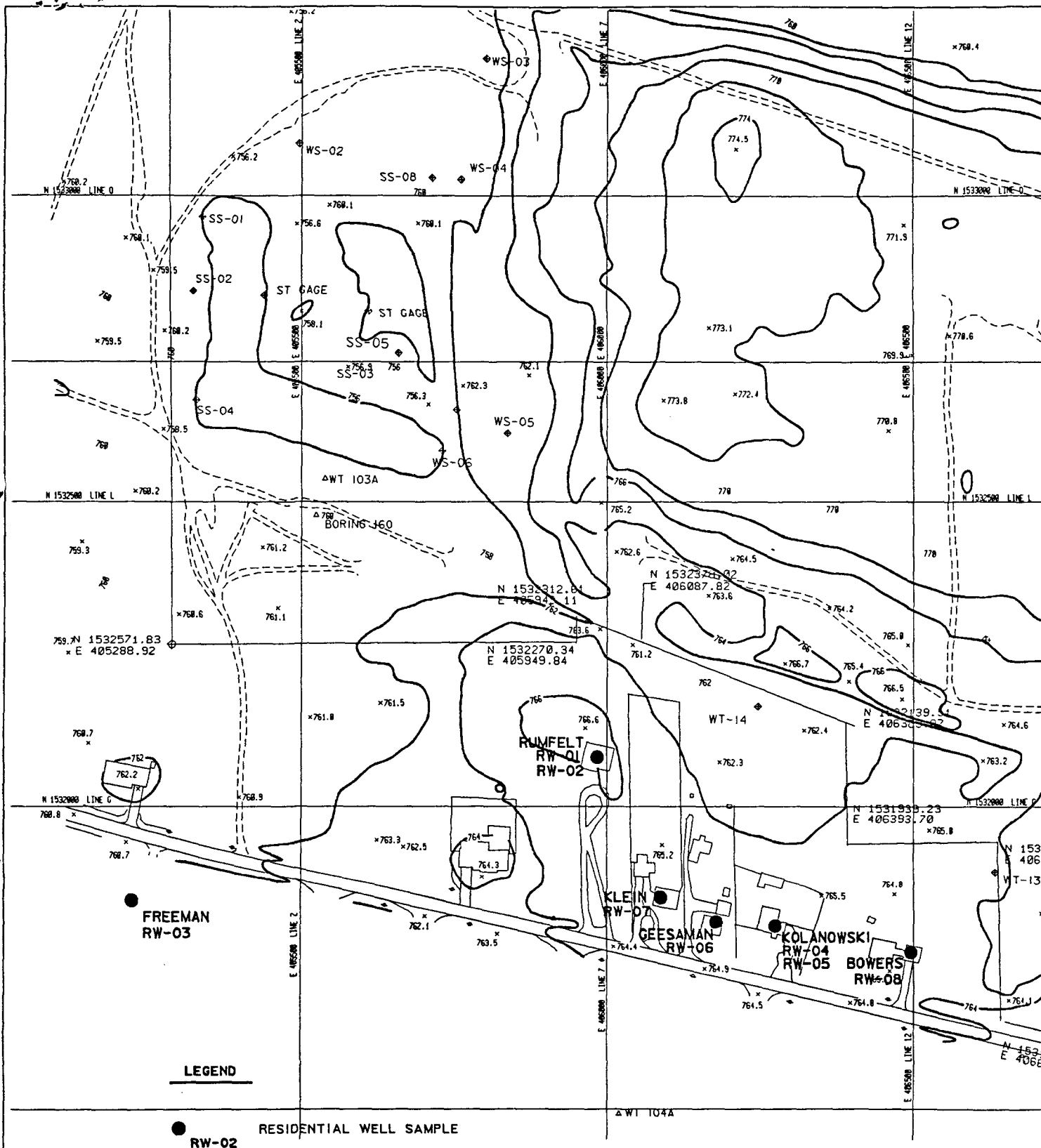
Groundwater samples were collected from five residential wells immediately south of the Himco Dump site along County Road 10, and one residential well immediately south of County Road 10 on October 22, 23, and 24, 1990. Four basements of these residences along County Road 10 were also screened for the presence of landfill gases.

Residential wells were sampled to investigate groundwater quality. Originally, all residences had shallow (approximately 22 feet deep) wells. Deeper wells (RW-01, RW-03, RW-04, RW-06, RW-07, RW-08) (at 152 to 172 feet) were installed in 1974. Although the state found high levels of manganese in these wells in 1974 and were ordered replaced, some of the original shallow wells remain. Two wells (RW-02 and RW-05) were sampled at residences where an older shallow well was accessible in addition to their present deep wells. Shallow wells were sampled in addition to deep wells at the Rumfelt and Kolanowski residences.

Basement gas was screened to evaluate if landfill gas which may be generated at the site has migrated off-site and into these nearby resident's basements. This screening was qualitative to check for the presence of methane and hydrogen sulfide.

Procedures

Groundwater sampling of residential wells and basement air screening was carried out as described in Sections 4.2.4 and 4.8 of the Final Field Sampling Plan, Himco Dump, Remedial Investigation/Feasibility Study, Elkhart, Indiana. The residents names and their addresses are: Noble and Selma Bowers, 28279 CR 10; Mark Freeman, 28552 CR 10; Dave and Joan Geesaman, 28331 CR 10; James and Christine Klein, 28343 CR 10; Helen Kolanowski, 28213 CR 10; and Herman and Patricia Rumfelt, 28369 CR 10 (Figure 1). Samples obtained from newer deep wells were obtained directly from the tap at the kitchen



MARCH 1991

FIGURE 1 RESIDENTIAL WELL LOCATIONS

HIMCO DUMP
SUPERFUND SITE
ELKHART, INDIANA

20026

Donohue ENGINEERS
ARCHITECTS
SCIENTISTS

sink or if available, at a tap in the basement ahead of the water softener. The tap was allowed to purge for five minutes before the sample was collected. Samples taken from shallow wells were purged by bailing. A 1-inch bailer was used in these 1 1/2-inch I.D. wells.

Samples for bromide analysis were field filtered using a millipore filtration unit and 0.45 micron filters. Measurements of field pH, conductivity, temperature, and dissolved oxygen were obtained at the field trailer immediately following sample collection. Preservatives, sample bottles, and holding times are summarized in Table 4-2 of the Final Field Sampling Plan.

Deviations from Project Plans

One of the six residences which were originally scheduled for well sampling and basement air screening was removed from the list when the owner of the home could not be located. A homeowner located south of the Himco Dump immediately south of County Road 10 (Freeman) solicited EPA to be added to the list of residential wells to be sampled. Sampling of the Freeman well brought the total residential well locations back up to the anticipated six. The Kolanowski residence did not have a basement and, consequently, was not screened for landfill gas.

Not all of the original six old shallow wells were intact and accessible. In practice, only two older shallow wells (RW-02 and RW-05) were accessible for sampling.

The shallow residential wells were not of large enough diameter (1-1/2-inch) to sample with a Keck pump as described in the field sampling plan. A 1-inch bailer was used as an alternative sampling method.

Five gallons were removed from each of the two residential wells. Readings of pH, conductivity, dissolved oxygen, and volume removed were not recorded during purging of the residential wells, but were recorded after 5 minutes of running the tap for deep wells, or upon removal of 5 gallons from shallow wells.

The 1-inch bailer was decontaminated between sampling locations by an alconox and tap water wash, a tap water rinse, an isopropanol rinse, and two deionized or distilled water rinses. Isopropanol rinsates were collected in a 5-gallon bucket and covered for eventual discharge into an on-site frac tank.

Summary of Results

Eight groundwater samples were collected from six locations. Six deep wells were sampled from taps and two shallow wells were sampled by bailing.

The Geesaman and Bower shallow wells were abandoned; the shallow Klein well was in a location which made it inaccessible to bailing, and the fourth shallow well was at a residence which was locked and not occupied.

Basement air was screened at the Rumfelt, Geesaman, Klein, and Bowers residences. A hydrogen sulfide and methane gas detector was used to screen the basement air. No detections of these compounds were registered during any of the basement air monitoring.

A/R/HIMCO/AB2

ORIGINAL

TECHNICAL MEMORANDUM NUMBER 7

DATE: January 24, 1991

TO: Vanessa Harris - Site Manager

CC: Marcia Kuehl - RI Lead
Roman Gau - Project Manager
Mike Crosser - TSQAM

FROM: Tom Puchalski

SUBJECT: EPA ARCS Region V Contract No. 68-W8-0093
EPA Work Assignment No. 17-5L4J
Donohue Project No. 20026.024
Himco Dump

LANDFILL CAP SOIL SAMPLING

Introduction

Twelve soil samples of the landfill cap at the Himco Dump site in Elkhart, Indiana, were collected for chemical analysis on November 8, 9, 10, 11, and 12. Sampling methods described in the Final Field Sampling Plan, Himco Dump Remedial Investigation/Feasibility Study, Elkhart, Indiana were followed. Sampling was done by Eric Slusser and Tom Puchalski of Donohue & Associates, Inc. The purpose of sampling the landfill cap was to characterize the chemistry of the white powder matrix which makes up the majority of the cap material.

Methods

Section 4.0 of the Final Field Sampling Plan, Himco Dump Remedial Investigation/ Feasibility Study, Elkhart, Indiana, describes the method used for soil cap sampling and the technique used to define the sampling locations. The sampling locations were spread out to cover the entire landfill cap. Soil samples were located from a systematic grid marked by survey stakes. The actual soil sampling locations are provided in Figure 1. Completed soils data forms are presented in Appendix A.

The twelve soil samples were collected from depths as shallow as three to nine inches and as deep as eight to sixteen inches. The depth varied dependent upon the thickness of the overlying sand and topsoil cover. The cover material overlying the white material, assumed to be calcium sulfate, was removed with a shovel prior to sampling at each location. A hand auger was used to dig out the white material. The sample was placed in a stainless steel bowl and immediately placed in two 4 oz. jars for volatile analysis. The remaining sample volume in the bowl was mixed using a stainless steel spoon. After a homogeneous mixture was obtained, the sample was divided into four quadrants. Small portions of each quadrant were used to fill each remaining sample jar.

Before sampling and between each sample location, all sampling equipment was decontaminated with: (1) a soap and tap water wash, (2) a tap water rinse, (3) an isopropanol rinse, and (4) two rinses with distilled or deionized water. Isopropanol rinses were retained in a covered 5-gallon pail for eventual discharge into the on-site frac tank.

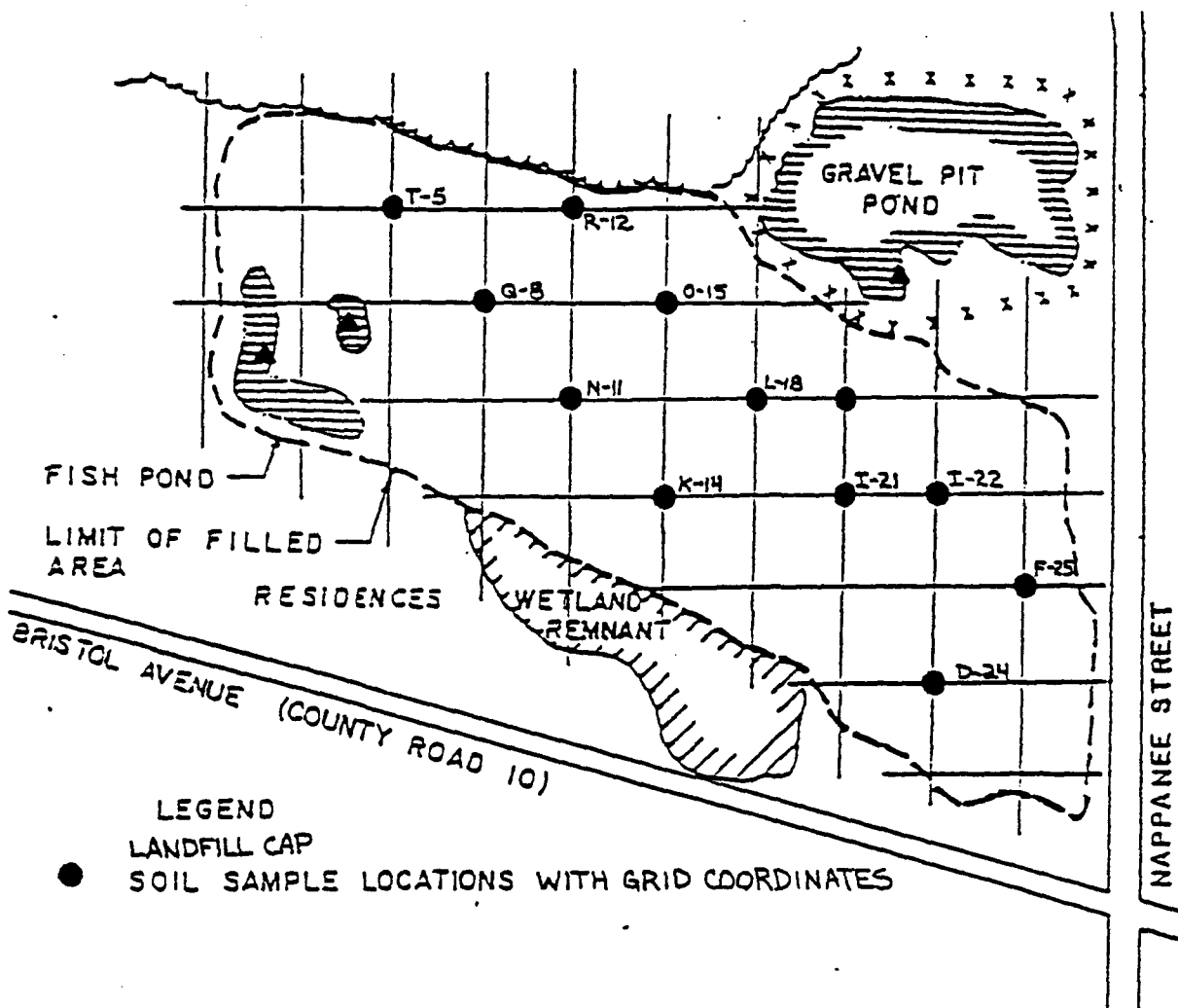
Deviations

Figure 4-1 of the Field Sampling Plan shows soil sampling locations based on a grid system which was not used in the field. The grid shown in Figure 4-1 is diagrammatic and not meant to represent the final surveyed grid. It was designed to show approximate soil cap sampling locations. Actual grid points were selected in the field using the general pattern, as shown in Figure 4-1, so that the entire area of the landfill cap was sampled. The actual grid points are shown in Figure 1 of this memorandum. Photographs were not taken of each location on the landfill cap as the sampling areas were similar, and the photo would not aid in identifying the location.

Summary of Results

Soil samples of the cap soil material were taken at twelve locations spaced out across the area of the landfill cap. In general, the white material thins from west to east. The appearance of the white material is uniform with no discernible trends. Soils data forms are provided in Appendix A of this memorandum.

A/R/HIMCO/AB1



0 500 1000

SCALE: FEET
SCALE IS APPROXIMATE

SOURCE: US EPA, AUGUST, 1986

Donohue APPROXIMATE SITE SAMPLING LOCATIONS



20026
MAY, 1990

FIELD SAMPLING PLAN
HIMCO DUMP SITE
ELKHART, INDIANA

FIGURE 1

Donohue

Soils Data Form

Soil Sample Area Capso. 1 ChSoil Subsample T-5 GS-C

Engineers & Architects & Scientists

Site Himco DumpProject No. 20026.02DATE 11/8/90TIME 1408COLLECTOR TOM PUCHALSKI
ERIC SLUSSERSAMPLE DEPTH 12-18" from surface

_____PHYSICAL DESCRIPTION OF SUBSAMPLING LOCATION: T-5 survey marker
at northwest corner of land fill cap at edge of woods.

_____DESCRIPTION OF SUBSAMPLE: White silt (MC) non plas, low rel, damp.

_____ANY OTHER CHARACTERISTICS OF NOTE: 1 foot of fine grained Brn silty
sand fill on top of white cap material. Used a shovel to remove upper sand
then hand augered from 12-18"

Donohue Soils Data Form Soil Sample Area Cap soil
Soil Subsample GS 02

Engineers & Architects & Scientists Site Himro Dump Project No. 20026-02

DATE 11/8/90
TIME 1641
COLLECTOR TOM RUCHALSKI
ERIC SLUSSER

SAMPLE DEPTH 6-18"

PHYSICAL DESCRIPTION OF SUBSAMPLING LOCATION: Q-8 survey stake
to 350 feet east of western edge of land fill cap

DESCRIPTION OF SUBSAMPLE: 6 inches of topsoil and brown silty sand
overlying sample. Sample is white silt (MC) w/ gas, brown, damp.

ANY OTHER CHARACTERISTICS OF NOTE: Bottom of white silt cap at
~ 18"

Donohue

Soils Data Form

Soil Sample Area Cap soil

Soil Subsample GS03

Engineers & Architects & Scientists

Site Himco Dump

Project No. 20026-02

DATE 11/9/90

TIME 840

COLLECTOR TDH PUCHALSKI
ERIC SLUSSER

SAMPLE DEPTH 6-18"

PHYSICAL DESCRIPTION OF SUBSAMPLING LOCATION: Cap soil at survey
stake N-11 near middle of flat covered land fill, vegetation at ground
surface consists of moss and grass.

DESCRIPTION OF SUBSAMPLE: Sample consists of white silt (ML)
with a trace of fine brown sand in thin (a few mm) stringers

ANY OTHER CHARACTERISTICS OF NOTE: _____

Donohue

Soils Data Form

Soil Sample Area Cap SoilSoil Subsample G504

Engineers & Architects & Scientists

Site Himco DumpProject No. 20026.033DATE 11/9/91TIME 937COLLECTOR TOM PUCHALSKI
ERIC SLUSSESAMPLE DEPTH 0-3" Silty Sand Cover - Not Sampled
3"-17" Sampled
white siltPHYSICAL DESCRIPTION OF SUBSAMPLING LOCATION: Survey marker K-14
near southeast end of landfill cap about 300 feet north of
wetland remnantDESCRIPTION OF SUBSAMPLE: White silt (m) with a trace of
brown sand in thin fractures. Moist, non plastic, low calcANY OTHER CHARACTERISTICS OF NOTE: Sumac is dead in this area.
Reached grey moist paper (waste) at 18". Methane gas was exiting the
auger hole. We immediately covered the hole

Donohue

Soils Data Form

Soil Sample Area LandfillSoil Subsample G505

Engineers & Architects & Scientists

Site Lime DumpProject No. 70026.00DATE 11/10/90TIME 841COLLECTOR Eric Slusser
Tom PuchalskiSAMPLE DEPTH 8-16"

_____PHYSICAL DESCRIPTION OF SUBSAMPLING LOCATION: Middle north area of
land fill cap \approx 100 feet north of woods at survey stake R-12
South of 11/10/90

_____DESCRIPTION OF SUBSAMPLE: White silt (ML) blowback, non plas, damp.

_____ANY OTHER CHARACTERISTICS OF NOTE: 0-8" brown fn gran silty sand fill.
Refusal at 18" is light brown paste-like material. No odor

Donohue

Soils Data Form

Soil Sample Area Landfill CaSoil Subsample G506

Engineers & Architects & Scientists

Site Himer DumpProject No. 20026-02DATE 11/10/90TIME 905COLLECTOR TOM RUCHALSKI
ERIC SLUSSERSAMPLE DEPTH 6-14"
8

PHYSICAL DESCRIPTION OF SUBSAMPLING LOCATION: ≈ 200 feet south
of brush at south end of quarry pond at survey stake A-15

DESCRIPTION OF SUBSAMPLE: White silt (ML), low coh. non plas. moist.
6" of cover fill consists of brown fine grained silty sand - ~~core~~
which was not sampled. Grey silty sand at 14" was also not
sampled.

ANY OTHER CHARACTERISTICS OF NOTE:

Donohue

Soils Data Form

Soil Sample Area Landfill CapSoil Subsample GSO7

Engineers & Architects & Scientists

Site Himco DumpProject No. 20026-02DATE 11/11/90TIME 9/12COLLECTOR ERIC SLUSSER
TOM PUCHALSKISAMPLE DEPTH 12-15"

PHYSICAL DESCRIPTION OF SUBSAMPLING LOCATION: At survey location
1-18 at area of grass and small trees and shrubs at east edge of
landfill cap ~ 400 feet south of the west edge of the quarry pond.

DESCRIPTION OF SUBSAMPLE: Sample consists of white silt (ML) low clay,
non plastic, moist with brown fractures - rare.

ANY OTHER CHARACTERISTICS OF NOTE: A thin layer of white silt
exists from 3-5" sandwiched between fine silty sand cover material

Donohue

Soils Data Form

Soil Sample Area LandfillSoil Subsample GS08

Engineers & Architects & Scientists

Site Himer DumpProject No. 20026.00DATE 11/11/90TIME 954COLLECTOR TOM PUCHALSKI
ERIC SLUSSERSAMPLE DEPTH 13"-15"

PHYSICAL DESCRIPTION OF SUBSAMPLING LOCATION: Near west edge of
access road at east edge of landfill cap at survey marker L-21. About
200 feet

DESCRIPTION OF SUBSAMPLE: White areas and light grey areas of silt (MU)
with nolets-trace. Trace light yellow fractures
0-6" - Brown fine silty sand
6-13" Black cinderly fill
13-15" White & gray silt - Sampled
15" Grey fine sand

ANY OTHER CHARACTERISTICS OF NOTE: Chemical odor

Donohue

Soils Data Form

Soil Sample Area Landfill

Soil Subsample AS1A9
967

Engineers & Architects & Scientists

Site Himen Dump

Project No. 20026-02

DATE 11/11/90

TIME 1127

COLLECTOR TOM PIKULSKI
ERIC SLUSSER

SAMPLE DEPTH 8-18"

PHYSICAL DESCRIPTION OF SUBSAMPLING LOCATION: East edge of high
flat land fill cap ~30 feet west of access road at survey marker I-21

DESCRIPTION OF SUBSAMPLE: White silt (ML) low ch. nodules, moist with
a trace of black fractures. 3" of brown firm SM could not sampled

ANY OTHER CHARACTERISTICS OF NOTE: Lichens at surface

Donohue

Soils Data Form

Soil Sample Area Landfill CapSoil Subsample GS10

Engineers & Architects & Scientists

Site Himca DumpProject No. 30026.07DATE 11/12/90TIME 853COLLECTOR TOM PUCHALSKI
ERIC SLUSSERSAMPLE DEPTH 3-9"

_____PHYSICAL DESCRIPTION OF SUBSAMPLING LOCATION: Same grid point
I-22 at east edge of access road. Piles of asphalt debris nearby.

_____DESCRIPTION OF SUBSAMPLE: White silt (ML) interlayered with brown 10YR 5/3
fine grained silty sand (SM). Sample has enacrid H₂S odor.

_____ANY OTHER CHARACTERISTICS OF NOTE: Base of silt defined by lower
fine grained brown sand.

Donohue

Soils Data Form

Soil Sample Area Landfill CorpSoil Subsample GS11E Dup

Engineers & Architects & Scientists

Site Hince DumpProject No. 20026.023DATE 11/12/90TIME 947COLLECTOR TOM PUCHALSKI
ERIC SLUSSERSAMPLE DEPTH 0-4" - Cover soil - Not Sampled
4"-18" - SampledPHYSICAL DESCRIPTION OF SUBSAMPLING LOCATION: 60 feet west of
Nardavine St extension at E-25DESCRIPTION OF SUBSAMPLE: White silt with a trace of rootlets.
Silt is moist, low coh, non plas.ANY OTHER CHARACTERISTICS OF NOTE: Did not reach the base of
the white silt

Donohue

Soils Data Form

Soil Sample Area Landfill (CP)Soil Subsample G512

Engineers & Architects & Scientists

Site Himco DumpProject No. 20026-03DATE 11/12/90TIME 1030COLLECTOR ERIC BLUSSER
TOM PUCHALSKISAMPLE DEPTH 4-8"PHYSICAL DESCRIPTION OF SUBSAMPLING LOCATION: Survey stake
D-24 east of access road ~ 100 feet NE of job trailerDESCRIPTION OF SUBSAMPLE: white silt (CL) with light brown fracture
fill staining & rootlets.ANY OTHER CHARACTERISTICS OF NOTE: Could not sample at D-23
as no white silt was present.

TECHNICAL MEMORANDUM NUMBER 8

ORIGINAL

DATE: April 3, 1991
TO: Vanessa Harris - Site Manager
CC: Roman Gau - Project Manager
Mike Crosser - TSQAM
FROM: Tom Puchalski
SUBJECT: EPA ARCS Region V Contract No. 68-W8-0093
EPA Work Assignment No. 17-5L4J
Donohue Project No. 20026.024
Himco Dump RI/FS

WELL SAMPLING

Introduction

Ten groundwater monitoring wells installed during this investigation, and 23 previously installed wells were sampled at the Himco Dump site on November 14 through January 9, 1991, to investigate the vertical and horizontal extent and degree of contamination of the uppermost unconsolidated aquifer. Groundwater samples were collected by Eric Slusser, Steve Spiewak, Tracy Koach, and Anya Kirykwicz of Donohue & Associates, Inc. Groundwater samples were collected as described in Section 4.2.4 of the Final Field Sampling Plan, Himco Dump Remedial Investigation/Feasibility Study, Elkhart, Indiana. The well locations are shown in Figure 1. Completed purge and sample collection forms are in Appendix A. Table 1 contains the well bottom depths for all wells used in the sampling event.

Methods

All field meters were calibrated at the beginning of each day before sampling activities began. The sampling equipment was transported to each well location in plastic coolers.

After unlocking the protective casing, a photoionization detector was used to monitor the air near the casing top. A decontaminated water level measuring tape was then lowered into the well casings to obtain a water level and well bottom depth. This information was recorded on the purge and sample form. A well volume was calculated from this information so that at least five volumes could be removed during the purging process.

A YSI water quality meter was connected in-line with a Keck pump so that direct measurements of pH, conductivity, and temperature could be collected from the purge water. Purging continued until the readings have stabilized to pH ± 0.1 unit, conductivity ± 10 percent, and temperature to $\pm 0.5^\circ$ C. This information was recorded on the purge and sample collection form. As soon as the purge pump was removed, a second reading of the water level was obtained.

An alternative purging method was used for 4-inch diameter wells due to the large volumes of purge water which needed to be removed before sampling. A stainless steel submersible pump was used which pumped up to 20 gallons per minute. This 220-volt electric pump received its power from a portable gasoline generator.

A 500-gallon polyethylene tank was strapped to the back of a four-wheel drive pickup truck so that the purge water could be collected from each well and transported to the on-site 21,000-gallon frac tank. Measurements of pH, conductivity, and temperature were recorded periodically during the purging process with a combination pH, conductivity, temperature meter. The Keck pump was used to sample these wells following purging with the submersible pump.

Wells F-1 and F-3 were purged by bailing with a 1-inch diameter bailer. Readings of pH, conductivity, and temperature were collected periodically as purging progressed.

The time between the completion of purging and the collection of the sample did not exceed 24 hours for any well. Table 4-2 of the Final Field Sampling Plan summarizes the sample container and preservative requirements. When a preservative was added to a sample, pH paper was used to ensure that adequate preservative was added.

Samples obtained for dissolved metals or bromide analysis were collected in a one liter polyethylene container for filtration at the field trailer. Samples were filtered with 0.45 micron paper using a millipore filtration unit in combination with nitrogen supplied by a pressurized tank.

All samples were stored in coolers with ice until custody was relinquished to the sample custodian at the field trailer.

Outer parts of the Keck pump and the one-inch bailer, which came into contact with groundwater and were used for sample collection, were cleaned between wells with an Alconox and tap water wash, a tap water rinse, an isopropanol rinse, and two deionized water rinses. The inner parts of the Keck pump and the submersible purge pump were cleaned by pumping distilled water through the system, or in the case of the purge pump, by rinsing the inside and outside several times with distilled water.

Deviations

Wells F-1 and F-3 were purged and sampled with a bailer instead of a Keck pump as described in the sampling plan. A Keck pump was too large to fit in these wells. Using a bailer did not effect the sample integrity.

A 3-inch submersible pump was used to purge the 4-inch diameter wells because a more rapid purging method than a Keck pump was needed to remove the large volume of groundwater from these wells. The purging was followed with sampling accomplished with a Keck pump.

Summary of Results

Twenty-three wells installed in 1977 and 1979 by the U.S.G.S. and ten wells installed by Donohue for this investigation were sampled for groundwater. Large volumes of purge water were required to be removed to purge the required five-well volumes because of the 4-inch diameter and extreme depth (up to 495 feet) of some of the U.S.G.S. wells.

TP/ke

A/R/HIMCO/AG7

WELL DESIGNATIONDEPTH TO SCREEN BOTTOM (in ft.)

B-1	495
B-2	12
B-3	129
B-4	173
CP-1	20
E-2	17
E-3	174
F-1	32
F-2	153
F-3	15
G-1	50
G-3	169
I-1	172
I-2	15
I-3	35
J-1	40
J-2	18
J-3	152
M-1	24
M-2	103
N-1	30
O-1	20
Q-1	20
WT-101A*	18.75
WT-102A*	18.50
WT-103A*	18.50
WT-104A*	18.80
WT-105A*	18.50
WT-106A*	21.25
P-101B*	100.50
P-101C*	167.50
P-102B*	67.90
P-102C*	162.00

* Wells installed by Donohue during this investigation. All others were installed by the U.S.G.S. in 1977 and 1979.

A/R/HIMCO/AG7

APPENDIX A
WELL PURGE AND SAMPLE COLLECTION FORMS

Engineers & Architects

5-1

Method of Purging Pumped _____ Bailed _____

Equipment _____ Airlift _____ N2 Lift _____ In. Bailer _____ Length _____ Ft. Material _____

Pump KOCK Manufacturer _____ Diameter _____ Description of site _____
(weather, temp., soil, conditions)

[illegible]

Notes O-1: $24.5 - 9.16 = 20.34$; $20.34 \times 0.163 = 3.32$; $3.32 \times 5 = 16.6$

Signature [Signature]

Date 1-3-94

P.M./86

Engineers & Architects

Well Purging and Sample Collection

 $\hat{x}-1$

Project No. 2026-223 Site HINO GULF
Method of Purging Pumped ☒ Bailed ☐
Equipment _____ Airlift _____ N2 Lift _____ In. Bailer _____ Length _____ Ft. Material _____
Pump KICK Manufacturer _____ Diameter _____ Description of site INDUSTRIAL STREET, NEXT TO HYDROGEN BRIDGE
(weather, temp., soil, conditions) 41. S. 100' N. 100' E. 20 40'S

[illegible]

Notes: 2" well $C = 163 \times 1872 = 305 = 1$ well volume WC = $2369 - 497 = 1872$ ft

Signature

Date 11-29-50

P.M./86

W. J. 1.9

Project No. 200 26 553 Site H1250 DREF
Method of Purging Pumped ☒ Bailed ☐
Equipment _____ Airlift _____ N2 Lift _____ In. Bailer _____ Length _____ Ft. Material _____
Pump KOK Manufacturer _____ Diameter _____ Description of site GRASSY, MID 3rd CLAY, RUINED
(weather, temp., soil, conditions)

[illegible]

Notes 2nd old calc.
 $0.163 \times 7.19 = 1.17 \text{ gals} = 1 \text{ well vol.}$ $78.70 - 1.17 = 77.53 \text{ ft}$
 $7.44 \times 0.163 = 1.21 \text{ gals} = 1 \text{ well vol.}$

cont'd on p. X.A.5 on 45/3200 m² of

Signature *Robert E. Shaw* Date *1/27/86*

۱۵/۱۲/۴۷

Pump KICK Manufacturer _____ Diameter _____ Description of site IN TREE WINDY MID 30's CLOUDY
(weather, temp., soil, conditions)

Notes: 2" old calc.
 $0.163 \times 7.11 = 1.16 \text{ gal} = 1 \text{ well vol.}$ $1516 - 10.3 = 786 \text{ f.}$
 $0.163 \times 786 = 128 \text{ gals} = 1 \text{ well vol.}$

Signature [Signature] Date 11-20-00

P.M./86

Engineers & Architects

Well Purging and Sample Collection

Project No. 20026, Q23 Site HL7CD DMF
Method of Purging Pumped / Bailed _____
Equipment _____ Airlift _____ N2 Lift _____ In. Bailer _____ Length _____ Ft. Material _____
Pump K&K Manufacturer _____ Diameter _____ Description of site _____
(weather, temp., soil, conditions)

old calc.

Notes $2'' \quad 0.163 \times 12.34 = 2.01 \text{ gal} = 1 \text{ well vol.}$

$2'' \quad 0.163 \times 13.19 = 2.15 \text{ gal} = 1 \text{ well vol.}$

$2'' \quad 18.48 - 5.29 =$

CONFIDENTIAL - A 3 SERGE READING ON YES 3500 m. 100

Signature John Smith Date 11-28-76

P.M./86

Engineers & Architects

WT 104/f

Pump KECK Manufacturer _____ Diameter _____ Description of site GRASS, BARELY, mid 40'S
(weather, temp., soil, conditions)

Well No. Time	Depth to Water	Depth to Bottom	Volume Calculated (gal.)	Volume Removed (gal.)	Depth After	pH	Cond.	Temp	Turbidity Y/N	Comments
WT 104A										
8:20	11.75'	18.90'	1.2 gal	0		7.77	0.088	10.1	slightly	
8:21				2		7.97	0.093	10.8		
8:23				3.5		8.25	0.097	11.0		
8:24				5		8.34	0.098	11.1		
8:26				7.5		8.44	0.100	11.2		
				8		8.49	0.101	11.3		
				9.5		8.53	0.102	11.3	↓	
				11.0		8.55	0.102	11.3	clear	
8:32				12.5		8.56	0.102	11.3	↓	
8:34				14		8.57	0.103	11.3	↓	
8:35	Begin Sampling TAKE Field Duplicate									DO. = 10.0 m/l
8:40	FINISH				11.75					

old c-l.

Notes $0.163 \times 6.32 = 1.03 \text{ g.l} = 1 \text{ well vol.}$

Abu. cal

$$0.163 \times 7.15 = 1.17 \text{ gal} = 1 \text{ well vol.}$$

Conductivity meter on 2 scale reading mS/cm on 4/1 3500 mS/cm

Signature L. L. E. No

Date 11-28-90

P.M./86

Engineers & Architects

WUSA

Method of Purging Pumped ✓ Bailed _____

Equipment _____ Airlift _____ N2 Lift _____ In. Bailer _____ Length _____ Ft. Material _____

Pump K&K Manufacturer _____ Diameter _____ Description of site AT THOSE LIPS, 1/2 30'S, LITE PULL, FT. CND.
(weather, temp., soil, conditions)

[illegible]

Notes 2" well old calc. $0.163 \times 8.32 = 1.36$ gal | well vol $18.52 - 9.72 =$
 $0.163 \times 880 = 1.43$ gal | well vol $WC = 80$

Coastal, 2005, 2006, 2007, 2008, 2009, 2010, 2011, 2012, 2013, 2014, 2015, 2016, 2017, 2018, 2019, 2020, 2021, 2022, 2023, 2024, 2025, 2026, 2027, 2028, 2029, 2030, 2031, 2032, 2033, 2034, 2035, 2036, 2037, 2038, 2039, 2040, 2041, 2042, 2043, 2044, 2045, 2046, 2047, 2048, 2049, 2050, 2051, 2052, 2053, 2054, 2055, 2056, 2057, 2058, 2059, 2060, 2061, 2062, 2063, 2064, 2065, 2066, 2067, 2068, 2069, 2070, 2071, 2072, 2073, 2074, 2075, 2076, 2077, 2078, 2079, 2080, 2081, 2082, 2083, 2084, 2085, 2086, 2087, 2088, 2089, 2090, 2091, 2092, 2093, 2094, 2095, 2096, 2097, 2098, 2099, 2100, 2101, 2102, 2103, 2104, 2105, 2106, 2107, 2108, 2109, 2110, 2111, 2112, 2113, 2114, 2115, 2116, 2117, 2118, 2119, 2120, 2121, 2122, 2123, 2124, 2125, 2126, 2127, 2128, 2129, 2130, 2131, 2132, 2133, 2134, 2135, 2136, 2137, 2138, 2139, 2140, 2141, 2142, 2143, 2144, 2145, 2146, 2147, 2148, 2149, 2150, 2151, 2152, 2153, 2154, 2155, 2156, 2157, 2158, 2159, 2160, 2161, 2162, 2163, 2164, 2165, 2166, 2167, 2168, 2169, 2170, 2171, 2172, 2173, 2174, 2175, 2176, 2177, 2178, 2179, 2180, 2181, 2182, 2183, 2184, 2185, 2186, 2187, 2188, 2189, 2190, 2191, 2192, 2193, 2194, 2195, 2196, 2197, 2198, 2199, 2200, 2201, 2202, 2203, 2204, 2205, 2206, 2207, 2208, 2209, 2210, 2211, 2212, 2213, 2214, 2215, 2216, 2217, 2218, 2219, 2220, 2221, 2222, 2223, 2224, 2225, 2226, 2227, 2228, 2229, 2230, 2231, 2232, 2233, 2234, 2235, 2236, 2237, 2238, 2239, 2240, 2241, 2242, 2243, 2244, 2245, 2246, 2247, 2248, 2249, 2250, 2251, 2252, 2253, 2254, 2255, 2256, 2257, 2258, 2259, 2260, 2261, 2262, 2263, 2264, 2265, 2266, 2267, 2268, 2269, 2270, 2271, 2272, 2273, 2274, 2275, 2276, 2277, 2278, 2279, 2280, 2281, 2282, 2283, 2284, 2285, 2286, 2287, 2288, 2289, 2290, 2291, 2292, 2293, 2294, 2295, 2296, 2297, 2298, 2299, 2300, 2301, 2302, 2303, 2304, 2305, 2306, 2307, 2308, 2309, 2310, 2311, 2312, 2313, 2314, 2315, 2316, 2317, 2318, 2319, 2320, 2321, 2322, 2323, 2324, 2325, 2326, 2327, 2328, 2329, 2330, 2331, 2332, 2333, 2334, 2335, 2336, 2337, 2338, 2339, 2340, 2341, 2342, 2343, 2344, 2345, 2346, 2347, 2348, 2349, 2350, 2351, 2352, 2353, 2354, 2355, 2356, 2357, 2358, 2359, 2360, 2361, 2362, 2363, 2364, 2365, 2366, 2367, 2368, 2369, 2370, 2371, 2372, 2373, 2374, 2375, 2376, 2377, 2378, 2379, 2380, 2381, 2382, 2383, 2384, 2385, 2386, 2387, 2388, 2389, 2390, 2391, 2392, 2393, 2394, 2395, 2396, 2397, 2398, 2399, 2400, 2401, 2402, 2403, 2404, 2405, 2406, 2407, 2408, 2409, 2410, 2411, 2412, 2413, 2414, 2415, 2416, 2417, 2418, 2419, 2420, 2421, 2422, 2423, 2424, 2425, 2426, 2427, 2428, 2429, 2430, 2431, 2432, 2433, 2434, 2435, 2436, 2437, 2438, 2439, 2440, 2441, 2442, 2443, 2444, 2445, 2446, 2447, 2448, 2449, 2450, 2451, 2452, 2453, 2454, 2455, 2456, 2457, 2458, 2459, 2460, 2461, 2462, 2463, 2464, 2465, 2466, 2467, 2468, 2469, 2470, 2471, 2472, 2473, 2474, 2475, 2476, 2477, 2478, 2479, 2480, 2481, 2482, 2483, 2484, 2485, 2486, 2487, 2488, 2489, 2490, 2491, 2492, 2493, 2494, 2495, 2496, 2497, 2498, 2499, 2500, 2501, 2502, 2503, 2504, 2505, 2506, 2507, 2508, 2509, 2510, 2511, 2512, 2513, 2514, 2515, 2516, 2517, 2518, 2519, 2520, 2521, 2522, 2523, 2524, 2525, 2526, 2527, 2528, 2529, 2530, 2531, 2532, 2533, 2534, 2535, 2536, 2537, 2538, 2539, 2540, 2541, 2542, 2543, 2544, 2545, 2546, 2547, 2548, 2549, 2550, 2551, 2552, 2553, 2554, 2555, 2556, 2557, 2558, 2559, 2560, 2561, 2562, 2563, 2564, 2565, 2566, 2567, 2568, 2569, 2570, 2571, 2572, 2573, 2574, 2575, 2576, 2577, 2578, 2579, 2580, 2581, 2582, 2583, 2584, 2585, 2586, 2587, 2588, 2589, 2590, 2591, 2592, 2593, 2594, 2595, 2596, 2597, 2598, 2599, 2600, 2601, 2602, 2603, 2604, 2605, 2606, 2607, 2608, 2609, 2610, 2611, 2612, 2613, 2614, 2615, 2616, 2617, 2618, 2619, 2620, 2621, 2622, 2623, 2624, 2625, 2626, 2627, 2628, 2629, 2630, 2631, 2632, 2633, 2634, 2635, 2636, 2637, 2638, 2639, 2640, 2641, 2642, 2643, 2644, 2645, 2646, 2647, 2648, 2649, 2650, 2651, 2652, 2653, 2654, 2655, 2656, 2657, 2658, 2659, 2660, 2661, 2662, 2663, 2664, 2665, 2666, 2667, 2668, 2669, 2670, 2671, 2672, 2673, 2674, 2675, 2676, 2677, 2678, 2679, 2680, 2681, 2682, 2683, 2684, 2685, 268

Signature [Signature]

Date 1-29-60

P.M./86

Engineers & Architects

Well Purging and Sample Collection

۱۲۶۱

Project No. 20026 023

Site Himco Dump

Method of Purging Pumped ^x Bailed

Equipment Keck Airlift _____ N2 Lift _____ In. Bailer _____ Length _____ Ft. Material _____

Pump _____ Manufacturer Johnson Diameter _____ Description of site h.m.d. 50's-60's, scattered ruins
(weather, temp., soil, conditions)

[illegible]

NOTES 2" well $\pi r^2 (748) = 0.163$ $0.163 \times 9.09 = 1.4 \text{ gal}$
he $0.163 \times 90 \text{ ft} = 1.46 = 1.5 \text{ gal/ft}$ 1 well vol.

Signature Steve Spang E. Shm Date 11-27-90

P.M./86

P.M./86

Engineers & Architects

Well Purging and Sample Collection

P-101C

Project No. 20026.023 Site Hince Dump

Method of Purging Pumped / Bailed _____

Equipment _____ Airlift _____ N2 Lift _____ In. Bailer _____ Length _____ Ft. Material _____

Pump _____ Manufacturer Keck Diameter 1.75" Description of site cold, cloudy, scattered
(weather, temp., soil, conditions)
snow, low 30s

[illegible]

Notes $2'' \text{ well} = 153.6 \times 0.163 = 25.04$ $w_c = 163.0 - 9.4 = 153.6$

* Very muddy bottom, hard to tell may have ~2 or 3' of Sediment

Conductivity readings on 2 scale in mS/cm

Signature

Eni & Alun

Date 11/9/91

7M./86

Engineers & Architects

Well Purging and Sample Collection

WT
~~WT~~ - 106 A
 (2) c/cos/h)

Pump X Manufacturer Keck Diameter 1.75 Description of site col'd cloudy mid 20s
(weather, temp., soil, conditions)

[illegible]

Notes: 2" well $11.50 \times 0.163 = 1.87 = 1$ well vol $wd 8.60 - 7.10 = 1.50$

Conductivity reading on 2 scale in mS/cm

Signature M. D. [illegible]

Date 1-8-91

P.M./86

Donohue

Well Purging and Sample Collection

Site Hinc. D.

✓

Pump Y Manufacturer K&K Diameter 1.75 Description of site cold, clay, mod. sw.
(weather, temp., soil, conditions)

47

Conductivity on 2 scale in mS/cm

Signature E. D. Hesse

Date 1/8/91

P.M./86

P-102 C

118-104

-8-91

P.M./86

Donohue

Well Purging and Sample Collection

Pump 10 Manufacturer Keck Diameter 1.75 Description of site Shady cold mid 20s
(weather, temp., soil, conditions)

P.M./86

Engineers & Architects

Well Purging and Sample Collection

N/T-10.2A

Project No. 20026.023

Site Hanco Dump

Method of Purging Pumped ✓ Bailed.

Equipment _____ Airlift _____ N2 Lift _____ In. Bailer _____ Length _____ Ft. Material _____

Pump K Manufacturer Keck Diameter 1.75 Description of site Cold 5-11, 12 & 20' wind
(weather, temp., soil, conditions)

South 45 mph, just up to 10 mph

[illegible]

Notes: $0.163 \times 871 = 142 = 1$ well vol

$$WC = 18.16 - 9.45 = 8.71$$

Conductivity Reading on 2 scale in mS/cm

Signature

Ein D. Schum

Date _____

1-7-91

P.M./86

TECHNICAL MEMORANDUM NUMBER 9

DATE: January 28, 1991
TO: Vanessa Harris - Site Manager
CC: Marcia Kuehl - RI Lead
Roman Gau - Project Manager
Mike Crosser - TSQAM
FROM: Tom Puchalski
SUBJECT: EPA ARCS Region V Contract No. 68-W8-0093
EPA Work Assignment No. 17-5L4J
Donohue Project No. 20026.024
Himco Dump RI/FS

ORIGINAL

SURFACE WATER/SEDIMENT SAMPLING

Introduction

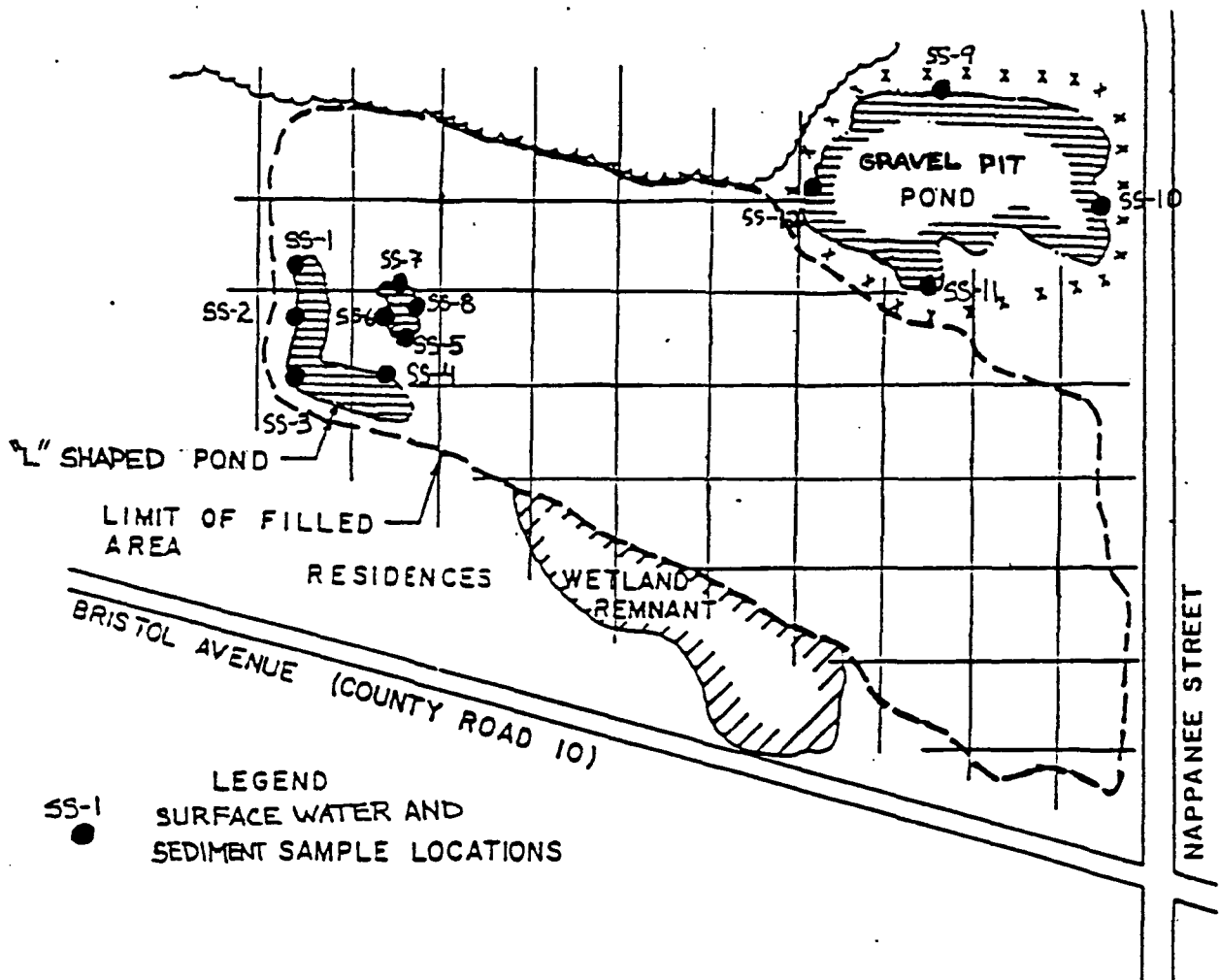
Surface water and sediment samples were taken at four locations at each of the three ponds at the Himco Dump Site in Elkhart, Indiana, to investigate the degree and extent of surface water and sediment contamination. Sampling was done by Eric Slusser and Tom Puchalski of Donohue & Associates, Inc., on October 17, 18, 19, and 20, 1991. This memorandum describes the sampling methods used in the field as compared to the methods described in the Final Field Sampling Plan.

Methods

Three surface water bodies are present at the Himco Dump Site. The two smaller ponds are located at the southwestern portion of the site. The larger of these two ponds is "L"-shaped with the longer channel oriented north-south and the shorter channel oriented east-west. Both channels of the "L"-shaped pond are approximately 100 feet wide and 400 feet long. The smaller pond is directly northeast of the "L"-shaped pond and is approximately 100 by 170 feet. The shorelines and bottoms of these two ponds are generally gravel and sand. Their depths are unknown, but because they were excavated with a backhoe, they are assumed to be less than 15 feet deep.

The gravel pit pond is the largest surface water body on-site. It is located in the northeast corner of the study area. It is approximately 850 feet wide in the east-west direction and 400 to 550 feet wide in the north-south direction. The depth of the gravel pit pond is unknown. The shoreline and bottom is generally gravel and sand.

The four locations at each of the three ponds were selected so that the north, south, east, and west shorelines were sampled (Figure 1). A description of the sampling location was written on the surface water and sediment field data form (Appendix A). A photograph was taken of each sample location.



SOURCE: US EPA, AUGUST, 1986

Donohue APPROXIMATE SITE SAMPLING LOCATIONS

20026

FIELD SAMPLING PLAN
HIMCO DUMP SITE
ELKHART, INDIANA

FIGURE 1

Engineers • Architects • Scientists

The surface water samples were collected before the sediment samples and on different days at all locations. Surface water was collected by lowering the capped sample bottle below the surface and opening it under water to allow the sample to trickle in. The bottle was then capped under water and brought back up out of the water. The water sample was put in a cooler with ice to be transported to the field trailer. Readings of pH, conductivity, temperature, and dissolved oxygen were taken in the back of a pickup truck at the edge of the pond immediately after carrying them from each location (Table 1).

Sediment samples were collected at the same locations as were surface water samples at approximately 2 to 3 feet offshore at water depths which ranged from 0 to 2 feet. A shovel was used to collect the sample from approximately 0 to 4 inches. Sediment samples were placed in a stainless steel bowl, and the excess water was poured off. Grab samples for volatile analysis were immediately placed in two 4-oz. jars with no headspace. The remainder of the sample was mixed using a stainless steel spoon. The resultant homogeneous mixture was spread evenly in the bowl. The sediment was divided into four quadrants. Small portions were taken from each quadrant for each jar until the remaining jars were filled. A visual description, including texture and color, was written on the field data form.

The shovel, sample composite bowl, and mixing spoon were decontaminated between sample locations by:

1. Alconox and tap water wash.
2. A tap water rinse.
3. An isopropanol rinse.
4. Two deionized or distilled water rinses.

Isopropanol rinsates were collected in a 5-gallon bucket and covered until eventual discharge into the on-site frac tank.

Deviations

A shovel was used instead of a bucket to collect the sediment sample because the sediment was consolidated by plant roots in some locations to the degree that a bucket could not scrape up the required sample volume.

Summary of Results

Twelve surface water and twelve sediment samples were collected. No visual evidence of contamination was apparent in any of these samples. Figure 1 shows the surface water/sediment sampling locations, and Appendix A contains the surface water and sediment field data forms, which describe the appearance of the samples.

TP/ke

A/R/HIMCO/AB4

TABLE 1

<u>Sample Number</u>	<u>Date</u>	<u>T° F</u>	<u>pH</u>	<u>Conductivity ms/cm</u>	<u>DO mg/l</u>
SS-1	10/17/90	69	8.11	792	6
SS-2	10/18/90	50.2	8.02	753	9
SS-3	10/18/90	48.5	8.31	704	8.4
SS-4	10/18/90	49.8	8.27	707	8.6
SS-5	10/18/90	49.6	7.93	534	8.4
SS-6	10/18/90	49.4	7.58	538	5.8
SS-7	10/18/90	48.3	7.06	431	3.2
SS-8	10/19/90	46.8	8.06	471	7.2
SS-9	10/19/90	55.6	8.06	637	7.2
SS-10	10/19/90	60.0	7.99	659	6.4
SS-11	10/19/90	61.7	8.00	693	6.7
SS-12	10/19/90	61.7	8.00	693	6.7

A/R/HIMCO/AB4

APPENDIX A

SURFACE WATER AND SEDIMENT FIELD DATA FORMS

Donohue

SURFACE WATER FIELD DATA

SITE IDENTIFIER NUMBER

SEDIMENT

CONTAMINATION SURVEY

(SB-1) 50-C

Engineering & Architecture

WATER
 DATE 10/17/90
 TIME 8:00 AM
 COLLECTOR Tom Puchalski
Eric Slusser

SEDIMENT
 DATE 10/17/90
 TIME 1140
 COLLECTOR Tom Puchalski
Eric Slusser

WATER DEPTH 1-foot
 pH 8.11
 TEMPERATURE OF WATER 69°F
 COLOR Clear
 ODOR None
 CLARITY Clear - some vegetation
 COND 792 μ S/cm
 DO 6 ml/l

SAME LOCATION

SEP 10/17/90
 Lt brown
~~Gray Sand, Black Muck Mix~~
H₂S None

PHYSICAL DESCRIPTION OF SAMPLING POINT NW corner of large L shaped fish
pond 15' east of corner 3' off of north shore.

ANY OTHER CHARACTERISTICS OF NOTE Sediment is light brown medium sand
with a trace of shaly 3/4" pebbles.

Donohue

SURFACE WATER FIELD DATA

SITE IDENTIFIER NUMBER

SEDIMENT

CONTAMINATION SURVEY

SS-2 SD-02

E. Donohue & Associates, Inc.

SEP 10/17/90 WATER
 DATE 10/17/90 10/18/90
 TIME 800 AM

COLLECTOR ERIC SLUSSE
TOM PUCHALSKI
DOROTHEA DOWNS

SEDIMENT

10/17/901440TOM PUCHALSKIERIC SLUSSEWATER DEPTH 2'pH 8.02TEMPERATURE OF WATER 50.2COLOR ClearODOR NoneCLARITY Clear - Non turbidCOND 753 ms/cmDO 9 mg/l

PHYSICAL DESCRIPTION OF SAMPLING POINT 125' south of north shore of L shaped
fish pond off of the west bank. Sandy marly dropoff.

SAME LOCATION

SEP 10/17/90
lt brown Grey sand, black
None H₂S

ANY OTHER CHARACTERISTICS OF NOTE Sediment is organic rich

Donohue

SURFACE WATER FIELD DATA
& SEDIMENT CONTAMINATION SURVEY

SITE IDENTIFIER NUMBER

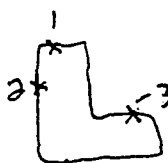
(SS-3) SD-C

Engineering & Architecture

WATER
 DATE 10/18/90
 TIME 8:15
 COLLECTOR ERIC SLUSSER
TOM PIXHALSKI
DOROTHEA DOWNS

SEDIMENT
10/17/90
3:30 p.m.
TOM PIXHALSKI
ERIC SLUSSER

WATER DEPTH 1'
 pH 5.8 48.5°F 8.31
 TEMPERATURE OF WATER 48.5°F
 COLOR Clear
 ODOR None
 CLARITY Clear - Non turbid
 COND 704
 DO 8.4



Lt Brown Sand
None

PHYSICAL DESCRIPTION OF SAMPLING POINT southeast corner of L shaped fish
pond 3' south of shore for sediment 1' off shore for
surface water

ANY OTHER CHARACTERISTICS OF NOTE Sandy gravel shoreline

Donohue

SURFACE WATER FIELD DATA

SITE IDENTIFIER NUMBER

& SEDIMENT

CONTAMINATION SURVEY

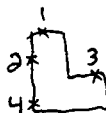
(SS-4) SD-0

Engineers & Architects, Inc.

WATER

DATE 10/18/90TIME 8:35 A.M.COLLECTOR ERIC SLUSSERTOM PUCHALSKIDOROTHEA DOWNS

SEDIMENT

10/18/901415SLUSSERPUCHALSKIWATER DEPTH 1-footpH 8.27TEMPERATURE OF WATER 49.8COLOR ClearODOR NoneCLARITY Clear707
8.61-footBrownNone

PHYSICAL DESCRIPTION OF SAMPLING POINT SW corner of large L shaped fish pond
1-foot off west shore. Water depth drops off to 5' close to shore.

ANY OTHER CHARACTERISTICS OF NOTE Sediment consists of medium grained sand in
gravelly sand gravel 3/4 - 1/2" sng. Some marl.

Donohue

SURFACE WATER FIELD DATA

SITE IDENTIFIER NUMBER

Environments & Analytics, Inc.

& SEDIMENT

CONTAMINATION SURVEY

SS-05
SD-05

WATER		SEDIMENT
DATE	10/18/90	10/18/90
TIME	10:55 AM	1445
COLLECTOR	ERIC SLUSSER	SLUSSER
	TOM PUCHALSKI	PUCHALSKI
	DOROTHEA DOWNS	
WATER DEPTH	1'	2'
pH	7.93	
TEMPERATURE OF WATER	49.6	
COLOR	Clear	Brown sand, black muck
ODOR	None	H ₂ S
CLARITY	Clear - Non turbid	
COND	534 μ S/cm	
DO	8.4 mg/l	
PHYSICAL DESCRIPTION OF SAMPLING POINT Middle of south shore of small pond near fish pond		

ANY OTHER CHARACTERISTICS OF NOTE Sediment - Gravelly sand & muck, gravel - most 1/2" sandy, sand med grn.

Donohue

SURFACE WATER FIELD DATA

SITE IDENTIFIER NUMBER

EXPERIMENT & ANALYSIS

SEDIMENT

CONTAMINATION SURVEY

SS-06
SD-06WATER
DATE 10/18/90

TIME 11:15 AM

COLLECTOR ERIC SLUSSER

TOM PUCHALSKI

DOROTHEA DOWNS

SEDIMENT

10/20/90

805

TOM PUCHALSKI

ERIC SLUSSER

WATER DEPTH 1'

pH 7.58

TEMPERATURE OF WATER 49.4

COLOR Light brown to clear

ODOR None

CLARITY Slight turbid

COND 538

DO 5.8

PHYSICAL DESCRIPTION OF SAMPLING POINT ≈ 25 feet south of north shore of small pond near
 L shaped fish pond on west bank $\approx 2'$ offshore

ANY OTHER CHARACTERISTICS OF NOTE Sediment sample is gravelly sand, light brown
 medium sand 75%, angular, coarse angular sand 10%, 15% 1/2" shaly
 gravel

Donohue

SURFACE WATER FIELD DATA

SITE IDENTIFIER NUMBER

2 SEDIMENT

CONTAMINATION SURVEY

55-07
507

WATER
 DATE 10/18/90
 TIME 1135 AM
 COLLECTOR DOROTHEA DOWNS
ERIC SLUSSER
TOM PUCHALSKI

SEDIMENT
10/20/90
834 AM
TOM PUCHALSKI
ERIC SLUSSER

WATER DEPTH 1'
 pH 7.06
 TEMPERATURE OF WATER 48.3°F
 COLOR Light brown
 ODOR Slight H₂S
 CLARITY Slight turbid
 COND 431
 DO 3.2

1'
Grey
Strong H₂S

PHYSICAL DESCRIPTION OF SAMPLING POINT

Middle of north shore of small pond in cattails.
Sheen on water - metallic grey.



ANY OTHER CHARACTERISTICS OF NOTE

Sediment is fine grained angular sand
with a trace of sbrd gvl x 1/4" dia. SM - Silty sand 20% sand

Donohue

SURFACE WATER FIELD DATA

SITE IDENTIFIER NUMBER

SEDIMENT

CONTAMINATION SURVEY

Experiments & Analysis

95-08
57-08

SURFACE WATER

DATE 10/19/90

TIME 820

COLLECTOR TOM PUCHALSKI

ERIC SLUSSER

SEDIMENT

10/20/90

920

TOM PUCHALSKI

ERIC SLUSSER

WATER DEPTH 8"

pH 8.06

TEMPERATURE OF WATER 46.8

COLOR Clear

ODOR None

CLARITY Clear

COND 471

DO 7.2

PHYSICAL DESCRIPTION OF SAMPLING POINT east shore of small pond north of L shaped fish pond midpoint of shore

Grey
None

ANY OTHER CHARACTERISTICS OF NOTE Slight sheen on water - non iridescent

Donohue

SURFACE WATER FIELD DATA

SITE IDENTIFIER NUMBER

CONTAMINATION SURVEY

SS-04
SD-09

EMPLOYERS & AGENTS

WATER

SEDIMENT

DATE 10/19/9010/20/90TIME 10001050COLLECTOR TOM PUCHALSKITOM PUCHALSKIERIC SLUSSERERIC SLUSSERDOROTHEA DOWNSWATER DEPTH 1'pH 8.06TEMPERATURE OF WATER 55.6COLOR Clear10YR 5/3 BrownODOR NoneNoneCLARITY ClearCOND 637DO 7.2PHYSICAL DESCRIPTION OF SAMPLING POINT Midpoint of north shore of quarry 2 feet offshoreANY OTHER CHARACTERISTICS OF NOTE sediment is silt, sand (sn) with a trace of 1/2" sbrd gvl

Donohue

SURFACE WATER FIELD DATA

SITE IDENTIFIER NUMBER

& SEDIMENT

CONTAMINATION SURVEY

SS-10
SD-10

FEDERATION OF ARCHITECTS

WATER

SEDIMENT

DATE 10/19/9010/20/90TIME 10201118 AMCOLLECTOR ERIC SLUSSERTOM PUCHALSKITOM PUCHALSKIERIC SLUSSERDOROTHEA DOWNSWATER DEPTH 1'1'pH 7.99TEMPERATURE OF WATER 60.0COLOR Clear10 YR 5/3 BrownODOR NoneNoneCLARITY ClearCOND 659 μ S/cmDO 6.4 μ S/cm mg/lPHYSICAL DESCRIPTION OF SAMPLING POINT Midpoint of east shore at quarry 2' offshore

ANY OTHER CHARACTERISTICS OF NOTE Sediment is silty sand (sn) with a trace of
1/4" sand gravel.

Donohue

SURFACE WATER FIELD DATA

SITE IDENTIFIER NUMBER

& SEDIMENT

CONTAMINATION SURVEY

SS-11
SD-11

E. J. Donohue & Associates, Inc.

WATER
 DATE 10/19/90
 TIME 1050
 COLLECTOR TOM PUCHALSKI
ERIC SLIKSER
DOROTHEA DOWNS

SEDIMENT
10/20/90
1150
TOM PUCHALSKI
ERIC SLIKSER

WATER DEPTH 1-foot1-footpH 8.00TEMPERATURE OF WATER 61.7COLOR ClearODOR NoneCLARITY ClearCOND 693DO 6.7

PHYSICAL DESCRIPTION OF SAMPLING POINT 2 feet off south shore of Quarry near
midpoint of shore in bay near fence gate at south of quarry

10 YR 5/3 Brown & N2/Black
None

ANY OTHER CHARACTERISTICS OF NOTE Sediment is GW gravelly sand 70%
1/2-1/4" shd. gr., 30% fn. gr. and sand some black silt in
areas mixed with gravelly sand.

Donohue

SURFACE WATER FIELD DATA

SITE IDENTIFIER NUMBER

SEDIMENT

CONTAMINATION SURVEY

55-12
5D-12

EXPOSURE & ANALYSIS

WATER
DATE 10/19/90TIME 1110COLLECTOR TOM PUCHALSKIERIC SLUSSERDOROTHEA DOWNSWATER DEPTH 1'pH 8.00TEMPERATURE OF WATER 61.7°FCOLOR ClearODOR NoneCLARITY ClearCOND 693 μ S/cmDO 6.7 mg/lPHYSICAL DESCRIPTION OF SAMPLING POINT Midpoint of west shore of quarry ~2 feet
off shore

SEDIMENT

10/20/901227TOM PUCHALSKIERIC SLUSSER1'104R S/B BrouseNoneANY OTHER CHARACTERISTICS OF NOTE sediment is gravelly sand, 70% fr grained
angular sand 30% shrd gvl '4-1/2", some 3"-not included
in samples

ORIGINAL

TECHNICAL MEMORANDUM - NO. 10

DATE: January 29, 1991

TO: Vanessa Harris - Site Manager

CC: Marcia Kuehl - RI Lead
Roman Gau - Project Manager
Mike Crosser - TSQAM

FROM: Tom Puchalski

SUBJECT: EPA ARCS Region V Contract No. 68-W8-0093
EPA Work Assignment No. 17-5L4J
Donohue Project No. 20026.024
Himco Dump

TEST PITS

Introduction

Twenty test pits were excavated at the Himco Dump Site in Elkhart, Indiana, on November 28, 29, 30, and December 1 to determine if metal drums are buried at the site. All excavations were carried out in Level B personal protection. Excavations were dug by Chris Goodwin and Mike Donohue of John Mathes and Associates, Inc. Air monitoring of the excavation and logging of the pit were done by Tom Puchalski of Donohue & Associates, Inc. Perimeter monitoring downwind of the excavation was done by Anya Kyrkowicz of Donohue & Associates, Inc. The purpose of this memo is to describe the test pit excavation methods and results as they relate to the Final Field Sampling Plan.

Methods

Test pit excavation locations were determined by Rob Stenson and Tom Puchalski of Donohue & Associates, Inc., from a magnetic anomaly map produced for the site by STS Consultants. Excavation procedures are described in Section 4.9 of the Final Field Sampling Plan, Himco Dump Remedial Investigation/Feasibility Study, Elkhart, Indiana.

A separate memorandum provided by STS Consultants describes the field and data evaluation methods they used to perform the EM, Magnetic survey, and produce anomaly maps (Appendix A).

Once the locations of the test pits were determined and marked on the magnetic anomaly map, their locations were staked in the field by reference to the site survey grid stakes. After defining the work zone with caution tape and setting up the Level B equipment, the excavation was ready to begin. As the excavation proceeded, the Donohue geologist described the types of waste and soil being excavated by completing a trench log. Readings on air monitoring equipment were periodically recorded on an atmospheric monitoring log. Air monitoring was also performed continuously by a second person at the downwind side

of the excavation outside of the work zone. Readings on a PID and OVA, H₂S, %O₂, LEL, and CO were all monitored. Photographs were taken of large metal objects or other objects of significance. The bottom of the pit was defined by reaching the water table or approximately 15 feet, whichever was shallower. Upon completion of the pit, a measuring tape was used to define the depth of the excavation and the depths to any significant waste or soil horizons. Following the completion of trench logs, the excavation was immediately backfilled. Prior to surveying in the trench locations, all were staked with wooden lath and survey tape.

Upon demobilization from the site, the backhoe was decontaminated by steam cleaning at the decontamination pad. Wastewater generated from steam cleaning activities was collected by the decontamination pad and pumped by sump pump from the collection pit to the on-site frac tank.

Deviations

The backhoe was decontaminated once before demobilization from the site. Decontamination was not required upon mobilization or in between test pit locations as described in the Final Field Sampling Plan because no sampling for chemical analysis was performed, and all test pit locations were on-site in areas of former waste disposal.

Summary of Results

Twenty test pit locations were excavated. Each test pit was twenty-five feet long. Some test pit locations were along the same direction and a direct extension of adjoining test pits, in some cases, producing up to a 100-foot long continuous trench. Test pit locations are provided in Figure 1. Completed test pit log forms are included in Appendix B.

Other than a few scarce 55-gallon drum lids, one rusted and crushed 55-gallon drum which may have been a burn barrel for garbage, and a few 25-gallon crushed drums, no significant buried drums were discovered. Other metallic objects were discovered which can account for the observed magnetic anomalies. Excavated metallic objects consist of scrap metal strips and angle iron, pipes, sheet metal, refrigerator condensers, wire, lawn mower parts, car bumpers, metal boxes, car mufflers, and pails.

A summary of the information contained in the trench logs and atmospheric monitoring logs follows.

Trench 1-4

Trenches 1-4 were excavated from northeast to southwest adjacent to each other to form one long 100-foot trench along hummocky terrain. Two iron beams, concrete, and metal pipe was protruding from the ground surface in several places. Grass covered hummocks were approximately six feet higher than the surrounding terrain. The spoils were piled on the down-wind east side of the trench. The trench was originally approximately 5 feet wide but this dimension widened to 10 feet at the north and south 25 feet due to cave-in. The trench depth varied from 6 feet on the northeast end to 12 feet on the southwest.

The stratigraphy of TP-1 through TP-4 can be summarized as follows. A thin 0.5 to 2.0-foot layer of silty sand topsoil fill overlies a white calcium sulfate layer which grades to black at its base. The calcium sulfate layer pinches out in TP-2 but is present as a brown and white silt layer in TP-3. It was not present in TP-4, but is correlative with black and white stringers 2 to 0.5 feet thick.

Municipal waste, from 2 to 5 feet thick, described in detail in the trench log, is present below the calcium sulfate. Water began flowing into the trench at 7 feet so the trench was not excavated deeper on this end. As the trench excavation proceeded south, no new water sources began flowing. TP-2, therefore, was excavated deeper to 11 feet. The waste layer pinched to about one foot thick in TP-2.

Metal objects were found which can explain the anomaly mapped for this area. Scrap metal strips, steel I-beams, metal pipe, sheet metal, and two drum lids were found within the waste layer in TP-1, 2, 3, and 4.

Air Monitoring

Air monitoring of TP-1 through TP-4 produced a high reading of 30 to 40 ppm and a low of 2 ppm on an OVA. No positive readings were produced on the PID, radiation detector, or lumidor. OVA readings down-wind of the trench at the work zone boundary were sporadic. Reading between 10 and 60 ppm lasted about 5 seconds spaced 1 to 2 minutes apart. Readings were not detected 250 feet down wind of the trench.

Trench 5-6

Trenches 5 and 6 were excavated adjoining one another to form one 50-foot trench oriented north-south. This trench was located in hummocky grass covered terrain similar to the location of TP1-TP4. Excavation spoils were piled on the eastern (down wind) side of the trench. The trench width was 5 feet. The depth extended to 14 feet.

The first foot of the profile of these two trenches consist of brown silty sand topsoil fill. Below the topsoil is calcium sulfate which varied in thickness from one to 9 feet. Below the calcium sulfate lenses is black silty sand with wood, plastic wrap, and sheet metal distributed throughout.

The water table was not reached in this excavation. The water source at the north end of TP-5 was perched water contained within the void space of the waste layer from 2-6 feet.

The majority of the metal objects were found at 8 feet in TP-5 and 6. The objects consist primarily of sheet metal. A small metal oven or refrigerator was excavated from TP-6 near the north end at approximately 8 feet.

Atmospheric Monitoring

The OVA was the only air monitoring instrument which had readings above background. Readings from 30 to 100 ppm were registered at the excavation. Downwind perimeter monitoring registered 20-30 ppm, 50 feet from the trench (east), 2 to 3 ppm, 150 feet east,

and 0 at 250 feet. Higher readings averaging 30 to 40 ppm and instantaneous sporadic readings greater than 100 ppm were observed at the 6-foot depth in TP-5.

Trench 7-8

Trenches 7-8 were excavated adjoining one another to form one north-south trench extending 50 feet. These two trenches were excavated approximately 5 to 7 feet wide and stopped at 12 feet where the water table was encountered. The water table was reached before the bottom of the waste; groundwater is flowing through the waste at this location.

The silty sand topsoil is only a few inches thick at this location. Below the topsoil is about 1 feet of calcium sulfate. From 1 foot to the bottom of the pit at 12 feet is mixed waste consisting of paper, wood, fiber templates, plastic bags, black sand, Alka-Seltzer wrappers, bottles and caps, toothpaste samples, and glass bottles.

Metal objects include one unmarked 55-gallon and one unmarked 25-gallon drums. More significant metal objects include metal pipe found at 2 feet in TP-8, car bumpers, refrigerator compressors, sheet metal, and aerosol cans. Markings on aerosol cans suggests one source as Sudden Beauty hair spray and Dristan Hay Fever Spray were most common. Three 55-gallon drum lids were also found. Only one had legible markings marked "Aliphatic Resin."

Native yellow brown sand was encountered near the south end of TP-8 from the surface to the base of the excavation at 12 feet.

Atmospheric Monitoring

Sporadic readings of up to 700 ppm were observed on the OVA. Thirty-two ppm H₂S were observed on the lumidor which periodically set off the instrument alarm. H₂S readings were also sporadic; readings were highest during excavation of calcium sulfate. Perimeter monitoring of the downwind side of the trench exhibited readings of 30 to 50 ppm on the OVA at the work zone tape, and 3 to 6 ppm at 75 feet downwind of the work zone tape.

Trench 9

Trench 9 was excavated from northeast to southwest extending 25 feet. The ground surface at this area is flat and sparsely grass covered. Calcium sulfate is present at the ground surface. The silty sand topsoil is approximately 6 inches thick. Below this thin layer of topsoil is 2.5 feet of calcium sulfate. From 3 to 5 feet, waste was excavated consisting of tires, wood, paper, black sand, Alka-Seltzer wrappers, rubber 1/8-inch bands, and plastic bags.

Few metal objects were excavated from this pit. Three unmarked 55-gallon drums lids and bundles of wire were excavated at about 4 feet.

A lower calcium sulfate layer extends half way across the trench from the northeast end from 5 to 8 feet in depth. Mixed paper and plastic waste make up the majority of the waste from 8 to 12 feet. The water table was encountered at 12 feet where the excavation stopped.

The lower limit of the waste was not reached before the water table was encountered. Groundwater is flowing through waste at this location. As the bottom of the trench filled with groundwater, gas was bubbling up through the water originating from the waste at the base of the trench.

Atmospheric Monitoring

Readings of up to 500 ppm were observed on the OVA during the excavation of TP-9. Most of the OVA readings were from 20 to 100 ppm at the trench. Readings of H₂S up to 38 ppm were observed during excavation and piling of calcium sulfate at the surface. Perimeter monitoring at the downwind border of the work zone exhibited OVA readings ranging from 2 to 90 ppm. Readings 100 feet further downwind were 2 to 7 ppm, and readings 200 feet downwind were 0.8 to 3 ppm. No perimeter readings above background were detected for H₂S or any other monitored parameters.

Trench 10-11

Trenches 10-11 were excavated oriented north-south with TP-10 on the north adjoining TP-11 on the south to form one 50-foot long trench. Spoils were piled on the east side of the trench.

TP 10-11 is located in a partially grass-covered area. The topsoil is about 1 foot thick consisting of yellow brown silty sand. A lens of waste extends about 12 feet south of the north boundary of TP-10. The lens is approximately 2 feet thick and consists of plastic bags, glass and plastic bottles, wood, and paper. The rest of the trench consists of white, black, and gray layers of calcium sulfate. A few scarce 1"x5" boards were found scattered throughout the calcium sulfate. Groundwater was encountered at 8 feet before the base of the calcium sulfate was reached. Very little metal was discovered in this trench. One piece of sheet metal was located 10 feet south of the north edge of TP-10 at 3 feet.

Atmospheric Monitoring

Positive readings of H₂S and OVA were observed during excavating of TP 10-11. No other instruments had readings above background. OVA readings ranged from 10 to 200 ppm at the trench and 0 to 90 ppm downwind of the trench at the work zone tape. H₂S readings ranged from 2 to 14 ppm at the trench with no H₂S detected downwind of the trench outside of the work zone.

Trench 12-13

TP 12-13 were excavated at the south end of the landfill cap at a relatively flat grass-covered area. Two 25-foot long, 5-foot wide trenches were oriented along a northeast trend and adjoined to create one 50-foot long trench. Excavation stopped at 10 feet when the water table was encountered.

Approximately 6 inches of yellow brown silty sand topsoil fill was found covering about 7.5 feet of white calcium sulfate. Some of the fracture faces of the calcium sulfate were yellow. This may relate to the H₂S atmospheric readings obtained during excavation of this material. This layer is relatively thick in this trench when compared to other trenches excavated on-site. At 8 feet, a 1-foot thick layer of waste was encountered within the

calcium sulfate. The waste consists of wood and paper with lesser amounts of sheet metal, rubber sheets, and Alka-Seltzer wrappers. Groundwater was observed to be pouring out of void spaces associated with the waste layer. This black groundwater poured into the bottom of the trench as the excavation proceeded. Gases were observed bubbling up through the groundwater from the calcium sulfate at the base of the trench.

Atmospheric Monitoring

Positive readings of H₂S and readings on the OVA were observed during trenching of TP 12-13. H₂S readings range from 1 to 46, averaging about 7 at the trench. No downwind H₂S was detected during perimeter monitoring outside the work zone. OVA readings range from 20- greater than 1,000 ppm, averaging about 200 ppm at the trench. Perimeter OVA ranged from 10 to 50 ppm, with average readings about 10 ppm. Readings of 1.5 to background were observed 100 feet downwind of the trench.

Trench 14-15

TP 14-15 were excavated at the southwest edge of the landfill cap at a grass-covered flat area immediately west of the slope east up to the top of the landfill cap. The western boundary of fill was excavated at TP 14-15. Two 25-foot long trenches were oriented east-west and adjoined to make one 50-foot long excavation. Spoils were piled on the north side of the trench. The trench was excavated to 5 feet wide, but sloughing of the sidewalls during excavation widened the trench to up to 15 feet in places.

The stratigraphic profile begins with approximately 1-foot of brown to yellow brown silty sand topsoil. Below this layer is a 1 foot thick layer of white to gray hardened calcium sulfate. Native sand was encountered from 2 to 9 feet. Several zones of black sand approximately 6 inches thick and 6 feet long were found throughout the buff to brown native sand. No water was encountered in TP-14. As the excavation proceeded east, the depth was decreased to 6 feet since no fill material was present below the calcium sulfate at one to two feet. At the eastern-most edge of TP-15, wood debris, a refrigerator compressor, metal pipe, and sheet metal debris were discovered at about 4 feet in depth. Groundwater began pouring out of this area of debris and proceeded to fill the trench with water. Backfilling of the trench began as soon as the water began pouring out. By the time the backfilling was complete, there was excess volume of groundwater which was displaced by backfill material so that a several inch deep by 30-foot wide puddle was left at the west end of TP-14 on the ground surface.

Atmospheric Monitoring

No abnormal readings were observed other than OVA detections. The OVA readings ranged from 1 to 400, averaging less than 20 ppm. Downwind perimeter OVA readings ranged from 0 to 90 ppm, averaging sporadic readings of 20 ppm. OVA readings were sporadic from 1 to 5 ppm 100 feet downwind. The absence of H₂S readings during the excavation of this trench may be related to the relatively little amount of calcium sulfate encountered.

Trench 16

One 25-foot long trench was oriented on a northwest trend at this location. Approximately one-half foot of brownish yellow fine-grained silty sand topsoil was found overlying a one-foot thick layer of calcium sulfate. Waste was excavated below the calcium sulfate. The waste consists of black wood, paper, plastic and glass bottles, rubber, plastic bags, and smaller amounts of sheet metal, metal pipe, and an empty gas container from a small engine. Black groundwater was reached at 4 feet so the excavation stopped at this depth. A few extra scoops were excavated to 6 feet at the southeast end of the trench. These saturated spoils were not removed, but piled in the northwestern end of the trench. This extra excavation was done to attempt to define the lower limit of the waste. Waste continued beyond 6 feet deep.

Atmospheric Monitoring

Reading of H₂S and positive readings on the OVA were observed during excavation of TP-16. H₂S readings range from 2 to 27 ppm at the trench, but were not detected downwind outside of the work zone. OVA readings ranged from 10 to 500 ppm. Perimeter OVA readings ranged from background to 12 ppm. No OVA readings were observed 50 feet downwind of the trench.

Trench 17

Trench TP-17 is oriented on an east-west trend extending 25 feet. The trench was approximately 5 feet wide. A thin (several inch) layer of yellow brown silty sand topsoil fill covers an 8-inch thick layer of calcium sulfate. Below the calcium sulfate, waste was encountered. Approximately 80 percent of the waste is rubber sheets and bands with minor paper, wood, glass bottles, and minor corroded sheet metal and aluminum bars at less than 2.5 feet. Groundwater was encountered at 2 feet in TP-17, so the excavation was stopped at this depth.

Atmospheric Monitoring

OVA readings up to 2 ppm were observed during trenching of TP-17. No other readings were observed above background on any air monitoring instruments either at the trench or downwind of the trench at the work zone perimeter.

Trench 18

TP-18 is oriented along an east-west trend. The excavation was approximately 5 feet wide and 25 feet long. A thin veneer of sandy topsoil covers about an 8-inch thick layer of calcium sulfate. Waste was excavated below the calcium sulfate layer. The waste consists of paper, plastic, rubber, glass, cardboard, one plastic unmarked, empty 55-gallon drum, and metal objects such as a car bumper, and 3x3x5-foot sheet metal box. Groundwater was encountered before the base of the waste at 7 feet.

Atmospheric Monitoring

The OVA was the only air monitoring device which detected air contaminants above background. OVA readings ranged from 2 to 100 ppm at the trench. OVA readings at the

work zone boundary downwind of the trench were sporadic ranging from 1 to 80 ppm . One hundred feet downwind, the OVA readings were down to background.

Trench 19

TP-19 is oriented slightly northeast trending. It is 25 feet long and approximately 5 feet wide. It is located at the northwest corner of the landfill cap.

The stratigraphic column begins with 1 foot of black, organic rich topsoil. From 1 foot to 2 feet, a layer of calcium sulfate was discovered. Below the calcium sulfate layer, waste was excavated. The waste consists primarily of wood, cardboard, glass bottles, beverage cans, and plastic. Small amounts of metal were excavated at the 3-foot depth consisting of a car muffler; two 55-gallon drums lids, unmarked and corroded; and a metal pail. The water table was encountered at 9 feet before the base of the waste was reached. Waste is, therefore, within the zone of saturation at this location.

Atmospheric Monitoring

The OVA was the only air monitoring instrument which had readings above background during the excavation of TP-19. Readings at the trench ranged from background to 2 ppm. Perimeter monitoring at the downwind direction revealed sporadic readings on the OVA which ranged from 0 to 120 ppm. Readings averaged about 50 ppm. Approximately 60 feet downwind from the trench, OVA readings were down to background with sporadic pulses to 5 ppm

Trench 20

TP-20 was excavated at the northeast corner of the site south of the quarry pond. This trench was oriented along a north-south trend extending 25 feet. The trench width varied from 5 to 8 feet.

The stratigraphic profile of this trench begins with a 1-foot thick layer of brown silty sand topsoil. Below the topsoil is a 1-foot thick layer of calcium sulfate. From 2 to 11 feet, waste is present. The waste consists of paper, cardboard, plastic bags, wood, black sand, and minor glass bottles. At the base of the waste, a second calcium sulfate layer was discovered. Groundwater was flowing from the interface of the waste and underlying white to gray calcium sulfate. A crumpled piece of sheet metal, roughly 3x3-foot, was excavated from the calcium sulfate at about the 12-foot depth. The excavation was completed at 13 feet where the water table was encountered.

Air Monitoring

Readings of H₂S and detections using the OVA were the only above background values observed during the excavation of TP-20. OVA readings at the trench ranged from background to greater than 1,000 ppm. Perimeter monitoring at the outside edge of the downwind side of the trench revealed OVA readings of 20 to 80 ppm with an average of 20 ppm. One hundred feet further downwind, the OVA readings averaged 10 ppm and were down to background 150 feet downwind from the trench.

TP/ke

A/R/HIMCO/AB5

APPENDIX A
FIELD PROCEDURES AND DATA EVALUATION METHODS
FOR GEOPHYSICAL SURVEY

TECHNICAL MEMORANDUM

ORIGINAL

DATE: April 30, 1991

TO: Vanessa Harris, Site Manager

CC: Roman Gau, Project Manager
Mike Crosser, TSQAM

FROM: David L. Grumman, Project Geophysicist
STS Consultants, Ltd.

SUBJECT: EPA ARCS Region V Contract No. 68-W8-0093
EPA Work Assignment No. 17-5L4J
Donohue Project No. 20026
STS Project No. 026.023
Himco Dump Site
Elkhart, Indiana

GEOPHYSICAL EXPLORATION PROGRAM

Introduction

STS Consultants, Ltd. (STS) was requested by Donohue to conduct combined electromagnetic and magnetic geophysical surveys at the above-referenced site. The objectives of the surveys were to identify and map anomalous zones to help target subsequent site explorations by Donohue. The survey encompassed approximately 60 acres at the Himco Dump Site. The specific geophysical survey areas include the fill areas, the unfilled margins of the dump, and a wetland remnant along the south central boundary of the landfill.

Survey Methods

The geophysical explorations consisted of combined electromagnetic terrain conductivity and magnetometer surveys.

Instrumentation

The electromagnetic (EM) survey was performed using a Geonics EM-31-DL terrain conductivity meter (EM-31) with a DL-55 data logger. The magnetometer (Mag) survey was performed using an EG&G G-856 proton precession magnetometer with two (top and bottom) sensors. The use of two sensors allows the measurement of the magnetic gradient at each survey position. A laptop field computer was used to download and process the field data during the survey. All geophysical survey instrumentation, with the exception of the field computer, were provided to STS by Donohue.

Mobilization and Field Personnel

Equipment operation was checked at STS's Northbrook, Illinois, office prior to mobilizing to the site. The geophysical survey equipment appeared to be in good working order. The STS field survey crew, Mark Stroebel, Michael Monteith, and David Grumman, arrived on-site Monday, October 22, 1990, and met with Ms. Marsha Kuehl and Mr. Tom Puchalski of Donohue to review the geophysical survey objectives and site safety procedures. At that time, a 100-foot by 100-foot staked grid was still being established on-site by a subcontract land surveyor.

Survey Procedures

EM and Mag readings were taken at 25-foot intervals along survey lines spaced every 25 feet. Distances were paced-off between each staked survey grid point. Survey line nomenclature is described further in the addendum to this memo. Consistent instrument orientations were used across the survey area. Only vertical dipole EM readings were taken, and perpendicular EM readings were not taken. Each STS instrument operator maintained a field notebook during the survey and noted conditions including surface obstructions, nearby metallic objects or structures, possible sources of electrical interference, reference points along selected survey lines (for data validation), and skipped readings.

Several base stations were established along the landfill's periphery to monitor magnetometer drift. The results of the base station readings generally showed low level drift in the magnetometer data during the field survey (+/- 75 gammas, approximate). The Mag field data were not adjusted to compensate for these low level variations during the data reduction. Selected survey points were also used to monitor drift in the EM readings; however, only negligible variations in the EM base station data were observed and drift corrections were not made.

Data Reduction

The field data were returned to STS's Northbrook, Illinois, office for data reduction and contouring. The data reduction steps for the magnetometer data consisted of: converting field data files to binary format, merging data files, gradient processing, grid position assignments, adjustments for erroneous and/or missing data, conversion of files to controllable ASCII (x-y-z) format for contouring, and computerized data contouring. A similar procedure was used to isolate the top and bottom Mag sensor readings. The EG&G program MAGPAC was used to reduce the Mag data.

A similar data reduction sequence was used for the EM data and consisted of: grid position assignments, adjustments for erroneous or missing data, separating quadrature and in-phase readings, conversion of data files to controllable ASCII (x-y-z) format, merging data files, and data contouring. The Geonics Ltd. program DAT31Q was used for the EM data reduction.

Deviations

Two field mobilizations were required to complete the survey since the survey grid had not been completed during the first mobilization. Field data from overlapping survey lines from both field efforts were evaluated and found to be consistent and generally reproducible between mobilizations.

An analysis of the Mag gradient data showed that the top sensor malfunctioned erratically during the survey, and thereby rendered the top sensor data unusable. The erratic data occurred at unpredictable intervals and appeared related to a sensor or instrument error. The anomalous top sensor readings did not match data trends in the more stable bottom sensor data. Consequently during data reduction, the bottom sensor total field data was isolated, reduced, and contoured.

The wetland remnant area was surveyed using an approximate grid system set-up by STS since no grid had been established by the land surveyors in this area.

Summary of Results

Over 3,000 site grid points were surveyed using the magnetometer and EM techniques.

Magnetometry Results

The contoured results of the magnetic data show several magnetic anomalies on-site. Figure 1 illustrates the contoured total field data (bottom sensor) and identifies the anomalies considered significant and not related to cultural interferences. These anomalies ranged between plus or minus 1000 to 4000 gammas in magnitude. Background magnetism appeared to be approximately 56750 gammas. A partial listing of some of the larger anomalies is as follows:

- Southeast-central region, directly north of site entrance.
- South central area, approximately 300 feet north of the remnant wetland.
- West central area (10, M).

EM Results

The contoured quadrature and in-phase EM data show several very large anomalous regions on-site (50 to 500 mmhos/m). More discreet anomalies are not easily resolved from the extensive quadrature anomalies, although several more localized in-phase anomalies (10 to 40 ppt) are apparent. Background levels were considered to be in the range of 10 to 40 mmhos/m for the quadrature phase and 0 to -2 ppt for the in-phase readings. Figures 2 and 3 illustrate the contoured quadrature and in-phase EM data, respectively. The extent of the large quadrature phase anomalies appears to highlight the approximate limits of filling, and shows that the surveys did provide minimal coverage beyond the fill boundaries. The in-phase data is considered more useful in the identification and mapping of conductive waste burial areas, i.e., areas which could contain concentrations of barrels, metal scrap, or highly conductive buried wastes. A partial list of the most significant in-phase anomalies includes:

- Southeast central area, north of site entrance.
- Southeast central, northwest of site entrance.
- Northeast central, south of former grave pit.
- Entire central region of landfill.

Data from the wetland remnant do not appear to show significant anomalous Mag or EM levels, as no readings appeared to be elevated above what would be considered background levels for sand soils. The quadrature data ranged between 2 and 20 mmhos/m. The wetland data was not included in the contoured data since the wetland survey grid could not be reliably tied into the site survey grid.

RS/ke

A/R/HIMCO/AH2

ADDENDUM TO TECHNICAL MEMORANDUM

Grid Position Nomenclature

Several survey positioning schemes were used during the survey. The land surveyors established a 100-foot by 100-foot staked grid using numbers (1-25) along the east-west axis (increasing eastward), and letters (A-U) along the north-south axis (increasing northward). Station A-25 was very close to the southeast corner of the survey area. STS adopted a geophysical survey line/station reference scheme by designating land survey line No. 25 as geophysical survey line 100, with the line numbers decreasing by 1 for each survey line moving west. Geophysical station numbers were simply the linear distance along each survey line north of the A line, where the A line equals 0 north. Finally, during data reduction, line numbers were reassigned to reflect Easting/Northing distances, in feet, by designating station A-25 equal to station 10,000 East, 0 North. The following table schematically presents the line numbering:

Survey Line Reference Nomenclature

<u>Land Surveyors Staked Location</u>	<u>Geophysical Field Survey</u>	<u>Geophysical Contour Coordinates</u>
Easting	Easting	Easting
25	100	10,000
	99	9,975
	98	9,950
	97	9,925
24	96	9,900
	95	,875
--	--	--
2	1	7,550
1	0	7,525
ns	201	7,475
ns	202	7,450

ns: Not Staked

The northing grid spacing was 25 feet, however, the EM meter automatically incremented/decremented this interval. The northing interval is irrelevant to the Magnetometer until data reduction. The range of northing coordinates for the survey area is 0 feet (southeast corner of site) to 2,050 feet (northwest corner of site).

Computer Data Files

The enclosed diskettes contain the following data:

<u>Disk</u>	<u>Files</u>	<u>Comment</u>
3 1/2" Diskette	HHimco1.new,..., HHimco19.new DHimco1.new,...,	Reduced EM Data files for using DAT31Q
	Himco1.dat,..., Himco16.dat	Raw Mag Data files (unreduced)
5 1/4" Diskette	Himco1VQ.xyz	x-y-z data file for EM quadrature data
	Himco1VI.xyz	x-y-z data file for EM in-phase data
	HimcoMG.dat	x-y-z data file for magnetometer
Gradiometer		data (erroneous)
	Himcobot.dat	x-y-z data file for bottom sensor magnetometer data
A/R/HIMCO/AH2		

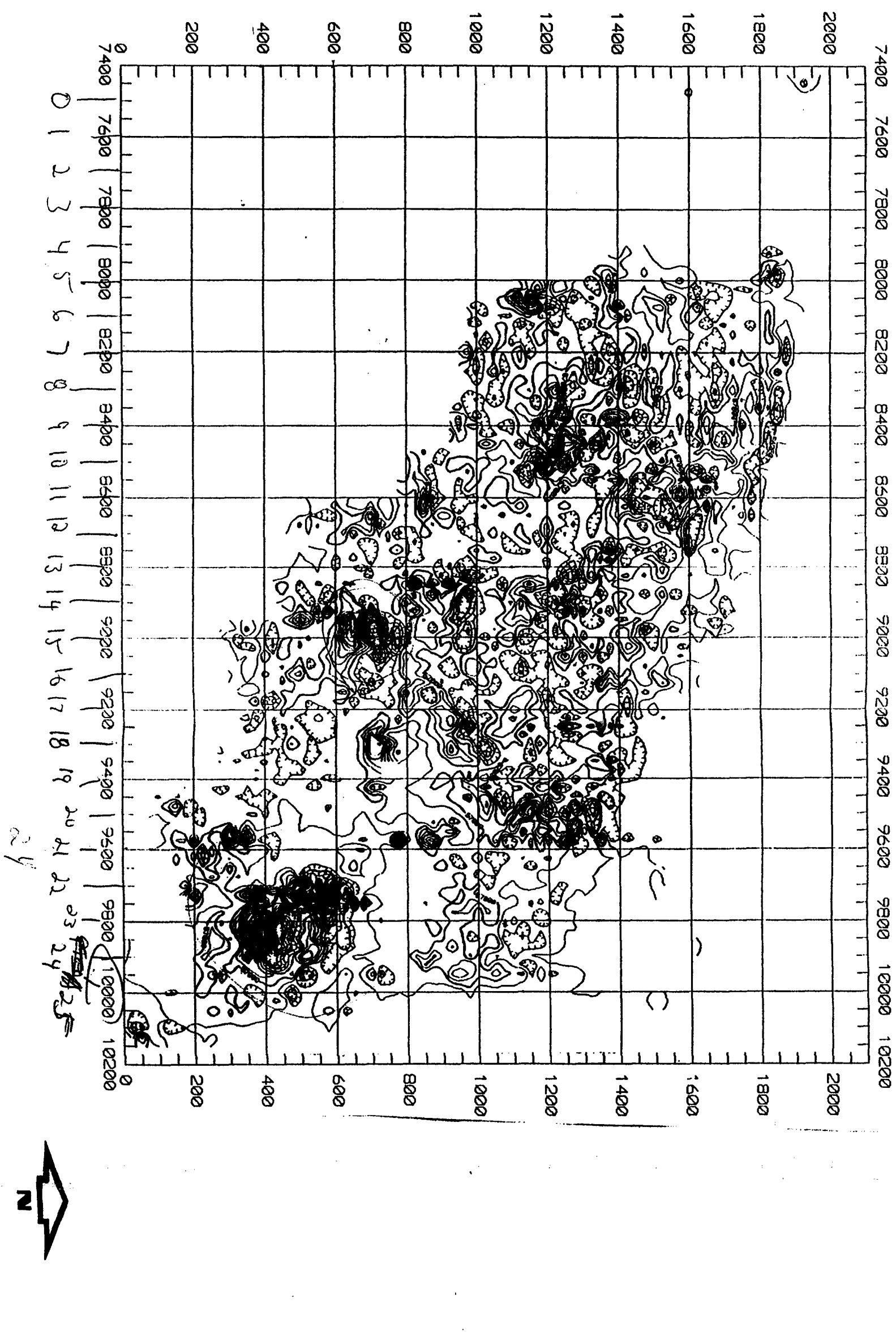


FIGURE 1
MAGNETOMETER SURVEY
(TECHNICAL MEMO)

HIMCO DUMP
SUPERFUND SITE
ELKHART, INDIANA

Donohue ENGINEERS
 ARCHITECTS
 SCIENTISTS

MAY 1991

20025

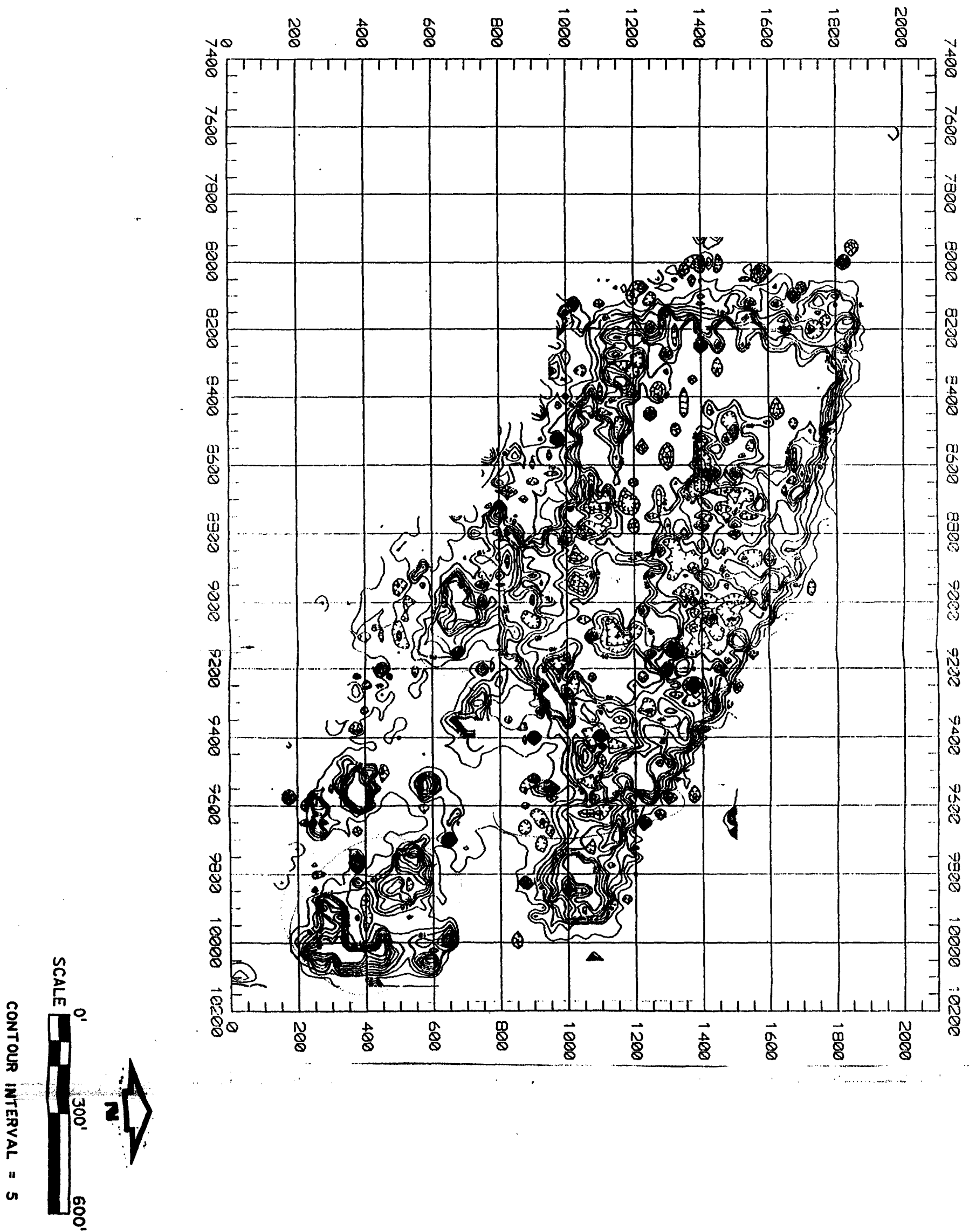


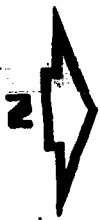
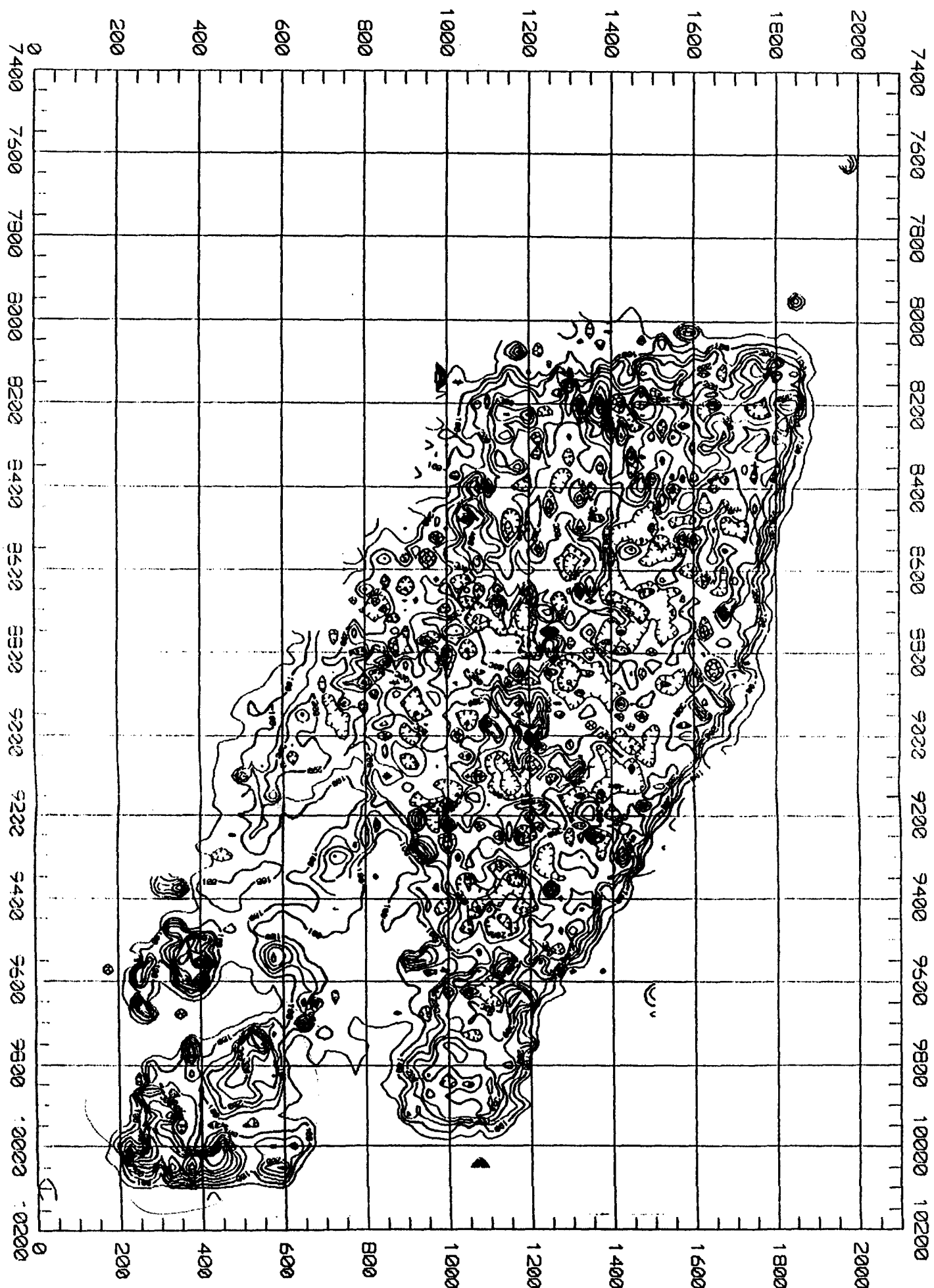
FIGURE 3
IN-PHASE EM-81 SURVEY
(TECHNICAL MEMO)

HIMCO DUMP
SUPERFUND SITE
ELKHART, INDIANA

Donohue ENGINEERS
 ARCHITECTS
 SCIENTISTS

MAY 1991

20026



SCALE
0' 300' 600'

CONTOUR INTERVAL = 50 mm/m

MAY 1991

**FIGURE 6
QUADRATURE PHASE EM-81 SURVEY
(TECHNICAL MEMO)**

**HIMCO DUMP
SUPERFUND SITE
ELKHART, INDIANA**

80028

Donohue ENGINEERS
ARCHITECTS
SCIENTISTS

APPENDIX B
TEST PIT LOGS

TRENCH LOG FORM



CLIENT: USEPA
 PROJECT: HIMCO
 PROJECT NO.: 20026.023
 DATE: 11/29/90
 GRID COORD.: START - N E N E
 END - N E N E
 CONTROL MONUMENT GRID COORD.: N E N E
 ELEVATION, TOP OF TRENCH:

SHEET 1 OF 1
 EXCAVATOR: MATHES
 LOG BY: TEP
 TRENCH NO.: TP-1
 TRENCH LENGTH: 0 FT TO 25 FT
 TRENCH WIDTH: 5 ft to 10 ft where caved

STRATA CHANGE OF WATER LEVEL	DEPTH	TRENCH LENGTH (FT)										DRUM QUANTITY	REMARK NO.
		1	2	3	4	5	6	7	8	9	0		
		White silt grading to blk at base											
		Black debris, saturated, bricks, wood, metal scraps, wire, railroad ties, trace of Alka seltzer bottles											
	5	Plastic bag layer ends here											
		Mauve material paste-like Water flows down to trench from here south											
		Bottom											
	10												
	15												
	20												
	25												

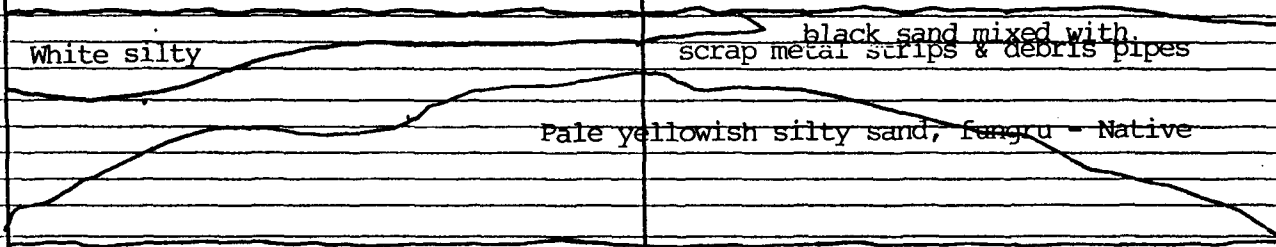
REMARKS:

TRENCH LOG FORM



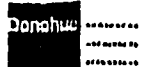
CLIENT: USEPA
 PROJECT: HIMCO
 PROJECT NO.: 20026-023
 DATE: 11/29/90
 GRID COORD.: START - N E N E
 END - N E N E
 CONTROL MONUMENT GRID COORD.: N E N E
 ELEVATION, TOP OF TRENCH:

SHEET 1 OF 1
 EXCAVATOR: MATHES
 LOG BY: TEP
 TRENCH NO.: TP-2
 TRENCH LENGTH: 25 FT TO 50 FT
 TRENCH WIDTH: 5 ft

STRATA CHANGE OF WATER LEVEL	DEPTH	TRENCH LENGTH (FT)										DRUM QUANTITY	REMARK NO.
		1	2	3	4	5	6	7	8	9	0		
		Ylw brn silty sand, roots moist											
													
	5	White silty					black sand mixed with scrap metal strips & debris pipes						
		Pale yellowish silty sand, fangru - Native											
	10	Bottom of pit											
	15												
	20												
	25												

REMARKS:

TRENCH LOG FORM



CLIENT: USEPA
 PROJECT: HIMCO
 PROJECT NO.: 20026.023
 DATE: 11/28/90
 GRID COORD.: START - N E N E
 END - N E N E
 CONTROL MONUMENT GRID COORD.: N E N E
 ELEVATION, TOP OF TRENCH:

SHEET 1 OF 1
 EXCAVATOR: MATHES
 LOG BY: TEP
 TRENCH NO.: TP-3
 TRENCH LENGTH: 50 FT TO 75 FT
 TRENCH WIDTH: 5-8 ft

STRATA CHANGE OF WATER LEVEL	DEPTH	TRENCH LENGTH (FT)										DRUM QUANTITY	REMARK NO.
		1	2	3	4	5	6	7	8	9	0		
		Ylw brn 10 yr 5/6 silty sand top soil moist, roots											
		Brown & white silt layer											
	5	Black sand metal strips & sscraps - metal corroded, 2 drum Lids, buff sand at base											
	10	25Y 7/4 Pale ylw fr green silty sand - Native soil											
	15												
	20												
	25												

REMARKS:



TRENCH LOG FORM

CLIENT: USEPA
PROJECT: HIMCO
PROJECT NO.: 20026.023
DATE: 11/28/90
GRID COORD.: START - N E N E
END - N E N E
CONTROL MONUMENT GRID COORD.: N E N E
ELEVATION, TOP OF TRENCH:

SHEET 1 OF 1
EXCAVATOR: MATHES
LOG BY: TEP
TRENCH NO.: TP-4
TRENCH LENGTH: 75 FT TO 100 FT
TRENCH WIDTH: 8 ft.

STRATA CHANGE OF WATER LEVEL	DEPTH	TRENCH LENGTH (FT)										DRUM QUANTITY	REMARK NO.
		1	2	3	4	5	6	7	8	9	0		
	5												
	10												
	15												
	20												
	25												

REMARKS:



TRENCH LOG FORM

CLIENT: USEPA
PROJECT: HIMCO
PROJECT NO.: 20026-023
DATE: 11/28/90
GRID COORD: START - N E N E
END - N E N E
CONTROL MONUMENT GRID COORD: N E N E
ELEVATION, TOP OF TRENCH: TP-5

SHEET 1 OF 1
EXCAVATOR: MATHES
LOG BY: TEP
TRENCH NO.: TP 5 & 6
TRENCH LENGTH: 75 FT TO 100 FT
TRENCH WIDTH: 5 feet

STRATA CHANGE OF WATER LEVEL	DEPTH	TRENCH LENGTH (FT)										DRUM QUANTITY	REMARK NO.
		--1--	--2--	--3--	--4--	--5--	25	--6--	--7--	--8--	--9--	50	
		Brown silty sand top soil											
	5	CaSO ₄											
		Most sheet metal at 8 ft											
		Sheet metal, metal strips, weed											
		black sand, plastic wrap											
	10	* * * * *											
		Large concentration of 3 x 6 sheet metal											
		Black silty sand											
		Black silty sand, metal strips concentrated at 8 ft BUT DISTRIBUTED THROUGHOUT											
	15												
		Bottom of pit											
	20												
	25												

REMARKS:



TRENCH LOG FORM

CLIENT: USEPA-ARCS
PROJECT: HIMCO
PROJECT NO.: 20026.023
DATE: 11/29/90
GRID COORD.: START - N E N E
END - N E N E
CONTROL MONUMENT GRID COORD.: N E N E
ELEVATION, TOP OF TRENCH: N TP-7 TP-8 S

SHEET 1 of 1
EXCAVATOR: MATHES CHRIS GOODWIN MIKE DONAHUE
LOG BY: TEP
TRENCH NO.: 7 & 8
TRENCH LENGTH: 0 FT TO 50 FT
TRENCH WIDTH: 5 ft.

STRATA CHANGE OF WATER LEVEL	DEPTH	TRENCH LENGTH (FT)										DRUM QUANTITY	REMARK NO.
		1	2	3	4	5	6	7	8	9	0		
		CaSO ₄					Metal Pipe						
		thin layer of topsoil					Car BUMPER, REFRIGERATOR COMPRESSOR						
	5	MIXED WASTE - FIBERGLASS TEMPLATES, WOOD, PAPER, AEROSOL CANS-SUDEN BEAUTY HAIR SPRAY, CRISTAN					SHEET METAL						
		TOOTH PASTE SAMPLER, Alka-Seltzer wrappers, plastic bags					metal pipe						
							DRUM - 25 gallon - CORRODED						
	10	black sand, alka seltzer lids					Matrix of mixed waste						
		BOTTOM OF PIT					BOTTOM OF PIT						
	15	DRUM:											
		1 55-gallon •					3 lids						
		unmarked					1 marked Aliphatic Resin						
	20	1 25-gallon +											
		unmarked											
	25												

REMARKS:

TRENCH LOG FORM



CLIENT: USEPA
 PROJECT: HIMCO DUMP
 PROJECT NO.: 20026.023
 DATE: 11/29/90
 GRID COORD.: START - N E N E
 END - N E N E
 CONTROL MONUMENT GRID COORD.: N E N E
 ELEVATION, TOP OF TRENCH: TD-9

SHEET 1 OF 1
 EXCAVATOR: MATHES
 LOG BY: TOM PUCHALSKI
 TRENCH NO.: TP-9
 TRENCH LENGTH: 0 FT TO 25 FT
 TRENCH WIDTH: 5-6 ft

STRATA CHANGE OF WATER LEVEL	DEPTH	TRENCH LENGTH (FT)										DRUM QUANTITY	REMARK NO.
		1	2	3	4	5	6	7	8	9	10		
		CaSO ₄											
		3 drum lids											
	5	Tires, wood, black sand, plastic bags, Alka-seltzer wrappers rubber in 1/8" bands											
		CaSO ₄											
	10	Paper, plastic bags											
	15	bottom at 12'											
	20												
	25												

REMARKS: The only metal present was three 55 gallon drum lids - unmarked, and bundles of wire all at about 4' depth.

TRENCH LOG FORM



CLIENT: USEPA
PROJECT: HIMCO
PROJECT NO.: 20026.023
DATE: 11/30/90
GRID COORD.: START - N E N E
END - N E N E
CONTROL MONUMENT GRID COORD.: N E N E
ELEVATION, TOP OF TRENCH: 10 11 S

SHEET 1 OF 1
EXCAVATOR: MATHES
LOG BY: TOM PUCHALSKI
TRENCH NO.: 10 & 11
TRENCH LENGTH: 0 FT TO 50 FT
TRENCH WIDTH: 5 ft.

STRATA CHANGE OF WATER LEVEL	DEPTH	TRENCH LENGTH (FT)										DRUM QUANTITY	REMARK NO.
		1	2	3	4	5	6	7	8	9	0		
		Ylw Brn silty sand TOP SOIL - roots											
		plastic bags, bottles, wood paper											
	5	CaSO ₄ - Black layer mixed with white & gray, some 1" x 5" boards.											
	10	Bottom of pit											
	15												
	20												
	25												

REMARKS: Very little metal. One piece of sheet metal was located 10 feet south of north edge of TP-10 at 3" depth.

Donohue

SHEET 1 OF 1
EXCAVATOR: MATHES
LOG BY: TEP
TRENCH NO.: 12 & 13
TRENCH LENGTH: 0 FT TO 50 FT
TRENCH WIDTH:

STRATA CHANGE OF WATER LEVEL	DEPTH	TRENCH LENGTH (FT)										DRUM QUANTITY	REMARK NO.
		1	2	3	4	5	6	7	8	9	0		
		Ylw brown silty sand top soil fill											
	5	CaSO ₄ White with some fracture faces yellow											
▽ ~ ~	10	wood, paper, sheet metal CaSO ₄					sheet metal Rubber sheets, wood						
		Alka-seltzer Wrapper											
	15												
	20												
	25												

REMARKS:

TRENCH LOG FORM



CLIENT: USEPA
 PROJECT: HIMCO
 PROJECT NO.: 20026.023
 DATE: 11/30/90
 GRID COORD.: START - N _____ E _____ N _____ E _____
 END - N _____ E _____ N _____ E _____
 CONTROL MONUMENT GRID COORD.: N _____ E _____ N _____ E _____
 ELEVATION, TOP OF TRENCH: W _____ 14 _____ 15 _____ E _____

SHEET 1 OF 1
 EXCAVATOR: Mathes
 LOG BY: Tom Puchalski
 TRENCH NO.: 14 & 15
 TRENCH LENGTH: 0 FT TO 50 FT
 TRENCH WIDTH: 5 - 7 ft

STRATA CHANGE OF WATER LEVEL	DEPTH	TRENCH LENGTH (FT)										DRUM QUANTITY	REMARK NO.
		1	2	3	4	5	6	7	8	9	0		
		Brown to Ylw brn silty sand topsoil - Roots											
		Hardened CaSO ₄ - White to gray											
		Natural sand buff to brown with black zones 6" thick --6' long, unsaturated											
	5												Wood & metal debris
													Flowing water
													Metal debris
	10												
	15												
	20												
	25												

REMARKS: Water began pouring from east end of trench and nearly filled trench by the time the backfill was complete. Rate of discharge did not slow during the 10 minutes of observation.

TRENCH LOG FORM



CLIENT: USEPA
 PROJECT: Himco
 PROJECT NO.: 20026.023
 DATE: December 1, 1990
 GRID COORD.: START - N E N E
 END - N E N E
 CONTROL MONUMENT GRID COORD.: N E N E
 ELEVATION, TOP OF TRENCH: NW

SHEET 1 OF 1
 EXCAVATOR: Mathes
 LOG BY: TEP
 TRENCH NO.: TP-16
 TRENCH LENGTH: 0 FT TO 25 FT
 TRENCH WIDTH: 5 feet

STRATA CHANGE OF WATER LEVEL	DEPTH	TRENCH LENGTH (FT)										DRUM QUANTITY	REMARK NO.
		1	2	3	4	5	6	7	8	9	0		
		CaSO ₄											
		Black - wood, paper, bottles, rubber, plastic bags. Trace of sheet											
		metal and metal pipe											
	5												
	10												
		Brownish ylw top soil, fine ground silty sand, roots moist.											
	15												
	20												
	25												

REMARKS: Metal - sheet metal - mirror - one sheet, metal gas can from lawnmower with hole in it, two 1" x 2' metal pipes. Shallow groundwater did not allow deeper excavation.

TRENCH LOG FORM



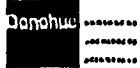
CLIENT: USEPA
 PROJECT: Himco
 PROJECT NO.: 20026.023
 DATE: 12/1/90
 GRID COORD.: START - N E N E
 END - N E N E
 CONTROL MONUMENT GRID COORD.: N E N E
 ELEVATION, TOP OF TRENCH: W

SHEET 1 OF 1
 EXCAVATOR: JMA
 LOG BY: TEP
 TRENCH NO.: 17
 TRENCH LENGTH: 0 FT TO 25 FT
 TRENCH WIDTH: 5

STRATA CHANGE OF WATER LEVEL	DEPTH	TRENCH LENGTH (FT)										DRUM QUANTITY	REMARK NO.
		1	2	3	4	5	6	7	8	9	0		
		CaSO ₄											
		80% rubber sheets and bands, rest - paper, wood, glass, trace aluminum											
		PHOTO #1											
	5	Ylw brown silty sand (SI7) top soil, roots, moist											
	10												
	15												
	20												
	25												

REMARKS:

TRENCH LOG FORM



CLIENT: USEPA
 PROJECT: Himco
 PROJECT NO.: 20026.023
 DATE: 12/1/90
 GRID COORD.: START - N E N E
 END - N E N E
 CONTROL MONUMENT GRID COORD.: N E N E
 ELEVATION, TOP OF TRENCH: W

SHEET 1 OF 1
 EXCAVATOR: Mathes
 LOG BY: Tom Puchalski
 TRENCH NO.: TP-18
 TRENCH LENGTH: 0 FT TO 25 FT
 TRENCH WIDTH: 5 ft

STRATA CHANGE OF WATER LEVEL	DEPTH	TRENCH LENGTH (FT)										DRUM QUANTITY	REMARK NO.
		1	2	3	4	5	6	7	8	9	0		
					topsoil	CaSO							
		Municipal Waste & paper, plastic, rubber, glass, cardboard x 1 plastic 55 gal drum											
	5						X - car bumper & other large metal objects (3 x 3 x 5 sheet metal box)						
	10												
	15												
	20												
	25												

REMARKS:

TRENCH LOG FORM



CLIENT: USEPA
 PROJECT: Himco
 PROJECT NO.: 20026.023
 DATE: 12/1/90
 GRID COORD.: START - N E N E
 END - N E N E
 CONTROL MONUMENT GRID COORD.: N E N E
 ELEVATION, TOP OF TRENCH: W

SHEET 1 OF 1
 EXCAVATOR: JMA (John Mathes & Assoc.)
 LOG BY: TEP
 TRENCH NO.: TP-19
 TRENCH LENGTH: 0 FT TO 25 FT
 TRENCH WIDTH: 5

STRATA CHANGE OF WATER LEVEL	DEPTH	TRENCH LENGTH (FT)										DRUM QUANTITY	REMARK NO.
		1	2	3	4	5	6	7	8	9	0		
		Black organic rich top soil					White CaSO ₄						
		muffler, drum lids, pail											
	5	Wood, cardboard, trash, bottles, cans,					glass, plastic						
	10												
	15												
	20												
	25												

REMARKS:

TRENCH LOG FORM



CLIENT: USEPA
 PROJECT: Hlmco Dump
 PROJECT NO: 20026.023
 DATE: 12/1/90
 GRID COORD: START - N E N E
 END - N E N E
 CONTROL MONUMENT GRID COORD: N E N E
 ELEVATION, TOP OF TRENCH: N

SHEET 1 OF 1
 EXCAVATOR: JMA
 LOG BY: TEP
 TRENCH NO: 20
 TRENCH LENGTH: 0 FT TO 25 FT
 TRENCH WIDTH: 5 - 8 ft

STRATA CHANGE OF WATER LEVEL	DEPTH	TRENCH LENGTH (FT)										DRUM QUANTITY	REMARK NO.
		5	10	15	20	25							
	5												
	10												
	15												
	20												
	25												

REMARKS:

top soil - brown silty sand
 $CaSO_4$

Paper, cardboard, plastic bags, minor glass bottles, wood, black sand

water at interface
 White to gray $CaSO_4$

crumpled sheet metal - Photo #7

bottom

ORIGINAL

TECHNICAL MEMORANDUM NUMBER 11

DATE: April 29, 1991
TO: Vanessa Harris
CC: Marcia Kuehl - RI Lead
Roman Gau - Project Manager
Mike Crosser - TSQAM
FROM: Tom Puchalski
SUBJECT: EPA ARCS Region V Contract No. 68-W8-0093
EPA Work Assignment No. 17-5L4J
Donohue Project No. 20026.024
Himco Dump Phase I

SLUG TESTING FIELD PROCEDURES AND ANALYSIS

Introduction

Following well development, groundwater monitoring wells listed in Table 1, were slug-tested at the Himco Dump. Wells E3, F1, F2, M1, and M2 were installed in 1977 and 1979 by the United States Geological Survey (U.S.G.S.) The remainder of the wells were installed by Donohue for this remedial investigation. The wells were slug-tested to determine hydraulic conductivity of outwash deposits at several points across the site at the depths listed in Table 1. Slug testing was done on December 1, 2, 14, and January 4, 1991, by Cathy Fruehe, Tracy Koach, Anya Kirykowicz, and Tom Puchalski of Donohue & Associates, Inc.

Field Methods

An ORS Environmental Equipment Model EL-200 data logger and pressure transducer were used to collect slug test data. The battery-operated unit translates water pressure into electrical signals within the transducer. The electrical signals are relayed by a cable to the data logger where they are converted and displayed as water level data. The time and water level data are recorded during the test and stored in the data logger memory until the data is sent to a disk or printer for later analysis.

Slug tests were performed as described in Section 4.2.3.3 of the Final Field Sampling Plan, Himco Dump Remedial Investigation/Feasibility Study, Elkhart, Indiana. The setup for the slug test began by unlocking the protective casing and using a decontaminated popper tape to measure the static water level and the depth to well bottom. This data was recorded on In-Field Hydraulic Conductivity Slug Test Forms (Appendix B). A 15 or 5 psi transducer was decontaminated with soap and tap water, and a tap water rinse before lowering into the well. The mode which allows the water level to be read on the data logger display was activated so that the depth of water above the transducer could be read while the transducer was lowered into the water. The transducer cable was duct taped to the protective casing when a maximum of approximately 9 feet of water was above the level

of the transducer. A 4-foot long stainless steel slug was slowly lowered down the well until a slight perturbation in static water level was noticed on the data logger LCD display, indicating the slug had intersected water table. The slug was raised a few inches above the water surface as the water level was allowed to equilibrate. After the water level had equilibrated, the data recording mode of the logger was activated simultaneously with lowering the slug 4 to 5 feet into the water. The falling water level and time were recorded in the data logger memory. When the static water level was re-established, the falling head test was ended. A record of the rising water level and time was obtained as the slug was removed from the water. The test was complete when the static water level was reached. These procedures were repeated until all 15 wells were slug tested.

Analysis Evaluation

Slug test data were analyzed using the method of Bouwer and Rice (1976), through the use of a PC-based computer program developed by Donohue & Associates, Inc. The assumptions of the method are that 1) the drawdown of the water table around the well is negligible, 2) flow above the water table (capillary fringe) can be ignored, 3) well losses are negligible, and 4) the aquifer is homogeneous and isotropic.

Deviations

For unknown reasons, the data plots resulting from a small number of tests were not indicative of a normal test. A straight line plot of the natural logarithm of the drawdown plotted against time was not provided, so the analysis could not be performed. A falling or a rising head test or both was successfully run for every previously selected well. Therefore, all the required results were obtained.

Summary of Results

Printouts of the data and data plots of drawdown versus time are included in Appendix A.

Selection of the segment of the data plot of the natural logarithm of drawdown versus time to be used for the calculation of hydraulic conductivity was based upon the following criteria as described in Bouwer and Rice (1976):

- o The straight line portion of the plot of recovery versus time is the valid data to be used in the analysis. An evaluation of the fit of the data to a straight line was accomplished by linear regression analysis included in the program. Most of the regression values indicated a strong linear relationship in the data. This implies that the assumptions of the analysis method are being met.
- o For the wells with rapid recovery times, the first few data points were used in the analysis. If the hydraulic conductivity of the aquifer was significantly different (several orders of the magnitude) from the hydraulic conductivity of the sand pack, sand pack dewatering was accounted for in the analysis.

REFERENCES

Bouwer, H., 1989, The Bouwer and Rice Slug Test - An Update, v. 27, n. 3, pp. 304-309.

Bouwer, H., and Rice, R.C., 1976, A Slug Test for Determining Hydraulic Conductivity of Unconfined Aquifers with Completely or Partially Penetrating Wells, Water Resources Research, v. 12, n. 3, pp. 423-428, 1976.

Freeze, R.A., and Cherry, J.A., 1979, Groundwater, Prentice-Hall, Inc., Englewood Cliffs, New Jersey, pp. 29.

TABLE 1

WELL NUMBER	HYDRAULIC CONDUCTIVITY (cm/s)	BOTTOM DEPTH OF SCREEN	SOIL CLASS+WELL SCREENED IN
M1-RISE	3.17x10 ⁻³	103.24	SP, GP
M1-FALL	1.43x10 ⁻³	103.24	SP, GP
F1-RISE	1.21x10 ⁻¹	31.28	*
F1-FALL	4.51x10 ⁻²	31.28	*
F2-FALL	1.27x10 ⁻³	147.83	*
F2-RISE	7.37x10 ⁻⁴	147.83	*
M2-RISE	3.69x10 ⁻²	24.76	*
E3-RISE	7.95x10 ⁻⁴	175.65	SP, GP
E3-FALL	4.61x10 ⁻⁴	175.65	SP, GP
P101B-FALL	3.99x10 ⁻³	100.47	SM
P101C-FALL	1.11x10 ⁻³	166.53	SP
P102B-RISE	3.50x10 ⁻²	67.25	SP
P102B-FALL	3.91x10 ⁻²	67.25	SP
P102C-RISE	3.59x10 ⁻³	159.96	SP
WT101A-RISE	2.69x10 ⁻²	18.70	SP
WT101A-FALL	9.45x10 ⁻³	18.70	SP
WT102A-RISE	4.14x10 ⁻³	18.18	SP-SM,SP-GP,SM
WT102A-FALL	6.80x10 ⁻³	18.18	SP-SM,SP-GP,SM
WT103A-RISE	4.10x10 ⁻²	18.47	SW-GW
WT103A-FALL	1.86x10 ⁻²	18.47	SW-GW
WT104A-RISE	3.89x10 ⁻²	18.69	SP,SW-GW
WT104A-FALL	5.07x10 ⁻³	18.69	SP,SW-GW
WT105A-RISE	1.93x10 ⁻²	18.56	SP
WT105A-FALL	1.01x10 ⁻²	18.56	SP
WT106A-RISE	4.71x10 ⁻²	18.50	SP-GP
WT106A-FALL	<u>8.40x10⁻²</u>	18.50	SP-GP
AVERAGE	2.33x10⁻²		

* Data not available.

+ United Soil Classification System

A/R/HIMCO/AB6

APPENDIX A
DATA PLOTS AND ANALYSIS

BOUWER AND RICE METHOD FOR INTERPRETATION OF SLUG TESTS: FOR UNCONFINED AND LEAKY CONFINED AQUIFERS.
 TO UTILIZE THIS WORKSHEET, ENTER YOUR DATA AT LOCATIONS MARKED BY AN "X".
 PROGRAM CAN INCLUDE EFFECTS OF SANDPACK DEWATERING (ASSUMING WATER IS RISING WITHIN THE SANDPACK).

TIME min	DEPTH TD	DRAWDOWN	TIME sec	LN	PROJECT NAME	WELL NO	DATE COLLECTED	RISE PIPE (ID)	EFFECTIVE SCREEN DIAMETER	EFFECTIVE SCREEN LENGTH	TIME DRAWDOWN (IN SUPPLY)	STATIC WATER LEVEL	DEPTH FROM SML TO EFF. SCREEN BOTTOM	AQUIFER DEPTH (SML TO AQUIFER BOTTOM)	INCLUDE SANDPACK DEWATERING (ENTER 1 IF YES, 0 IF NO)	SANDPACK'S SPECIFIC YIELD (Sv)
1	8.42	1.560	0.00	0.4447	HIMCO	M-1 RISE	12-2-90									
2	8.44	1.540	0.20	0.4318												
3	8.46	1.520	0.40	0.4187												
4	8.48	1.490	0.60	0.3988												
5	8.50	1.480	0.80	0.3929												
6	8.52	1.460	1.00	0.3784												
7	8.54	1.440	1.20	0.3646												
8	8.56	1.420	1.40	0.3577												
9	8.57	1.410	1.60	0.3436												
10	8.59	1.390	1.80	0.3293												
11	8.61	1.370	2.00	0.3148												
12	8.62	1.360	2.20	0.3075												
13	8.64	1.340	2.40	0.2927												
14	8.65	1.330	2.60	0.2852												
15	8.67	1.310	2.80	0.2706												
16	8.68	1.300	3.00	0.2624												
17	8.70	1.280	3.20	0.2469												
18	8.72	1.260	3.40	0.2311												
19	8.74	1.240	3.60	0.2151												
20	8.75	1.230	3.80	0.2070												
21	8.76	1.220	4.00	0.1989												
22	8.78	1.200	4.20	0.1823												
23	8.79	1.190	4.40	0.1740												
24	8.81	1.170	4.60	0.1570												
25	8.83	1.150	5.00	0.1398												
26	8.84	1.140	5.20	0.1310												
27	8.86	1.120	5.40	0.1133												
28	8.88	1.100	5.60	0.0953												
29	8.89	1.090	6.00	0.0862												
30	8.91	1.070	6.20	0.0677												
31	8.92	1.060	6.40	0.0583												
32	8.94	1.040	6.60	0.0392												
33	8.95	1.030	7.00	0.0296												
34	8.98	1.000	8.00	0.0000												
35	9.03	0.950	9.00	-0.0513												
36	9.06	0.900	10.00	-0.1054												
37	9.13	0.850	11.00	-0.1625												
38	9.19	0.790	12.00	-0.2357												
39	9.23	0.750	13.00	-0.2877												
40	9.27	0.710	14.00	-0.3425												
41	9.32	0.660	15.00	-0.4155												
42	9.35	0.630	16.00	-0.4620												
43	9.39	0.590	17.00	-0.5276												
44	9.43	0.550	18.00	-0.5978												
45	9.46	0.520	19.00	-0.6539												
46	9.49	0.490	20.00	-0.7133												
47	9.52	0.460	21.00	-0.7765												
48	9.55	0.430	22.00	-0.8440												
49	9.58	0.400	23.00	-0.9163												
50	9.62	0.360	24.00	-1.0217												
51	9.66	0.320	25.00	-1.1394												
52	9.71	0.270	26.00	-1.2693												
53	9.74	0.240	27.00	-1.4271												
54	9.77	0.210	28.00	-1.5666												
55	9.79	0.190	30.00	-1.6607												
56	9.82	0.160	32.00	-1.8326												
57	9.84	0.140	35.00	-1.9661												
58	9.86	0.120	41.00	-2.1203												
59	9.87	0.110	43.00	-2.2073												
60	9.89	0.090	45.00	-2.4077												
61	9.91	0.080	47.00	-2.5257												

BOUWER AND RICE CURVE COEFFICIENTS:

RATIO OF $L/(r \text{ sub } w) = 15.00$

---LOE OF $L/(r \text{ sub } w) = 1.1761$

FOR PARTIALLY PENETRATING WELLS---

A = 1.93

B = 0.29

FOR FULLY PENETRATING WELLS---

C = 1.36

---EVALUATION OF $LN(Re/(r \text{ sub } w))$:

CONST.1 = 0.1971

CONST.2 = 5.5599 \times (MAX. OF 6.0) = 5.5599

$LN(Re/(r \text{ sub } w)) = 2.30$

EFFECTIVE $r \text{ sub } c$ (for sandpack dewatering) = 0.0833

$(1/T)(LN(Yo/Yt))$ (SLOPE) = $-6.50E-02 \text{ sec}^{-1}$

HYDRAULIC CONDUCTIVITY (K) = $1.04E-04 \text{ ft/sec}$

$3.17E-03 \text{ cm/sec}$

Regression Output:

Constant 4.96E-01

Std Err of Y Est 0.0842

R Squared 0.9947

No. of Observations 66

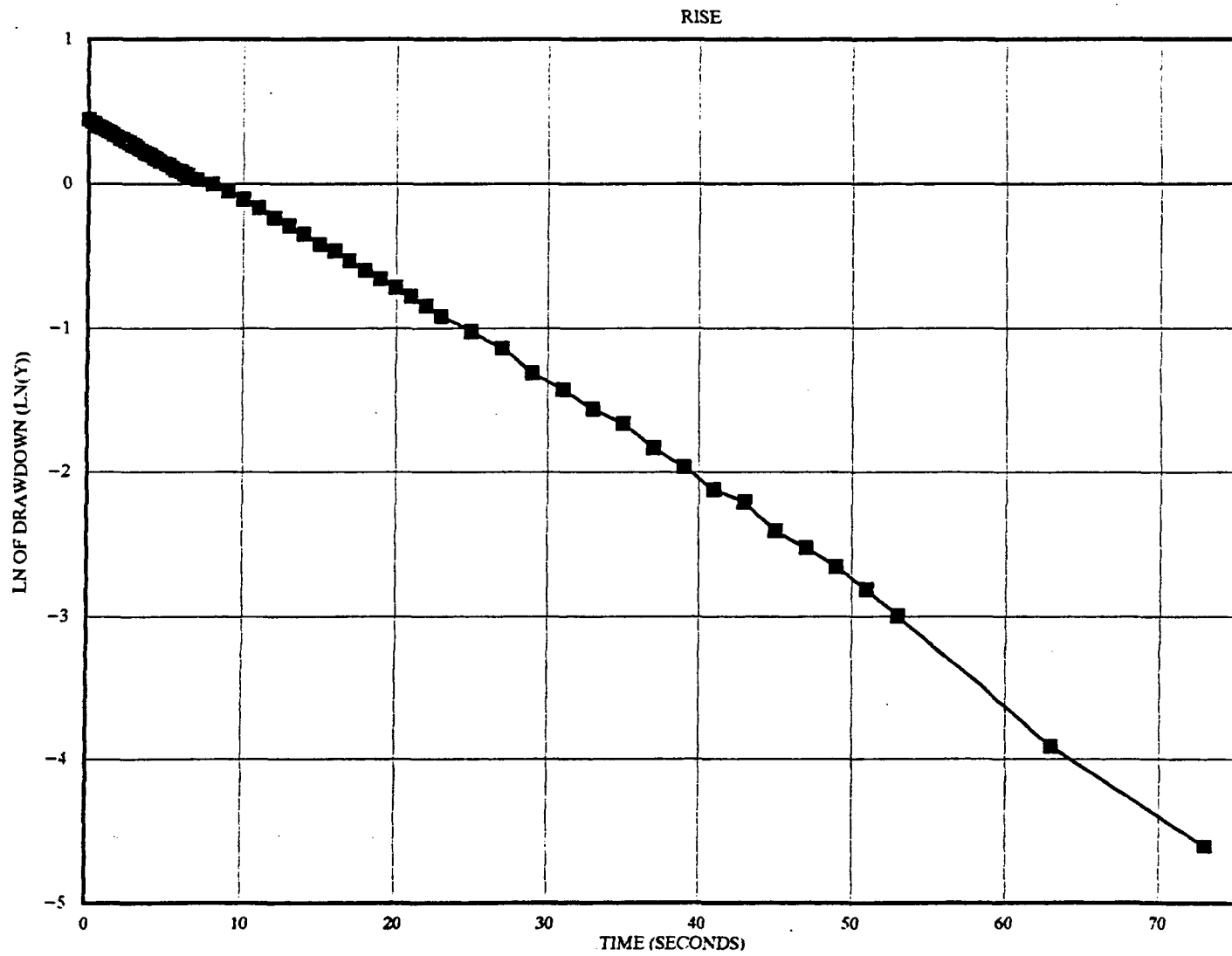
Degrees of Freedom 64

Y Coefficient(s) $-6.50E-02$

Std Err of Coef. 0.0006

$t = 0 - 73.9$

RATE OF RECOVERY TEST: WELL M-1



BOUWER AND RICE METHOD FOR INTERPRETATION OF SLUG TESTS: FOR UNCONFINED AND LEAKY CONFINED AQUIFERS.

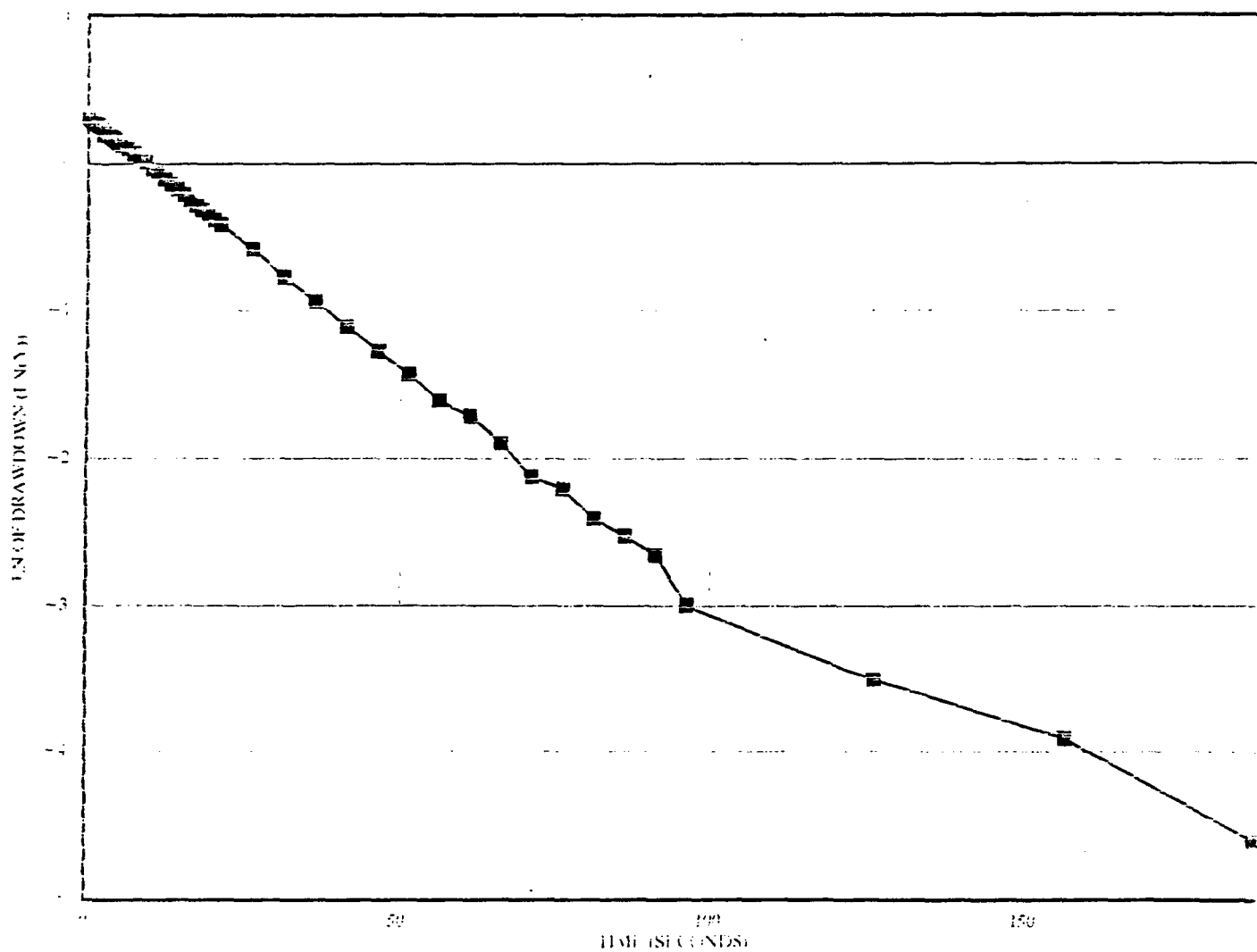
TO UTILIZE THIS WORKSHEET, ENTER YOUR DATA AT LOCATIONS MARKED BY AN "X".

PROGRAM CAN INCLUDE EFFECTS OF SANDPACK DEWATERING (ASSUMING WATER IS RISING WITHIN THE SANDPACK).

TIME min	DEPTH TO: (ft)	TIME sec	LN	PROJECT NAME	WIMCO
(X)	(Y)	(X)	(Y)	PROJECT NO	20026.024
1	11.36	1.360	0.00	ANALYST	PODHALSKI
2	11.34	1.360	0.20	DATE COLLECTED	11-2-90
3	11.33	1.350	0.40	RISE PIPE (ID)	12 r sub c = 2.0 in. = 0.0833 (radius in ft.)
4	11.32	1.340	0.60	EFFECTIVE SCREEN DIAMETER (2 r sub w)	5.0 in. = 0.3333 (radius in ft.)
5	11.31	1.330	0.80	EFFECTIVE SCREEN LENGTH (L)	5.00 Ft.
6	11.30	1.320	1.00	WELL DEWATERING (IN SUBSET) (Ymax)	-1.58 Ft.
7	11.29	1.310	1.40	STATIC WATER LEVEL (SWL)	5.98 Ft.
8	11.28	1.300	1.80	DEPTH FROM SWL TO EFF. SCREEN BOTTOM (H)	88.40 Ft.
9	11.27	1.290	1.80	TEST AQUIFER DEPTH (SWL TO AQUIFER BOTTOM) (D)	175.00 Ft.
10	11.25	1.270	2.20	INCLUDE SANDPACK DEWATERING (ENTER 1 IF YES, 0 IF NO)?	0
11	11.24	1.260	2.40	SANDPACK'S SPECIFIC YIELD (Sy)	0.10
12	11.23	1.250	2.60	BOUWER AND RICE CURVE COEFFICIENTS:	
13	11.22	1.240	2.80	RATIO OF L/(r sub w) = 15.00	
14	11.21	1.230	3.00	---LOG OF L/(r sub w) = 1.1761	
15	11.20	1.220	3.20	FOR PARTIALLY PENETRATING WELLS--	
16	11.19	1.210	3.40	A = 1.93	
17	11.18	1.200	3.60	B = 0.29	
18	11.17	1.190	4.00	FOR FULLY PENETRATING WELLS--	
19	11.16	1.180	4.20	C = 1.38	
20	11.15	1.170	4.40	---EVALUATION OF LN(Re/(r sub w)):	
21	11.14	1.160	4.60	CONST.1 = 0.1971	
22	11.13	1.150	4.80	CONST.2 = 5.5599 = (MAX. OF 6.0) = 5.5599	
23	11.12	1.140	5.00	LN(Re/(r sub w)) = 2.30	
24	11.11	1.130	5.40	EFFECTIVE r sub c (for sandpack dewatering) = 0.0833	
25	11.09	1.110	6.40	(1/T)/(LN(Yo/Yt)) (SLOPE) = -2.94E-02 sec ⁻¹	
26	11.05	1.070	7.40	HYDRAULIC CONDUCTIVITY (K) = 4.70E-05 ft/sec	
27	11.02	1.040	8.40	1.43E-03 cm/sec	
28	10.99	1.010	9.40	Regression Output:	
29	10.94	0.960	10.40	Constant 2.37E-01	
30	10.92	0.940	11.40	Std Err of Y Est 0.1530	
31	10.88	0.900	12.40	R Squared 0.9841	
32	10.85	0.870	13.40	No. of Observations 58	
33	10.82	0.840	14.40	Degrees of Freedom 56	
34	10.79	0.810	15.40	Y Coefficient(s) -2.94E-02	
35	10.76	0.780	16.40	Std Err of Coef. 0.0005	
36	10.73	0.750	17.40		
37	10.71	0.730	18.40		
38	10.68	0.700	19.40		
39	10.66	0.680	20.40		
40	10.64	0.660	21.40		
41	10.54	0.560	26.40		
42	10.44	0.460	31.40		
43	10.37	0.390	36.40		
44	10.31	0.330	41.40		
45	10.26	0.280	46.40		
46	10.22	0.240	51.40		
47	10.18	0.200	56.40		
48	10.16	0.180	61.40		
49	10.13	0.150	66.40		
50	10.10	0.120	71.40		
51	10.09	0.110	76.40		
52	10.07	0.090	81.40		
53	10.06	0.080	86.40		
54	10.05	0.070	91.40		
55	10.03	0.050	96.40		
56	10.01	0.020	101.40		
57	10.00	0.020	106.40		
58	9.99	0.010	111.40		

t = 0-186.4 s

RATE OF RECOVERY TEST: WELL M-1

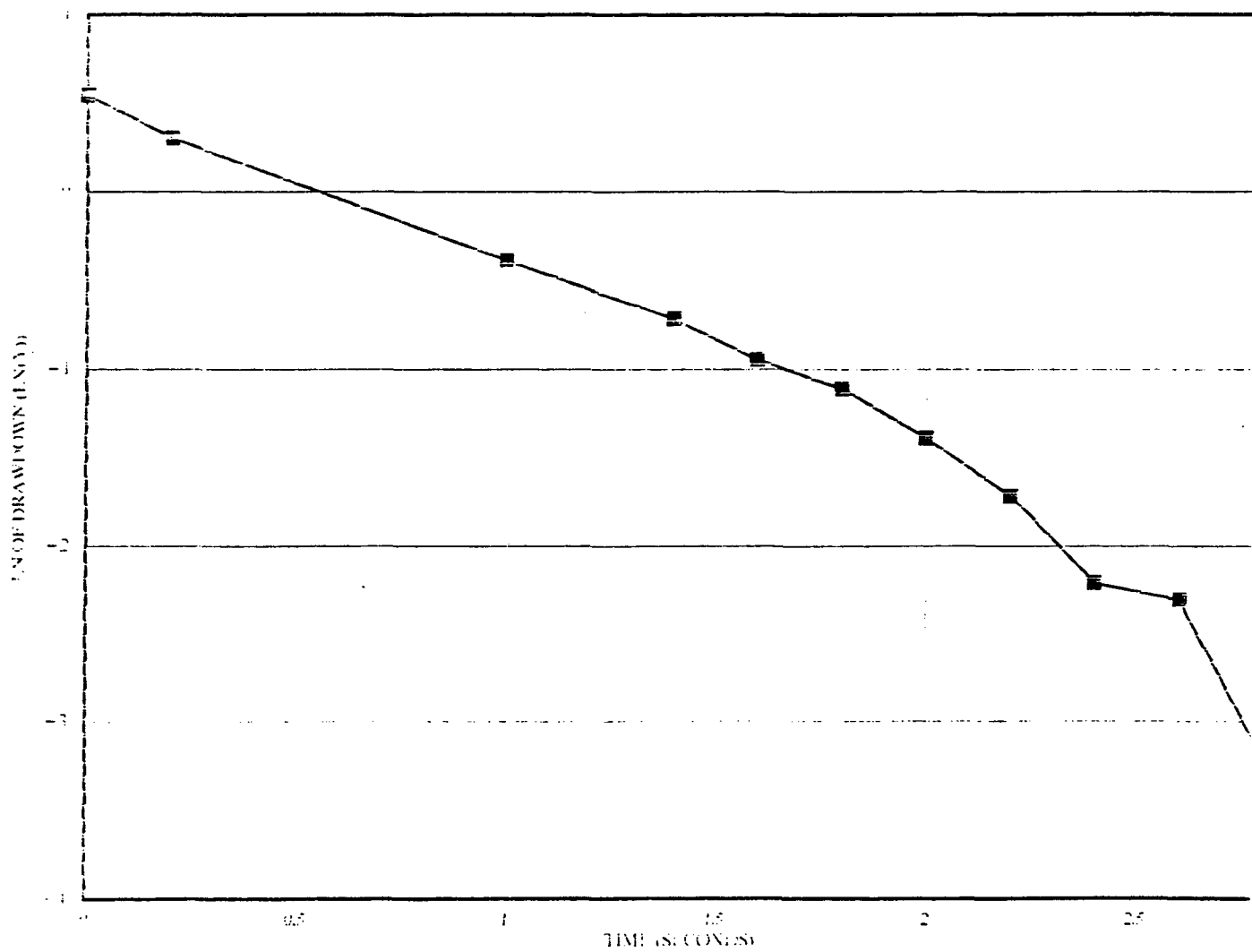


BOUNER AND RICE METHOD FOR INTERPRETATION OF SLUG TESTS: FOR UNCONFINED AND LEAKY CONFINED AQUIFERS.
 TO UTILIZE THIS WORKSHEET, ENTER YOUR DATA AT LOCATIONS MARKED BY AN "X".
 PROGRAM CAN INCLUDE EFFECTS OF SANDPACK DEWATERING (ASSUMING WATER IS RISING WITHIN THE SANDPACK).

TIME min	DEPTH TD	DRAWDOWN	TIME sec	LN	PROJECT NAME	PROJECT NO
1	11.78	1.730	0.00	0.5491	SHIMCO	20026.024
2	11.41	1.360	0.20	0.3075	ANALYST	PF-1 FALL
3	10.70	0.650	1.00	-0.0857	DATE COLLECTED	12-2-90
4	10.54	0.490	1.40	-0.7132	WELLS RISE (IN)	1 = sub c) = 1.0 in. = 0.0633 (radius in ft.)
5	10.44	0.390	1.60	-0.9416	EFFECTIVE SCREEN DIAMETER: (2 r sub w) =	8.0 in. = 0.3333 (radius in ft.)
6	10.36	0.330	1.80	-1.1867	EFFECTIVE SCREEN LENGTH: (L)	5.00 Ft.
7	10.30	0.250	2.00	-1.3863	MAX DRAWDOWN (IN SURSET): (Hmax)	-1.70 Ft.
8	10.23	0.180	2.20	-1.7146	STATIC WATER LEVEL: (SNL)	10.05 Ft.
9	10.16	0.110	2.40	-2.2073	DEPTH FROM SNL TO EFF. SCREEN BOTTOM: (H)	22.85 Ft.
10	10.15	0.100	2.60	-2.2026	TEST. AQUIFER DEPTH (SNL TO AQUIFER BOTTOM): (D)	175.00 Ft.
11	10.09	0.040	2.80	-3.2189	INCLUDE SANDPACK DEWATERING (ENTER 1 IF YES, 0 IF NO)?	0
12	10.07	0.020	3.00	-3.9120	SANDPACK'S SPECIFIC YIELD (Sy)	0.10
13	10.06	0.010	8.00	-4.6052	BOUNER AND RICE CURVE COEFFICIENTS:	
14	10.05	0.000	10.00	ERR	RATIO OF L/(r sub w) =	15.00
15					---LOG OF L/(r sub w) =	1.1761
16					FOR PARTIALLY PENETRATING WELLS--	
17					A =	1.93
18					B =	0.29
19					FOR FULLY PENETRATING WELLS--	
20					C =	1.38
21					---EVALUATION OF LN(Hr/(r sub w)):	
22					CONST.1 =	0.2602
23					CONST.2 =	6.1235 = (MAX. OF 6.0) = 6.0000
24					LN(Hr/(r sub w)) =	1.98
25					EFFECTIVE r sub c (for sandpack dewatering) = 0.0633	
26					(1/T)(LN(Yo/Yt)) (SLOPE) = -1.0E+00 sec ⁻¹ (-1)	
27					HYDRAULIC CONDUCTIVITY (K) = 1.48E-03 ft/sec (*****)	
28					4.51E-02 cm/sec (*****)	
29					Regression Output: t = 0-2.6 s	
30					Constant	6.47E-01
31					Std Err of Y Est	0.1620
32					R Squared	0.9750
33					no. of Observations	10
34					Degrees of Freedom	8
35					T Coefficient(s)	-1.0E+00
36					Std Err of Coef.	0.0610

RATE OF RECOVERY TEST: WELL F-1

FAIL



TO UTILIZE THIS WORKSHEET, ENTER YOUR DATA AT LOCATIONS MARKED BY AN "g".
FRESHMAN CAN INCLUDE EFFECTS OF SANDPACK DENSITIES ASSUMING WATER IS FLOWING WITHIN THE SANDPACK).

TIME AND DATE FOR OBSERVATION	TIME SEC	LN	WELL NO	WELL DEPTH	WELL SIZE	DATE
1	5.41	0.440	0.60	10.00	12.00	1962
2	5.75	0.320	0.20	11.00	12.00	1962
3	5.87	0.080	0.80	12.00	12.00	1962
4	10.05	0.020	1.00	13.00	12.00	1962
5						
6						
7						
8						
9						
10						
11						
12						
13						
14						
15						
16						
17						
18						
19						
20						
21						
22						
23						
24						
25						
26						
27						
28						
29						
30						
31						
32						
33						
34						
35						
36						
37						
38						
39						
40						
41						
42						
43						

WELL NO. 1

WELL DEPTH. 12.00

WELL SIZE. 12.00

WELL DATE. 1962

WELL TYPE. 1

WELL LOCATION. 1

WELL OWNER. 1

WELL STATUS. 1

WELL COMMENTS. 1

WELL NOTES. 1

WELL RECORD. 1

WELL DATA. 1

WELL ANALYSIS. 1

WELL DESIGN. 1

WELL CONSTRUCTION. 1

WELL OPERATION. 1

WELL MAINTENANCE. 1

WELL REPAIRS. 1

WELL REPLACEMENTS. 1

WELL REMOVALS. 1

WELL ABANDONMENTS. 1

WELL CLOSURES. 1

WELL RE-OPENINGS. 1

WELL RE-INSPECTIONS. 1

WELL RE-TESTS. 1

WELL RE-EVALUATIONS. 1

WELL RE-DESIGNS. 1

WELL RE-CONSTRUCTIONS. 1

WELL RE-OPERATIONS. 1

WELL RE-MAINTENANCES. 1

WELL RE-REPAIRS. 1

WELL RE-REPLACEMENTS. 1

WELL RE-REMOVALS. 1

WELL RE-ABANDONMENTS. 1

WELL RE-CLOSURES. 1

WELL RE-RE-OPENINGS. 1

WELL RE-RE-INSPECTIONS. 1

WELL RE-RE-TESTS. 1

WELL RE-RE-EVALUATIONS. 1

WELL RE-RE-DESIGNS. 1

WELL RE-RE-CONSTRUCTIONS. 1

WELL RE-RE-OPERATIONS. 1

WELL RE-RE-MAINTENANCES. 1

WELL RE-RE-REPAIRS. 1

WELL RE-RE-REPLACEMENTS. 1

WELL RE-RE-REMOVALS. 1

WELL RE-RE-ABANDONMENTS. 1

WELL RE-RE-CLOSURES. 1

WELL RE-RE-RE-OPENINGS. 1

WELL RE-RE-RE-INSPECTIONS. 1

WELL RE-RE-RE-TESTS. 1

WELL RE-RE-RE-EVALUATIONS. 1

WELL RE-RE-RE-DESIGNS. 1

WELL RE-RE-RE-CONSTRUCTIONS. 1

WELL RE-RE-RE-OPERATIONS. 1

WELL RE-RE-RE-MAINTENANCES. 1

WELL RE-RE-RE-REPAIRS. 1

WELL RE-RE-RE-REPLACEMENTS. 1

WELL RE-RE-RE-REMOVALS. 1

WELL RE-RE-RE-RE-ABANDONMENTS. 1

WELL RE-RE-RE-RE-CLOSURES. 1

WELL RE-RE-RE-RE-RE-OPENINGS. 1

WELL RE-RE-RE-RE-RE-INSPECTIONS. 1

WELL RE-RE-RE-RE-RE-TESTS. 1

WELL RE-RE-RE-RE-RE-EVALUATIONS. 1

WELL RE-RE-RE-RE-RE-DESIGNS. 1

WELL RE-RE-RE-RE-RE-CONSTRUCTIONS. 1

WELL RE-RE-RE-RE-RE-OPERATIONS. 1

WELL RE-RE-RE-RE-RE-MAINTENANCES. 1

WELL RE-RE-RE-RE-RE-REPAIRS. 1

WELL RE-RE-RE-RE-RE-REPLACEMENTS. 1

WELL RE-RE-RE-RE-RE-REMOVALS. 1

WELL RE-RE-RE-RE-RE-RE-ABANDONMENTS. 1

WELL RE-RE-RE-RE-RE-RE-CLOSURES. 1

WELL RE-RE-RE-RE-RE-RE-RE-OPENINGS. 1

WELL RE-RE-RE-RE-RE-RE-RE-INSPECTIONS. 1

WELL RE-RE-RE-RE-RE-RE-RE-TESTS. 1

WELL RE-RE-RE-RE-RE-RE-RE-EVALUATIONS. 1

WELL RE-RE-RE-RE-RE-RE-RE-DESIGNS. 1

WELL RE-RE-RE-RE-RE-RE-RE-CONSTRUCTIONS. 1

WELL RE-RE-RE-RE-RE-RE-RE-OPERATIONS. 1

WELL RE-RE-RE-RE-RE-RE-RE-MAINTENANCES. 1

WELL RE-RE-RE-RE-RE-RE-RE-REPAIRS. 1

WELL RE-RE-RE-RE-RE-RE-RE-REPLACEMENTS. 1

WELL RE-RE-RE-RE-RE-RE-RE-REMOVALS. 1

WELL RE-RE-RE-RE-RE-RE-RE-RE-ABANDONMENTS. 1

WELL RE-RE-RE-RE-RE-RE-RE-RE-CLOSURES. 1

WELL RE-RE-RE-RE-RE-RE-RE-RE-RE-OPENINGS. 1

WELL RE-RE-RE-RE-RE-RE-RE-RE-RE-INSPECTIONS. 1

WELL RE-RE-RE-RE-RE-RE-RE-RE-RE-TESTS. 1

WELL RE-RE-RE-RE-RE-RE-RE-RE-RE-EVALUATIONS. 1

WELL RE-RE-RE-RE-RE-RE-RE-RE-RE-DESIGNS. 1

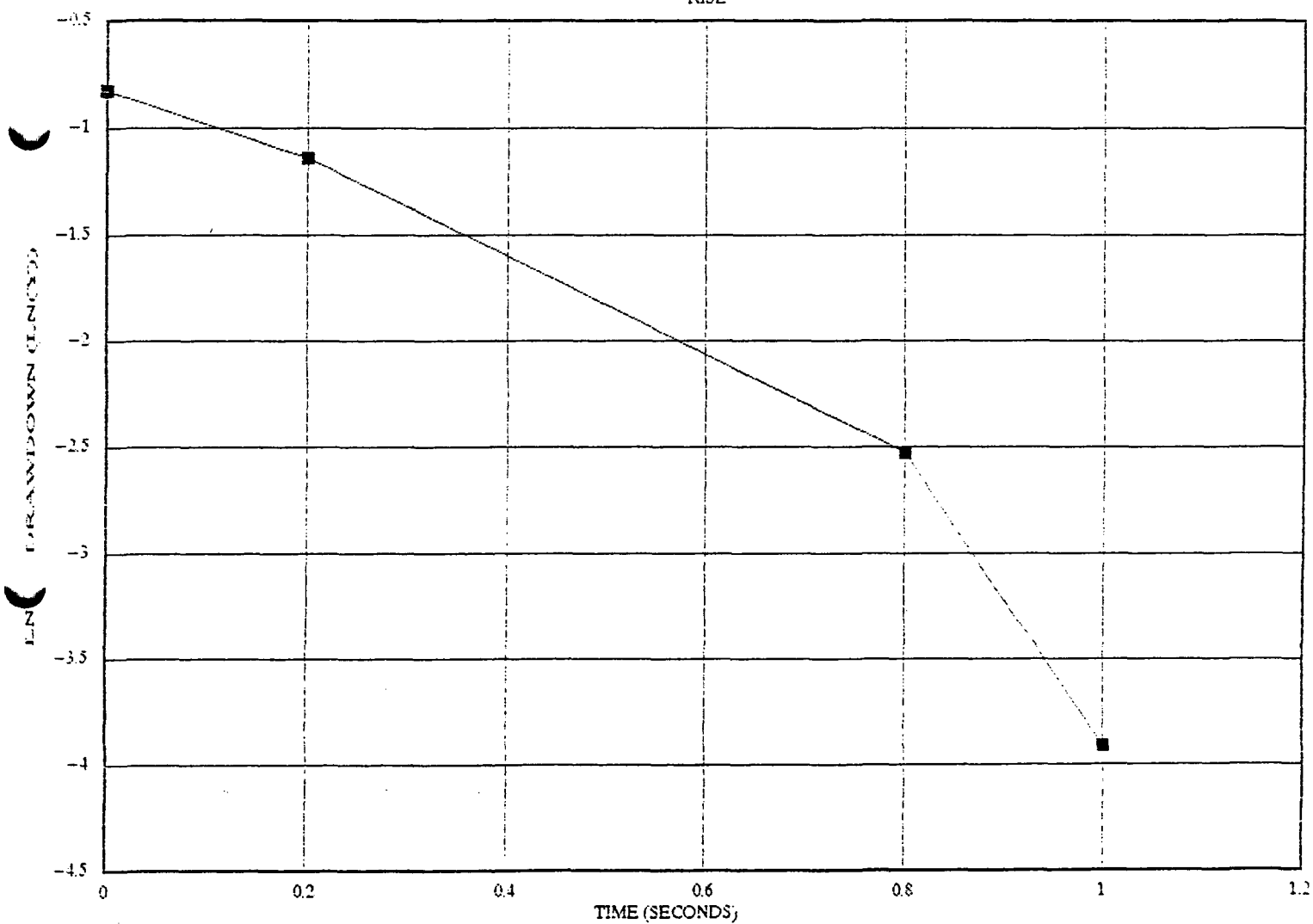
WELL RE-RE-RE-RE-RE-RE-RE-RE-RE-CONSTRUCTIONS. 1

WELL RE-RE-RE-RE-RE-RE-RE-RE-RE-OPERATIONS. 1

WELL RE-RE-RE-RE-RE-RE-RE-RE-RE

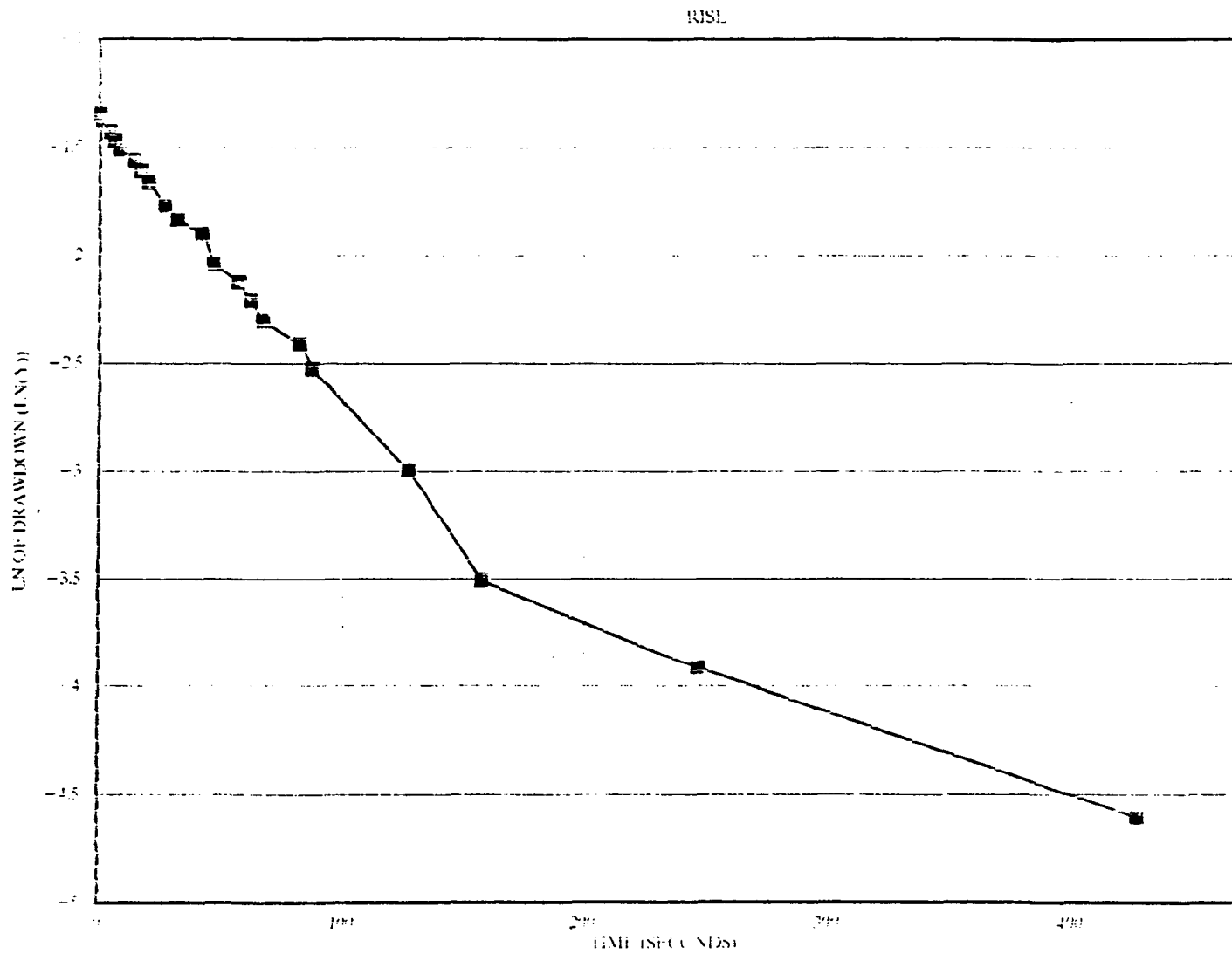
RATE OF RECOVERY TEST: WELL F-1

RISE



TIME	DATE	DEPTH TO DRAWDOWN	TIME	LN	PROJECT NAME	WIMCO
(H)	(M)	(FT)	(H)	(M)	PROJECT NO	20026.024
1	1	9.9	0.260	0.00	WELL NO	1F-1 RISE
2	1	9.61	0.250	1.00	ANALYST	1F02HLSKI
3	1	9.82	0.240	4.00	DATE COLLECTED	10-2-90
4	1	9.65	0.239	0.00	RISE PIPE (ID)	(2 r sub c) = 2.0 in. = 0.0833 (radius in ft.)
5	1	9.84	0.226	8.00	EFFECTIVE SCREEN DIAMETER (C r sub w) =	8.0 in. = 0.3333 (radius in ft.)
6	1	9.85	0.210	14.00	EFFECTIVE SCREEN LENGTH (L) =	5.00 Ft.
7	1	9.86	0.200	17.00	MAJ DRAWDOWN (IN SUBSET) (Ymax) =	0.26 Ft.
8	1	9.87	0.190	20.00	STATIC WATER LEVEL (SWL) =	10.06 Ft.
9	1	9.89	0.170	27.00	DEPTH FROM SWL TO EFF. SCREEN BOTTOM (W) =	166.25 Ft.
10	1	9.90	0.160	32.00	EST. AQUIFER DEPTH (SWL TO AQUIFER BOTTOM) (D) =	175.00 Ft.
11	1	9.91	0.150	42.00	INCLUDE SANDPACK DEWATERING (ENTER 1 IF YES, 0 IF NO)?	0
12	1	9.93	0.150	47.00	SANDPACK'S SPECIFIC YIELD (Sy) =	0.10
13	1	9.94	0.120	57.00	BOUNDARY AND RISE CURVE COEFFICIENTS:	
14	1	9.95	0.110	62.00	RATIO OF L/(r sub w) =	15.00
15	1	9.96	0.100	67.00	---LOE OF L/(r sub w) =	1.1761
16	1	9.97	0.090	82.00	FOR PARTIALLY PENETRATING WELLS--	
17	1	9.98	0.080	87.00	A =	1.93
18	1	10.01	0.050	127.00	B =	0.29
19	1	10.03	0.030	157.00	FOR FULLY PENETRATING WELLS--	
20	1	10.04	0.020	247.00	C =	1.38
21	1	10.05	0.010	427.00	---EVALUATION OF LN(Re/(r sub w)):	
22	1				CONST.1 =	0.1771
23	1				CONST.2 =	3.2677
24	1				LN(Re/(r sub w)) =	2.71
25	1					
26	1					
27	1				EFFECTIVE r sub c (for sandpack dewatering) =	0.0833
28	1				(1/T)(LN(Yo/Y1)) (SLOPE) =	-1.29E-02 sec ⁻¹ (-1)
29	1					
30	1				HYDRAULIC CONDUCTIVITY (K) =	2.42E-05 ft/sec
31	1					7.37E-04 cm/sec
32	1				t = 0-1273	
33	1					
34	1					
35	1				Constant	-1.39E+00
36	1				Std Err of Y Est	0.0292
37	1				R Squared	0.9962
38	1				No. of Observations	18
39	1				Degrees of Freedom	16
40	1					
41	1				X Coefficient(s)	-1.25E-02
42	1				Std Err of Coef.	0.0002
43	1					

RATE OF RECOVERY TEST: WELL F-2

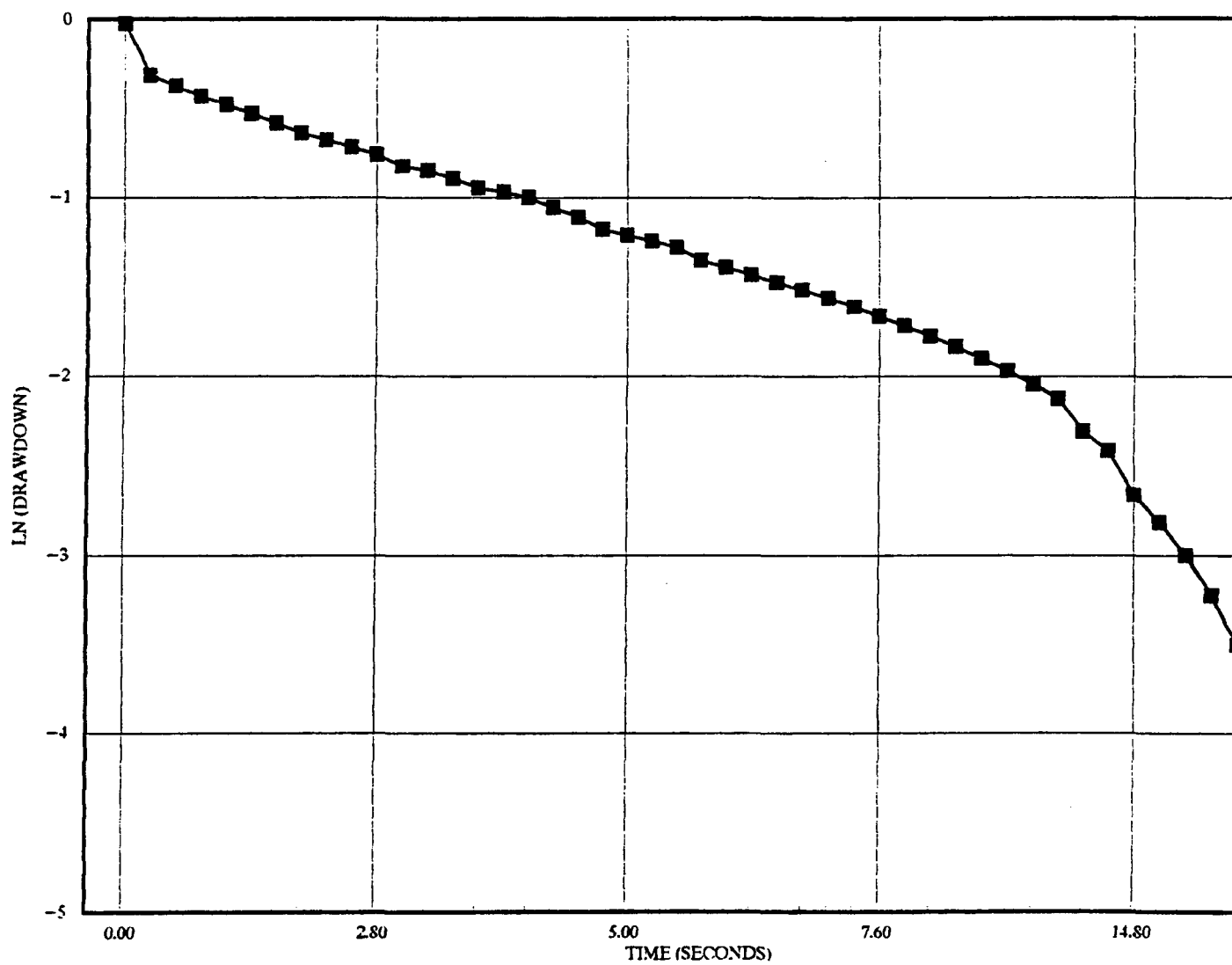


BOUWER AND RICE METHOD FOR INTERPRETATION OF SLUR TESTS: FOR UNCONFINED AND LEAKY CONFINED AQUIFERS.
 TO UTILIZE THIS WORKSHEET, ENTER YOUR DATA AT LOCATIONS MARKED BY AN "X".
 PROGRAM CAN INCLUDE EFFECTS OF SANDPACK DEWATERING (ASSUMING WATER IS RISING WITHIN THE SANDPACK).

TIME min	DEPTH TO WATER Ft.	DEPTH TO DRAINAGE Ft.	TIME sec	LN	PROJECT NAME	PROJECT NO	WELL NO	ANALYST	DATE COLLECTED	WELL TYPE	WELL DEPTH (ft)	WELL RADIUS (ft)	SCREEN LENGTH (ft)	MAX DRAWDOWN (IN SUBSET)	STATIC WATER LEVEL (SWL)	DEPTH FROM SWL TO EFF. SCREEN BOTTOM (H)	TEST. AQUIFER DEPTH (SWL TO AQUIFER BOTTOM) (D)	INCLUDE SANDPACK DEWATERING (ENTER 1 IF YES, 0 IF NO)?	SANDPACK'S SPECIFIC YIELD (Sy)
1	6.03	0.780	0.00	-0.02	SHIMCO	20026.024	1	BOUWER	10-1-90	1	2.0 in. = 0.0833 (radius in ft.)	0.3333 (radius in ft.)	5.00 ft.	0.98 ft.	7.61 ft.	9.53 ft.	175.00 ft.	0	0.10
2	6.08	0.750	0.40	-0.31															
3	6.32	0.690	1.20	-0.37															
4	6.36	0.650	1.40	-0.43															
5	6.39	0.620	1.60	-0.48															
6	6.42	0.590	1.80	-0.53															
7	6.45	0.560	2.00	-0.58															
8	6.48	0.530	2.20	-0.63															
9	6.50	0.510	2.40	-0.67															
10	6.52	0.490	2.60	-0.71															
11	6.54	0.470	2.80	-0.76															
12	6.57	0.440	3.00	-0.82															
13	6.58	0.430	3.20	-0.84															
14	6.60	0.410	3.40	-0.89															
15	6.62	0.390	3.60	-0.94															
16	6.63	0.380	3.80	-0.97															
17	6.64	0.370	4.00	-0.99															
18	6.66	0.350	4.20	-1.05															
19	6.68	0.330	4.40	-1.11															
20	6.70	0.310	4.60	-1.17															
21	6.71	0.300	5.00	-1.20															
22	6.72	0.290	5.20	-1.24															
23	6.73	0.280	5.40	-1.27															
24	6.75	0.260	5.60	-1.35															
25	6.76	0.250	6.00	-1.39															
26	6.77	0.240	6.20	-1.43															
27	6.78	0.230	6.40	-1.47															
28	6.79	0.220	6.60	-1.51															
29	6.80	0.210	6.80	-1.56															
30	6.81	0.200	7.00	-1.61															
31	6.82	0.190	7.60	-1.66															
32	6.83	0.180	8.00	-1.71															
33	6.84	0.170	8.40	-1.77															
34	6.85	0.160	8.60	-1.83															
35	6.86	0.150	9.00	-1.90															
36	6.87	0.140	9.40	-1.97															
37	6.88	0.130	9.80	-2.04															
38	6.89	0.120	11.80	-2.12															
39	6.91	0.100	12.80	-2.30															
40	6.92	0.090	12.80	-2.41															
41	6.94	0.070	14.80	-2.66															
42	6.95	0.060	15.80	-2.81															
43	6.96	0.050	18.80	-3.06															
44	6.97	0.040	26.80	-3.22															
45	6.98	0.030	22.60	-3.51															
46	6.99	0.020	27.60	-3.91															
47	7.00	0.010	32.60	-4.61															

t=0.4-9.85

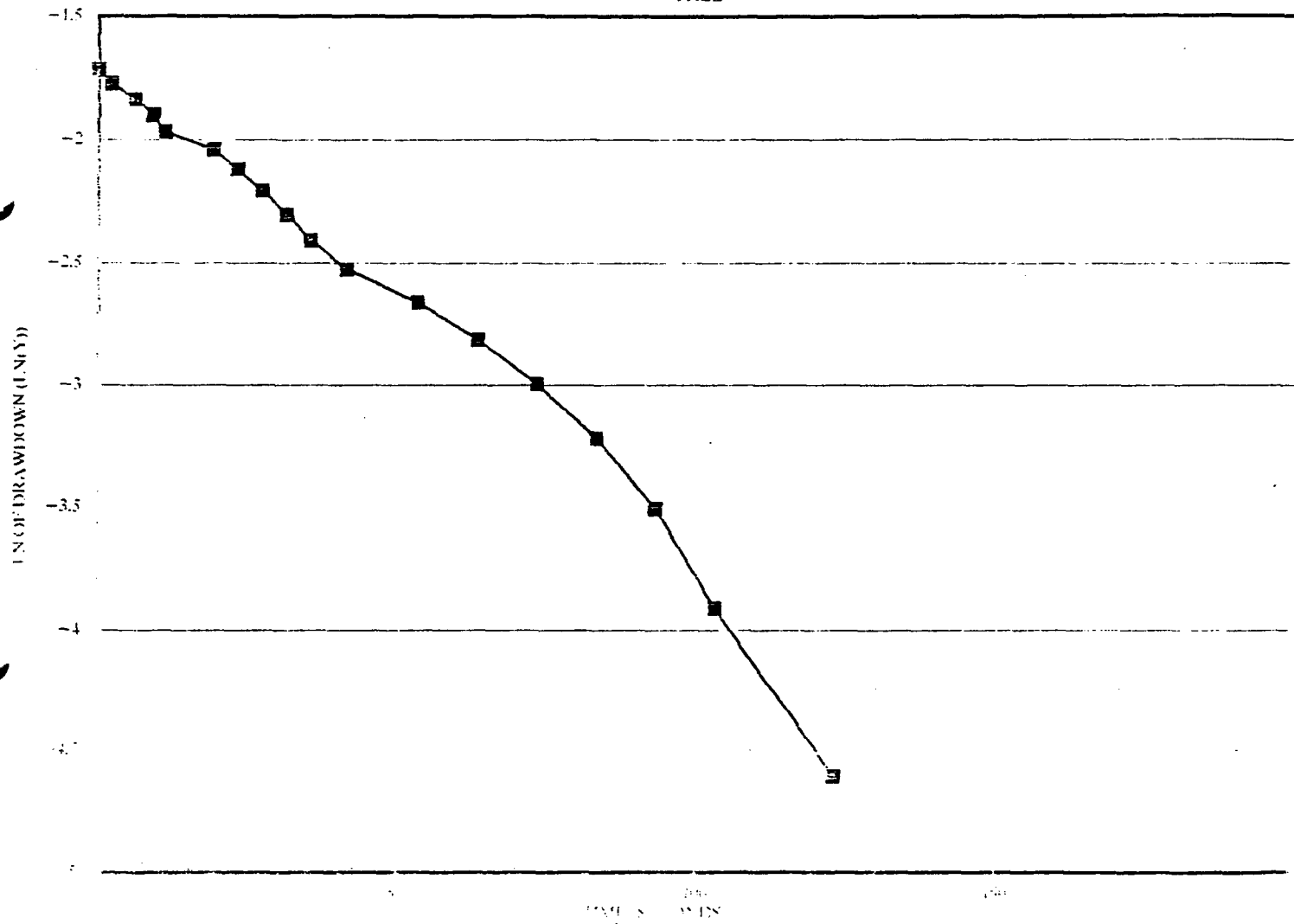
RATE OF RECOVERY WELL M-2 RISE



TIME MIN	DEPTH TO WATER FT.	TIME SEC	LN	PROJECT NO	WELL NO	DATE COLLECTED	WELL NAME	WELL TYPE	WELL DATE	WELL NAME	WELL TYPE	WELL DATE
1	8.15	0.180	0.00	-1.7148	20000.024	12-1-50	WELL NO	12-1-50	WELL NAME	WELL TYPE	WELL DATE	WELL NAME
2	8.14	0.170	0.00	-1.7720		12-1-50	WELL NO	12-1-50	WELL NAME	WELL TYPE	WELL DATE	WELL NAME
3	8.13	0.160	0.00	-1.8326		12-1-50	WELL NO	12-1-50	WELL NAME	WELL TYPE	WELL DATE	WELL NAME
4	8.12	0.150	9.00	-1.8971		12-1-50	WELL NO	12-1-50	WELL NAME	WELL TYPE	WELL DATE	WELL NAME
5	8.11	0.140	11.00	-1.9661		12-1-50	WELL NO	12-1-50	WELL NAME	WELL TYPE	WELL DATE	WELL NAME
6	8.10	0.130	19.00	-2.0402		12-1-50	WELL NO	12-1-50	WELL NAME	WELL TYPE	WELL DATE	WELL NAME
7	8.09	0.120	25.00	-2.1203		12-1-50	WELL NO	12-1-50	WELL NAME	WELL TYPE	WELL DATE	WELL NAME
8	8.08	0.110	27.00	-2.2073		12-1-50	WELL NO	12-1-50	WELL NAME	WELL TYPE	WELL DATE	WELL NAME
9	8.07	0.100	31.00	-2.3026		12-1-50	WELL NO	12-1-50	WELL NAME	WELL TYPE	WELL DATE	WELL NAME
10	8.06	0.090	35.00	-2.4079		12-1-50	WELL NO	12-1-50	WELL NAME	WELL TYPE	WELL DATE	WELL NAME
11	8.05	0.080	41.00	-2.5257		12-1-50	WELL NO	12-1-50	WELL NAME	WELL TYPE	WELL DATE	WELL NAME
12	8.04	0.070	55.00	-2.6593		12-1-50	WELL NO	12-1-50	WELL NAME	WELL TYPE	WELL DATE	WELL NAME
13	8.03	0.060	65.00	-2.8134		12-1-50	WELL NO	12-1-50	WELL NAME	WELL TYPE	WELL DATE	WELL NAME
14	8.02	0.050	73.00	-2.9957		12-1-50	WELL NO	12-1-50	WELL NAME	WELL TYPE	WELL DATE	WELL NAME
15	8.01	0.040	85.00	-3.2189		12-1-50	WELL NO	12-1-50	WELL NAME	WELL TYPE	WELL DATE	WELL NAME
16	8.00	0.030	95.00	-3.5066		12-1-50	WELL NO	12-1-50	WELL NAME	WELL TYPE	WELL DATE	WELL NAME
17	7.99	0.020	105.00	-3.9120		12-1-50	WELL NO	12-1-50	WELL NAME	WELL TYPE	WELL DATE	WELL NAME
18	7.98	0.010	125.00	-4.6052		12-1-50	WELL NO	12-1-50	WELL NAME	WELL TYPE	WELL DATE	WELL NAME
19	7.97	0.000	185.00	ERR		12-1-50	WELL NO	12-1-50	WELL NAME	WELL TYPE	WELL DATE	WELL NAME
20						12-1-50	WELL NO	12-1-50	WELL NAME	WELL TYPE	WELL DATE	WELL NAME
21						12-1-50	WELL NO	12-1-50	WELL NAME	WELL TYPE	WELL DATE	WELL NAME
22						12-1-50	WELL NO	12-1-50	WELL NAME	WELL TYPE	WELL DATE	WELL NAME
23						12-1-50	WELL NO	12-1-50	WELL NAME	WELL TYPE	WELL DATE	WELL NAME
24						12-1-50	WELL NO	12-1-50	WELL NAME	WELL TYPE	WELL DATE	WELL NAME
25						12-1-50	WELL NO	12-1-50	WELL NAME	WELL TYPE	WELL DATE	WELL NAME
26						12-1-50	WELL NO	12-1-50	WELL NAME	WELL TYPE	WELL DATE	WELL NAME
27						12-1-50	WELL NO	12-1-50	WELL NAME	WELL TYPE	WELL DATE	WELL NAME
28						12-1-50	WELL NO	12-1-50	WELL NAME	WELL TYPE	WELL DATE	WELL NAME
29						12-1-50	WELL NO	12-1-50	WELL NAME	WELL TYPE	WELL DATE	WELL NAME
30						12-1-50	WELL NO	12-1-50	WELL NAME	WELL TYPE	WELL DATE	WELL NAME
31						12-1-50	WELL NO	12-1-50	WELL NAME	WELL TYPE	WELL DATE	WELL NAME
32						12-1-50	WELL NO	12-1-50				

RATE OF RECOVERY TEST: WELL E-3

FALL

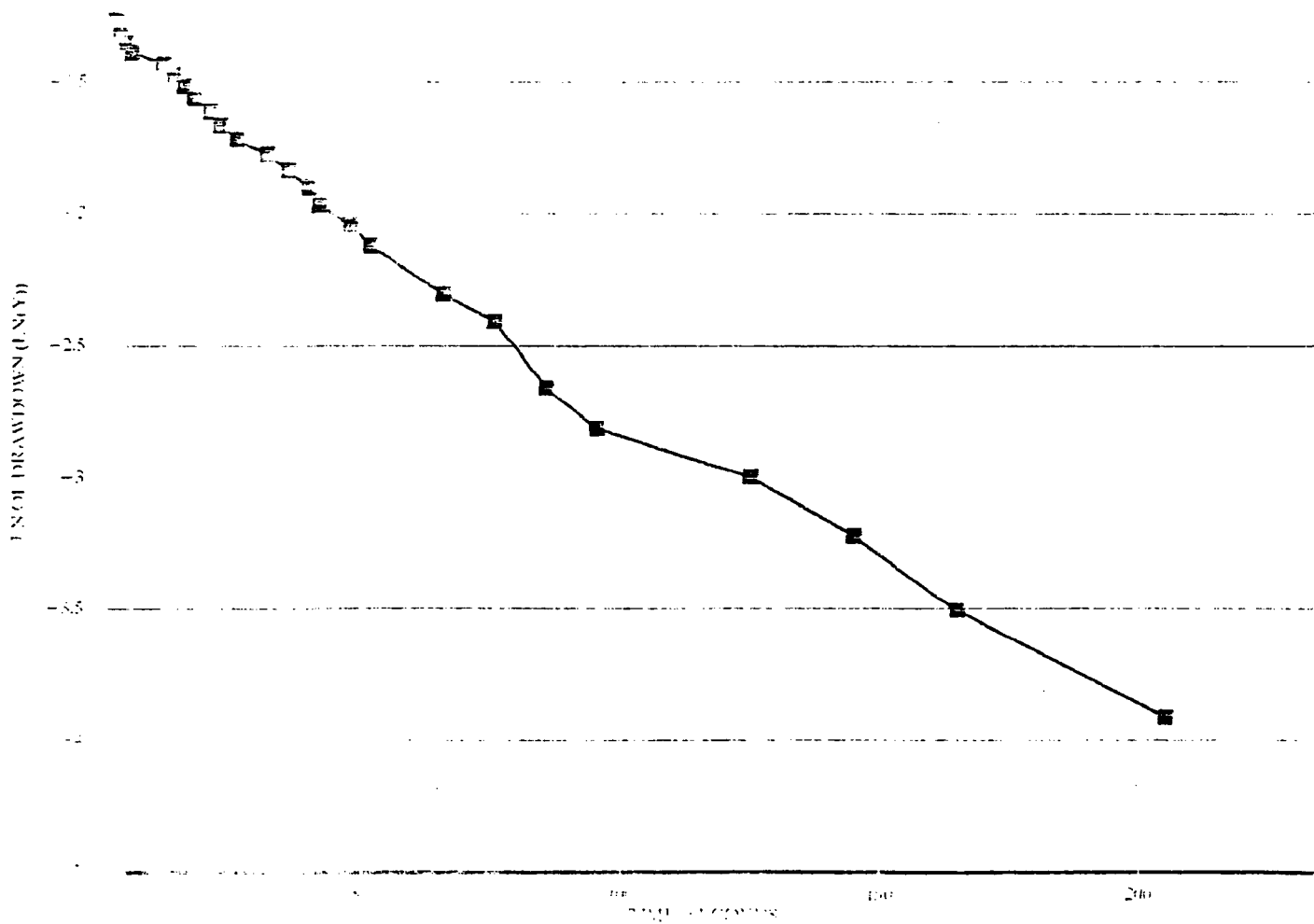


BOUWER AND RICE METHOD FOR INTERPRETATION OF SLUG TESTS: FOR UNCONFINED AND LEAKY CONFINED AQUIFERS.
 TO UTILIZE THIS WORKSHEET, ENTER YOUR DATA AT LOCATIONS MARKED BY AN "X".
 PROGRAM CAN INCLUDE EFFECTS OF SANDPACK DEWATERING (ASSUMING WATER IS RISING WITHIN THE SANDPACK).

TIME min	DEPTH TO WATER Ft.	TIME sec	LN	PROJECT NAME	WELL NO
1	7.96	0.010	0.00	WAL-157	12-14-90
2	7.86	0.250	2.00	DATE COLLECTED	12-14-90
3	7.69	0.280	2.80	RISER PIPE (ID):	(2 r sub c) = 2.0 in. = 0.0833 (radius in ft.)
4	7.70	0.270	3.00	EFFECTIVE SCREEN DIAMETER:	(2 r sub w) = 8.0 in. = 0.3333 (radius in ft.)
5	7.71	0.260	4.00	EFFECTIVE SCREEN LENGTH: (L)	= 11.60 Ft.
6	7.72	0.250	5.00	MAX DRAWDOWN (IN SUBSET): (Ymax)	= 0.26 Ft.
7	7.73	0.240	11.00	STATIC WATER LEVEL: (SNL)	= 7.97 Ft.
8	7.74	0.230	13.00	DEPTH FROM SNL TO EFF. SCREEN BOTTOM: (H)	= 11.60 Ft.
9	7.75	0.220	15.00	TEST. AQUIFER DEPTH (SNL TO AQUIFER BOTTOM): (D)	= 175.00 Ft.
10	7.76	0.210	17.00	INCLUDE SANDPACK DEWATERING (ENTER 1 IF YES, 0 IF NO)?	1
11	7.77	0.200	20.00	SANDPACK'S SPECIFIC YIELD (Sy)	= 0.10
12	7.78	0.190	22.00	BOUWER AND RICE CURVE COEFFICIENTS:	
13	7.79	0.180	25.00	RATIO OF L/(r sub w) = 34.80	
14	7.80	0.170	31.00	---LOG OF L/(r sub w) = 1.5416	
15	7.81	0.160	35.00	FOR PARTIALLY PENETRATING WELLS--	
16	7.82	0.150	39.00	A = 2.60	
17	7.83	0.140	41.00	B = 0.36	
18	7.84	0.130	47.00	FOR FULLY PENETRATING WELLS--	
19	7.85	0.120	51.00	C = 2.03	
20	7.87	0.100	65.00	---EVALUATION OF LN(Re/(r sub w)):	
21	7.88	0.090	75.00	CONST.1 = 0.3099	
22	7.90	0.070	85.00	CONST.2 = 6.1948 = (MAX. OF 6.0) = 6.0000	
23	7.91	0.060	95.00	LN(Re/(r sub w)) = 2.24	
24	7.92	0.050	125.00	EFFECTIVE r sub c (for sandpack dewatering) = 0.1318	
25	7.93	0.040	145.00	(1/T)(LN(Yo/Yt)) (SLOPE) = -1.55E-02 sec ⁻¹ (-1)	
26	7.94	0.030	165.00	HYDRAULIC CONDUCTIVITY (K) = 2.61E-05 ft/sec	
27	7.95	0.020	205.00	7.95E-04 cm/sec	
28				t = 4-205	
29				Regression Output:	
30				Constant -1.28E+00	
31				Std Err of Est 0.0201	
32				R Squared 0.9622	
33				No. of Observations 7	
34				Degrees of Freedom 5	
35				K Coefficient(s) -1.55E-02	
36				Std Err of Coef. 6.0914	

RATE OF RECOVERY TEST: WELL E-3

RISE

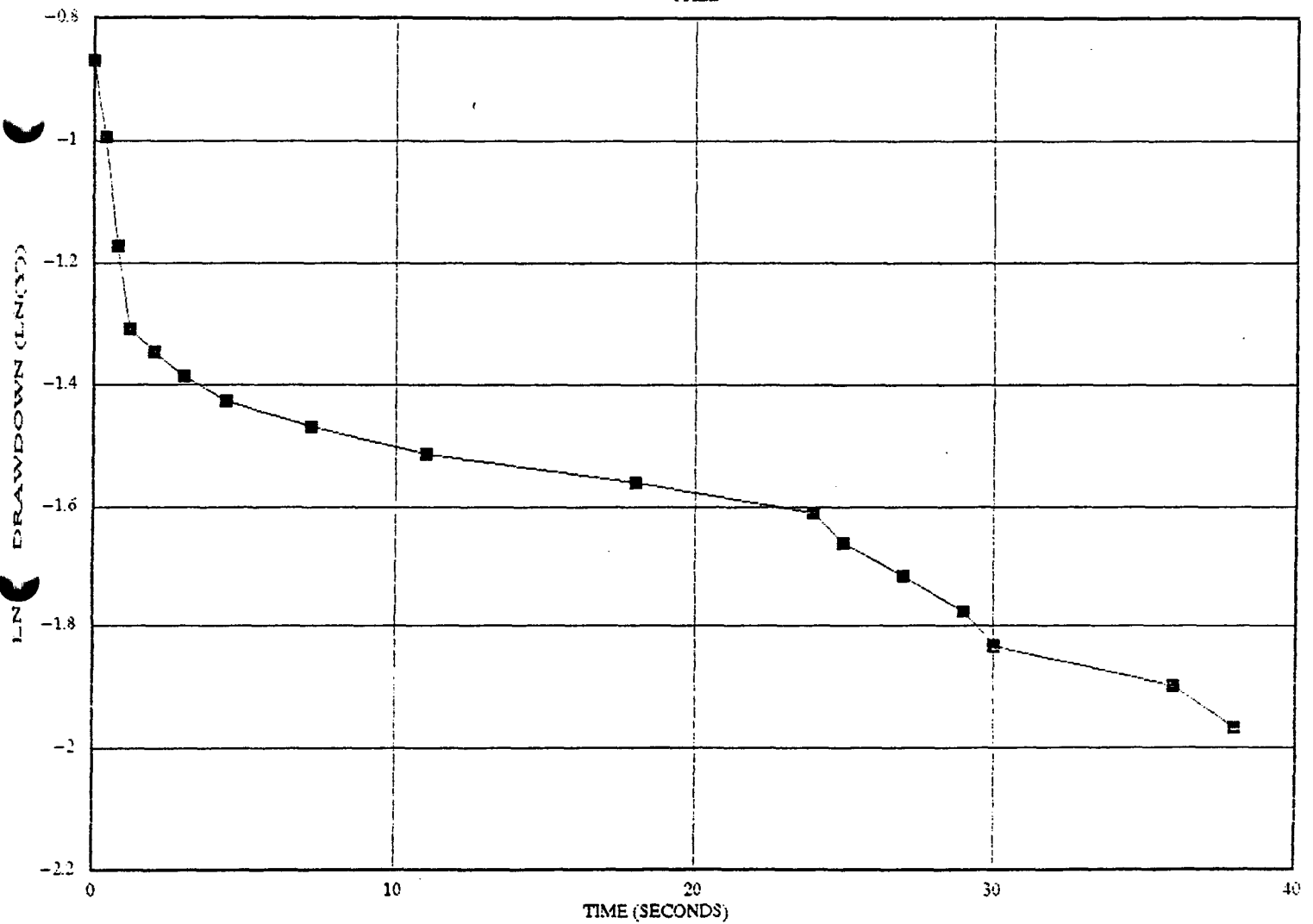


PROGRAM CAN INCLUDE EFFECTS OF SANDFILL Dewatering (ASSUMING WATER IS RISING WITHIN THE SANDFILL).

TIME	INCEPT	TIME	LN	PROJECT NAME	PROJECT NO	DATE
(1)	(2)	(3)	(4)	(5)	(6)	(7)
1	10.42	0.420	0.00	WELL NO	W-2 FALL	
2	10.43	0.370	0.40	ANALYST	ELIAS	
3	10.37	0.310	0.80	DATE COLLECTED	11-2-90	
4	10.33	0.270	1.20	WELDER PIPE (ID):	(2 r sub c) =	2.0 in. = 0.0833 (radius in ft.)
5	10.32	0.260	2.00	EFFECTIVE SCREEN DIAMETER:	(2 r sub w) =	6.0 in. = 0.3333 (radius in ft.)
6	10.31	0.250	3.00	EFFECTIVE SCREEN LENGTH: (L)	=	5.00 Ft.
7	10.29	0.240	4.40	MAX DRANDOWN (IN SUSSET): (Ymax)	=	-0.43 Ft.
8	10.29	0.230	7.20	STATIC WATER LEVEL: (SWL)	=	10.06 Ft.
9	10.28	0.220	11.00	DEPTH FROM SWL TO EFF. SCREEN BOTTOM: (H)	=	166.25 Ft.
10	10.27	0.210	15.00	TEST. AQUIFER DEPTH (SWL TO AQUIFER BOTTOM): (D)	=	175.00 Ft.
11	10.26	0.200	24.00	INCLUDE SANDPACK DEWATERING (ENTER 1 IF YES, 0 IF NO)?		1
12	10.25	0.190	25.60	SANDPACK'S SPECIFIC YIELD (Sy)	=	0.10
13	10.24	0.180	27.00	BOUNCE AND RICE CURVE COEFFICIENTS:		
14	10.23	0.170	29.60	RATIO OF L/(r sub w) =		15.00
15	10.22	0.160	30.00	---LOG OF L/(r sub w) =		1.1761
16	10.21	0.150	36.00	FOR PARTIALLY PENETRATING WELLS--		
17	10.20	0.140	38.00	A =	1.93	
18				B =	0.29	
19				FOR FULLY PENETRATING WELLS--		
20				C =	1.38	
21				---EVALUATION OF LN(Re/(r sub w)):		
22				CONST.1 =	0.1771	
23				CONST.2 =	3.2677	(MAX. OF 6.0) = 3.2677
24				LN(Re/(r sub w)) =	2.71	
25				EFFECTIVE r sub c (for sandpack dewatering) =	0.1318	
26				(1/T)(LN(Yo/Yt)) (SLOPE) =	-8.88E-03 sec ⁻¹	
27				HYDRAULIC CONDUCTIVITY (K) =	4.17E-05 ft/sec	(*****)
28					1.27E-03 cm/sec	(*****)
29				Regression Outputs:		
30				Constant	-1.40E+00	
31				Std Err of Y Est	0.0122	
32				R Squared	0.9783	
33				No. of Observations	5	
34				Degrees of Freedom	3	
35				X Coefficient(s)	-8.28E-03	
36				Std Err of Coef.	0.0008	

RATE OF RECOVERY TEST: WELL F-2

FALL

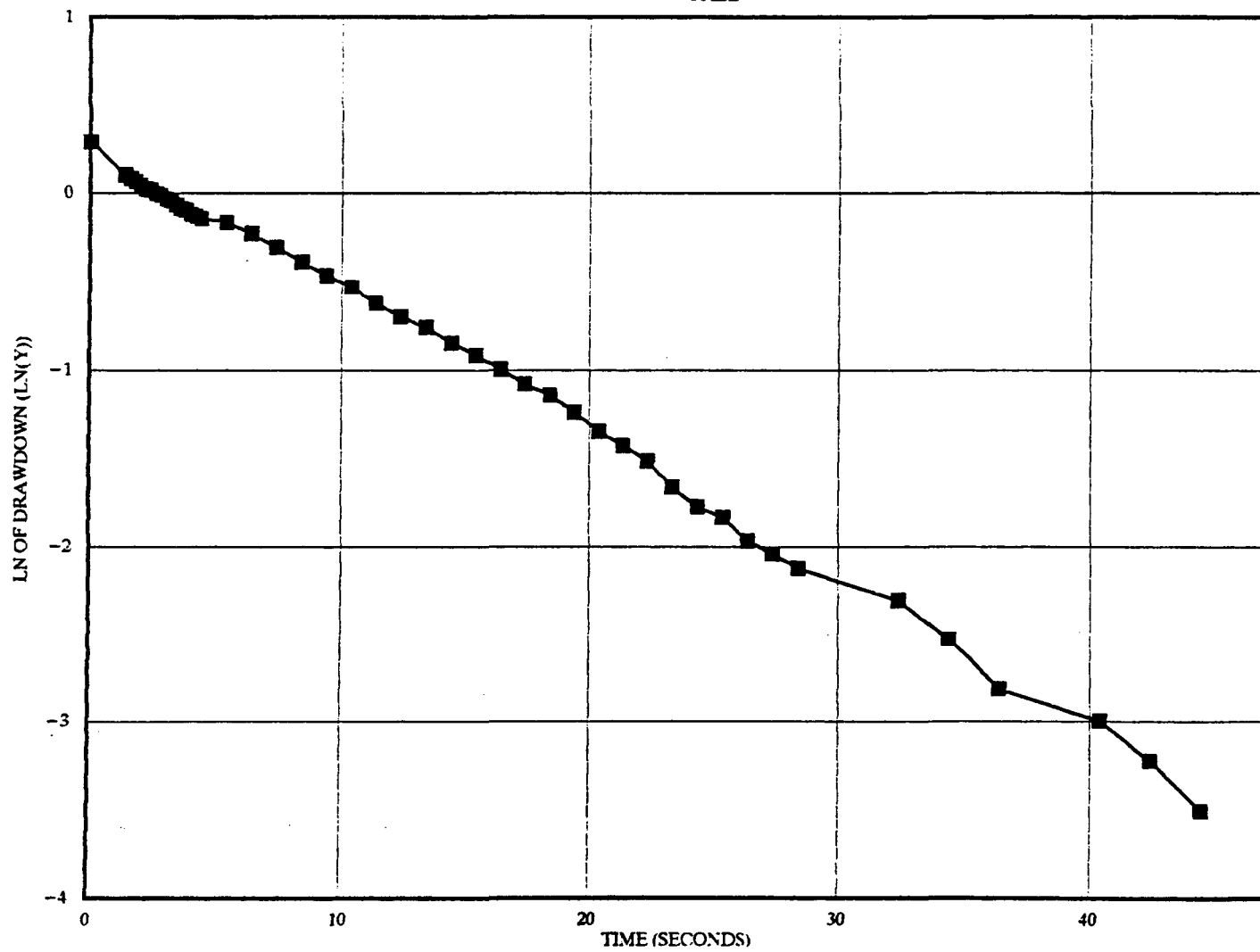


BOUNER AND RICE METHOD FOR INTERPRETATION OF SLUG TESTS: FOR UNCONFINED AND LEAKY CONFINED AQUIFERS.
 TO UTILIZE THIS WORKSHEET, ENTER YOUR DATA AT LOCATIONS MARKED BY AN "X".
 PROGRAM CAN INCLUDE EFFECTS OF SANDPACK DEWATERING (ASSUMING WATER IS RISING WITHIN THE SANDPACK).

TIME min	DEPTH TO DRAWDOWN	TIME sec	LN	PROJECT NAME	WIMED
(1)	(2)	(3)	(4)	(5)	(6)
1	11.80	1.340	0.00	PROJECT NO	20626.024
2	11.57	1.110	1.40	WELL NO	11018 FALL
3	11.55	1.090	1.60	ANALYST	BUCHALSKI
4	11.53	1.070	1.80	DATE COLLECTED	04-Jan-91
5	11.51	1.050	2.00	TRISER PIPE (ID):	(2 r sub c) = 2.0 in. = 0.0833 (radius in ft.)
6	11.49	1.030	2.20	EFFECTIVE SCREEN DIAMETER:(2 r sub w) =	6.0 in. = 0.3333 (radius in ft.)
7	11.48	1.020	2.40	EFFECTIVE SCREEN LENGTH: (L) =	5.00 Ft.
8	11.46	1.000	2.60	MAX DRAWDOWN (IN SUBSET): (Ymax) =	-1.34 Ft.
9	11.45	0.990	2.80	STATIC WATER LEVEL: (SWL) =	10.46 Ft.
10	11.43	0.970	3.00	DEPTH FROM SWL TO EFF. SCREEN BOTTOM: (H) =	91.00 Ft.
11	11.42	0.960	3.20	TEST, AQUIFER DEPTH (SWL TO AQUIFER BOTTOM): (D) =	175.00 Ft.
12	11.40	0.940	3.40	INCLUDE SANDPACK DEWATERING (ENTER 1 IF YES, 0 IF NO)?	0
13	11.38	0.920	3.60	SANDPACK'S SPECIFIC YIELD (Sy) =	0.10
14	11.37	0.910	3.80	BOUNER AND RICE CURVE COEFFICIENTS:	
15	11.35	0.890	4.00	RATIO OF L/(r sub w) =	15.00
16	11.34	0.880	4.20	---LOG OF L/(r sub w) =	1.1761
17	11.33	0.870	4.40	FOR PARTIALLY PENETRATING WELLS--	
18	11.31	0.850	4.60	A =	1.93
19	11.26	0.800	4.80	B =	0.29
20	11.20	0.740	5.00	FOR FULLY PENETRATING WELLS--	
21	11.14	0.680	5.20	C =	1.38
22	11.09	0.630	5.40	---EVALUATION OF LN(Re/(r sub w)):	
23	11.05	0.590	5.60	CONST.1 =	0.1961
24	11.00	0.540	5.80	CONST.2 =	5.5294 =(MAX. OF 6.0)= 5.5294
25	10.96	0.500	6.00	LN(Re/(r sub w)) =	2.31
26	10.93	0.470	6.20		
27	10.89	0.430	6.40	EFFECTIVE r sub c (for sandpack dewatering) =	0.0833
28	10.86	0.400	6.60	(1/T)(LN(Yd/Yt)) (SLOPE) =	-8.15E-02 sec ⁻¹ (-1)
29	10.83	0.370	6.80		
30	10.80	0.340	7.00	HYDRAULIC CONDUCTIVITY (K) =	1.31E-04 ft/sec
31	10.78	0.320	7.20		3.99E-03 cm/sec
32	10.75	0.290	7.40		
33	10.72	0.260	7.60	Regression Output:	t=0-44.4s
34	10.70	0.240	7.80	Constant	2.59E-01
35	10.69	0.220	8.00	Std Err of Y Est	0.0606
36	10.65	0.190	8.20	R Squared	0.9966
37	10.63	0.170	8.40	No. of Observations	47
38	10.62	0.160	8.60	Degrees of Freedom	45
39	10.60	0.140	8.80		
40	10.59	0.130	9.00	Y Coefficient(s)	-8.15E-02
41	10.56	0.120	9.20	Std Err of Coef.	0.0007
42	10.54	0.100	9.40		
43	10.54	0.080	9.60		
44	10.52	0.060	9.80		
45	10.51	0.050	10.00		
46	10.50	0.040	10.20		
47	10.49	0.030	10.40		
48					

RATE OF RECOVERY TEST: WELL P101B

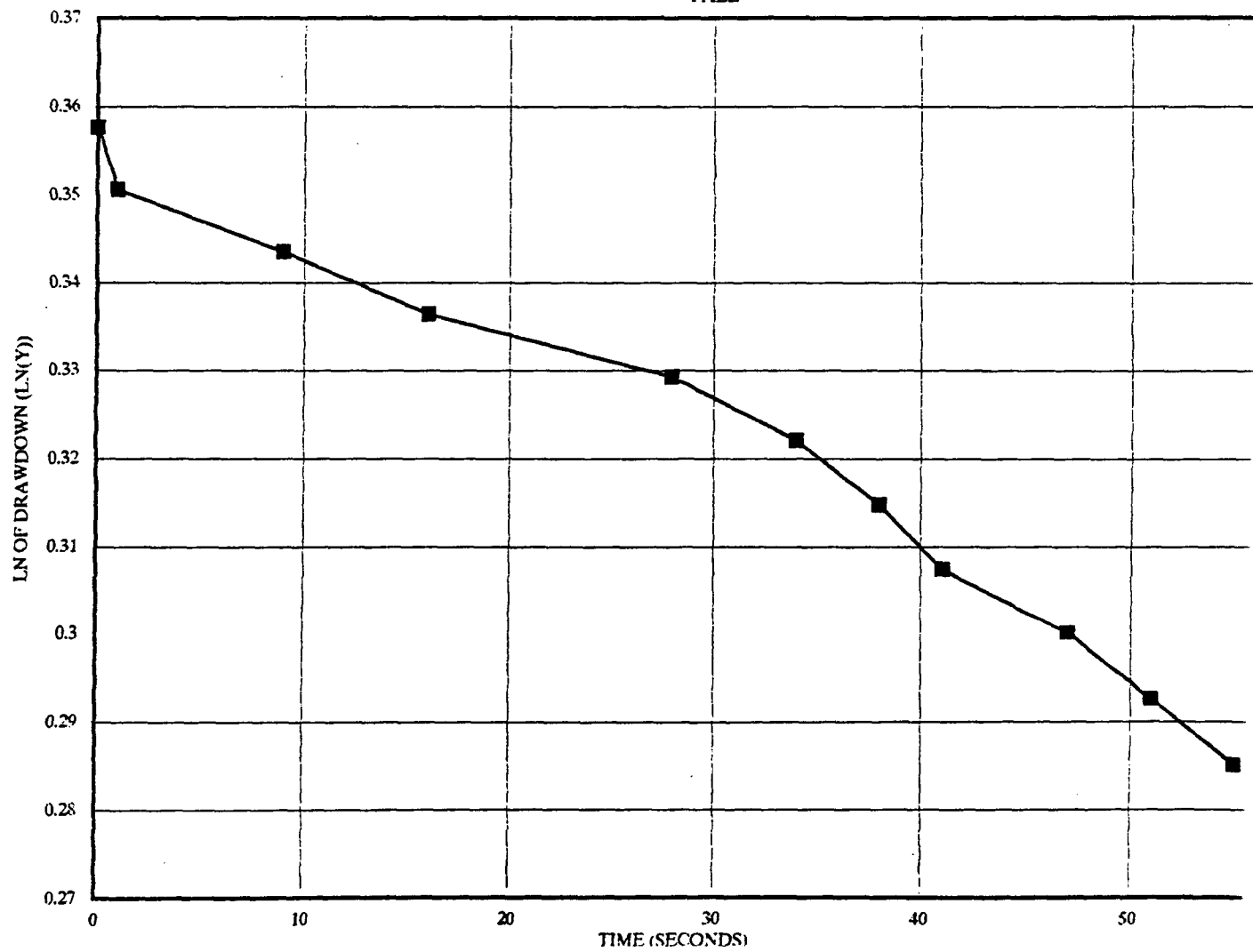
FALL



TIME sec	DEPTH TO DRAWDOWN	TIME sec	LN	PROJECT NO	PROJECT NAME
(1)	(2)	(3)	(4)	(5)	(6)
1	11.06	1.430	0.00	03577	WELL NO
2	10.99	1.420	1.00	03507	ANALYST
3	10.95	1.410	9.00	03436	DATE COLLECTED
4	10.57	1.400	16.00	03365	DRISER PIPE (ID):
5	10.96	1.390	28.00	03293	EFFECTIVE SCREEN DIAMETER:(2 r sub w) =
6	10.95	1.380	34.00	03221	EFFECTIVE SCREEN LENGTH: (L) =
7	10.94	1.370	38.00	03148	MAX DRAWDOWN (IN GUSET): (Ymax) =
8	10.93	1.360	41.00	03075	STATIC WATER LEVEL: (SML) =
9	10.92	1.350	47.00	03001	DEPTH FROM SML TO EFF. SCREEN BOTTOM: (H) =
10	10.91	1.340	51.00	02927	TEST, AQUIFER DEPTH (SML TO AQUIFER BOTTOM): (D) =
11	10.90	1.330	55.00	02852	INCLUDE SANDPACK DEWATERING (ENTER 1 IF YES, 0 IF NO)?
12					SANDPACK'S SPECIFIC YIELD (SY) =
13					
14					RATIOS AND RICE CURVE COEFFICIENTS:
15					RATIO OF L/(r sub w) =
16					---LOG OF L/(r sub w) =
17					FOR PARTIALLY PENETRATING WELLS--
18					A =
19					B =
20					FOR FULLY PENETRATING WELLS--
21					C =
22					
23					---EVALUATION OF LN(Re/(r sub w)):
24					CONST.1 =
25					CONST.2 =
26					LN(Re/(r sub w) =
27					
28					EFFECTIVE r sub c (for sandpack dewatering) =
29					(1/T)(LN(Yo/Yt)) (SLOPE) =
30					
31					HYDRAULIC CONDUCTIVITY (K) =
32					
33					
34					Regression Output:
35					Constant
36					Std Err of Y Est
37					R Squared
38					No. of Observations
39					Degrees of Freedom
40					
41					1 Coefficient:
42					Std Err of Coef.
43					

RATE OF RECOVERY TEST: WELL P101C

FALL



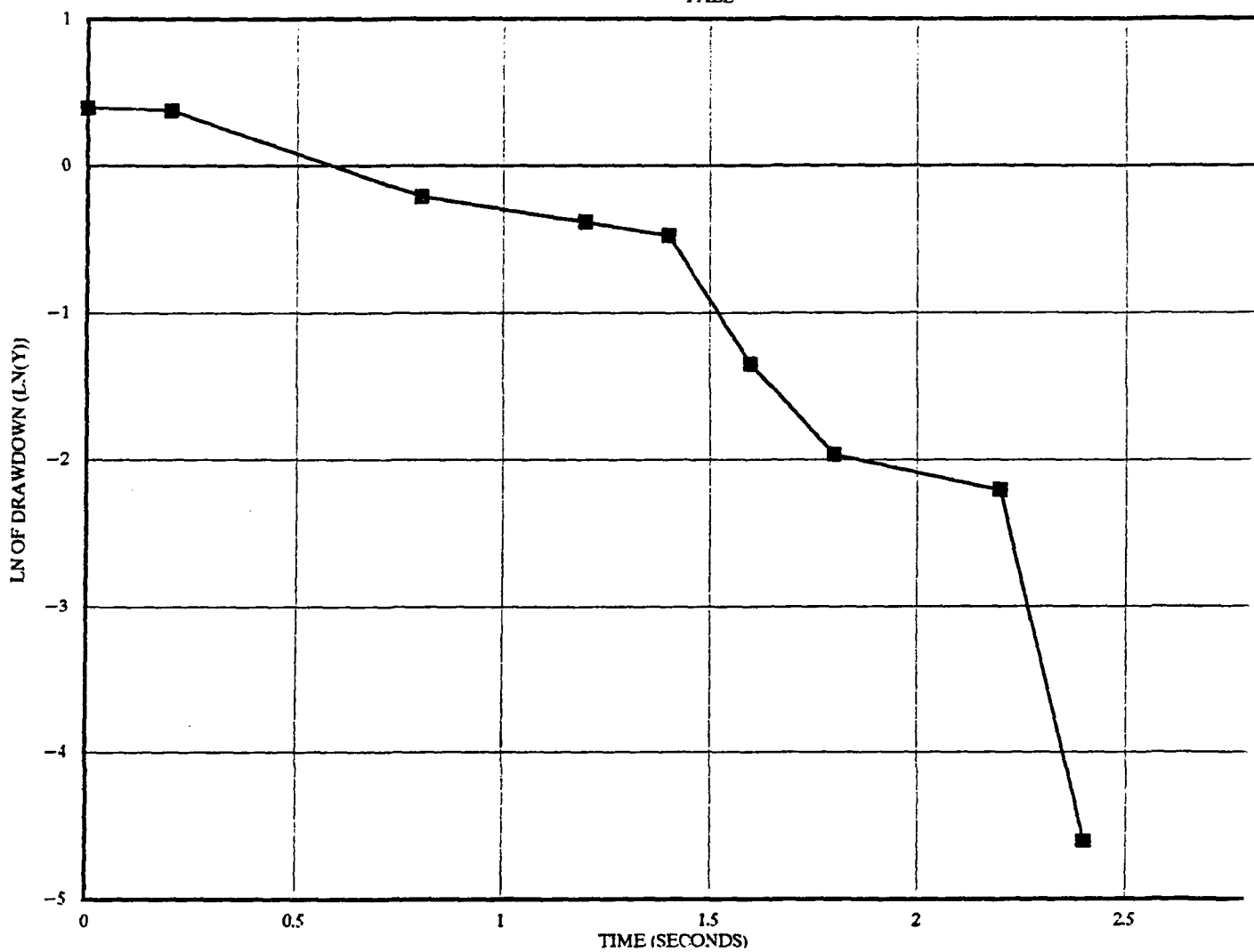
BOUMER AND RICE METHOD FOR INTERPRETATION OF SLUG TESTS: FOR UNCONFINED AND LEAKY CONFINED AQUIFERS.
 TO UTILIZE THIS WORKSHEET, ENTER YOUR DATA AT LOCATIONS MARKED BY AN "X".
 PROGRAM CAN INCLUDE EFFECTS OF SANDPACK DEWATERING (ASSUMING WATER IS RISING WITHIN THE SANDPACK).

TIME min	DEPTH TO DRAWDOWN	TIME sec	LN	PROJECT NAME	PROJECT NO	WELL NO	ANALYST	DATE COLLECTED	RISE PIPE (ID)	(2 r sub c)	(2 r sub c)	EFFECTIVE SCREEN DIAMETER (2 r sub w)	EFFECTIVE SCREEN LENGTH (L)	MAX DRAWDOWN (IN SUESET)	(Ymax)	STATIC WATER LEVEL (SNL)	DEPTH FROM SNL TO EFF. SCREEN BOTTOM (H)	AQUIFER DEPTH (SNL TO AQUIFER BOTTOM) (D)	INCLUDE SANDPACK DEWATERING (ENTER 1 IF YES, 0 IF NO)?	SANDPACK'S SPECIFIC YIELD (Sv)
11.25	1.490	0.00	0.3988	HIMCO	20026.024	F102F FALL	PUCHALSKI	04-Jan-91												
11.22	1.460	0.20	0.3784																	
10.57	0.810	0.80	-0.2107						12 r sub c	2.0 in.	0.0833 (radius in ft.)									
10.44	0.680	1.20	-0.3857							8.0 in.	0.3333 (radius in ft.)									
10.38	0.620	1.40	-0.4786									9.00 Ft.								
10.02	0.260	1.60	-1.3471										2.46 Ft.							
9.90	0.140	1.80	-1.9661											5.76 Ft.						
9.87	0.110	2.20	-2.2073													58.46 Ft.				
9.77	0.010	2.40	-4.6052														175.00 Ft.			
																		0		
																			0.10	
BOUMER AND RICE CURVE COEFFICIENTS:																				
RATIO OF L/(r sub w) =										27.00										
---LOG OF L/(r sub w) =										1.4314										
FOR PARTIALLY PENETRATING WELLS--																				
A =										2.33										
B =										0.32										
FOR FULLY PENETRATING WELLS--																				
C =										1.74										
---EVALUATION OF LN(Re/(r sub w)):																				
CONST.1 =										0.2129										
CONST.2 =										5.8568 *(MAX. OF 6.0) = 5.8568										
LN(Re/(r sub w)) =										2.71										
EFFECTIVE r sub c (for sandpack dewatering) =										0.0833										
(1/T)/(LN(Yo/Yt)) (SLOPE) =										-1.23E+00 sec ⁻¹										
HYDRAULIC CONDUCTIVITY (K) =																				
1.28E-03 ft/sec										3.91E-02 cm/sec										
Regression Output:																				
Constant										6.85E-01										
Std Err of Y Est										0.3651										
R Squared										0.8865										
No. of Observations										8										
Degrees of Freedom										6										
X Coefficient(s)										-1.23E+00										
Std Err of Coef.										0.1795										

t=0-2.25

RATE OF RECOVERY TEST: WELL P102B

FALL

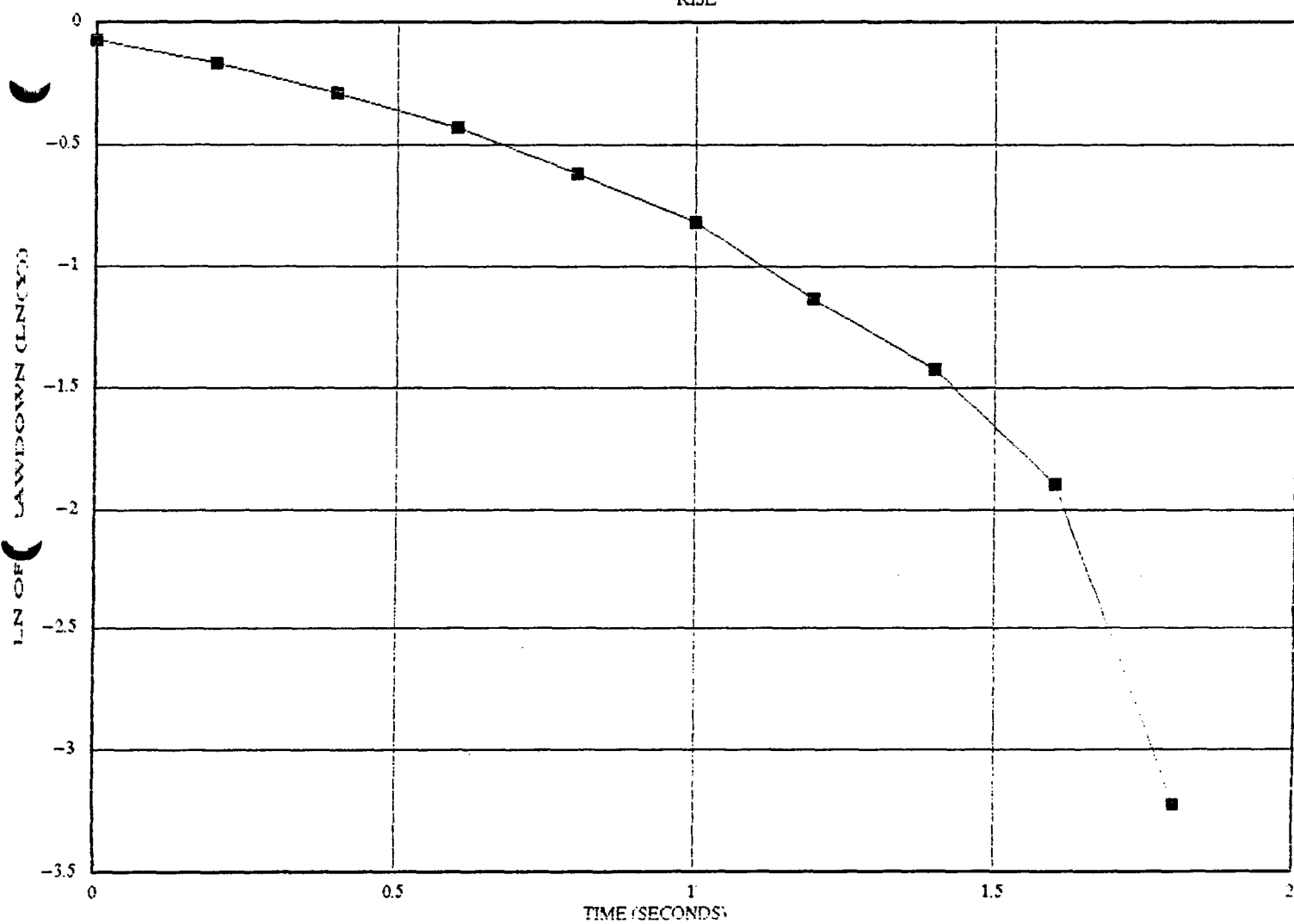


BOUWER AND RICE METHOD FOR INTERPRETATION OF SLUG TESTS: FOR UNCONFINED AND LEAKY CONFINED AQUIFERS.
 TO UTILIZE THIS WORKSHEET, ENTER YOUR DATA AT LOCATIONS MARKED BY AN "X".
 PROGRAM CAN INCLUDE EFFECTS OF SANDPACK DEWATERING (ASSUMING WATER IS RISING WITHIN THE SANDPACK).

TIME	WATER FL.	DEPTH TO	DRANDOWN	TIME sec	LN	PROJECT NAME	SHMCO
(H)	(Y)	(X')	(Y)	(X')	(Y)	PROJECT NO	20026.024
1	6.83	0.430	0.00	-0.0726		WELL NO	1F002 RISE
2	6.91	0.850	0.20	-0.1625		DATE COLLECTED	04-Jan-91
3	9.01	0.750	0.40	-0.2677		RISE PIPE (ID):	(2 r sub c) = 2.0 in. = 0.0833 (radius in ft.)
4	9.11	0.650	0.60	-0.4306		EFFECTIVE SCREEN DIAMETER: (2 r sub w) =	5.0 in. = 0.3333 (radius in ft.)
5	9.22	0.540	0.80	-0.6162		EFFECTIVE SCREEN LENGTH: (L) =	9.00 Ft.
6	9.32	0.440	1.00	-0.8210		MAX DRAWDOWN (IN SUBSET): (Ymax) =	2.46 Ft.
7	9.44	0.320	1.20	-1.1394		STATIC WATER LEVEL: (SML) =	9.76 Ft.
8	9.52	0.240	1.40	-1.4271		DEPTH FROM SML TO EFF. SCREEN BOTTOM: (H) =	58.46 Ft.
9	9.61	0.150	1.60	-1.8973		TEST AQUIFER DEPTH (SML TO AQUIFER BOTTOM): (D) =	175.00 Ft.
10	9.72	0.040	1.80	-3.2189		INCLUDE SANDPACK DEWATERING (ENTER 1 IF YES, 0 IF NO)?	0
11						SANDPACK'S SPECIFIC YIELD (Sv) =	0.10
12							
13						BOUWER AND RICE CURVE COEFFICIENTS:	
14						RATIO OF L/(r sub w) =	27.00
15						---LOS OF L/(r sub w) =	1.4314
16						FOR PARTIALLY PENETRATING WELLS--	
17						A =	2.33
18						B =	0.32
19						FOR FULLY PENETRATING WELLS--	
20						C =	1.74
21							
22						---EVALUATION OF LN(Re/(r sub w)):	
23						CONST.1 =	0.2129
24						CONST.2 =	5.8566 = (MAX. OF 6.0) = 5.8568
25						LN(Re/(r sub w)) =	2.71
26							
27						EFFECTIVE r sub c (for sandpack dewatering) =	0.0833
28						(1/T)/(LN(Yo/Yt)) (SLOPE) =	-1.10E+00 sec ⁻¹ (-1)
29							
30						HYDRAULIC CONDUCTIVITY (K) =	1.15E-03 ft/sec (*****)
31							3.50E-02 cm/sec (*****)
32							
33						Regression Outputs:	t = 0 -1.65
34						Constant	1.17E-01
35						Std Err of Y Est	0.1537
36						R Squares	0.9447
37						No. of Observations	9
38						Degrees of Freedom	7
39							
40						I Coefficient(s)	-1.16E+00
41						Std Err of Coef.	0.1005
42							
43							

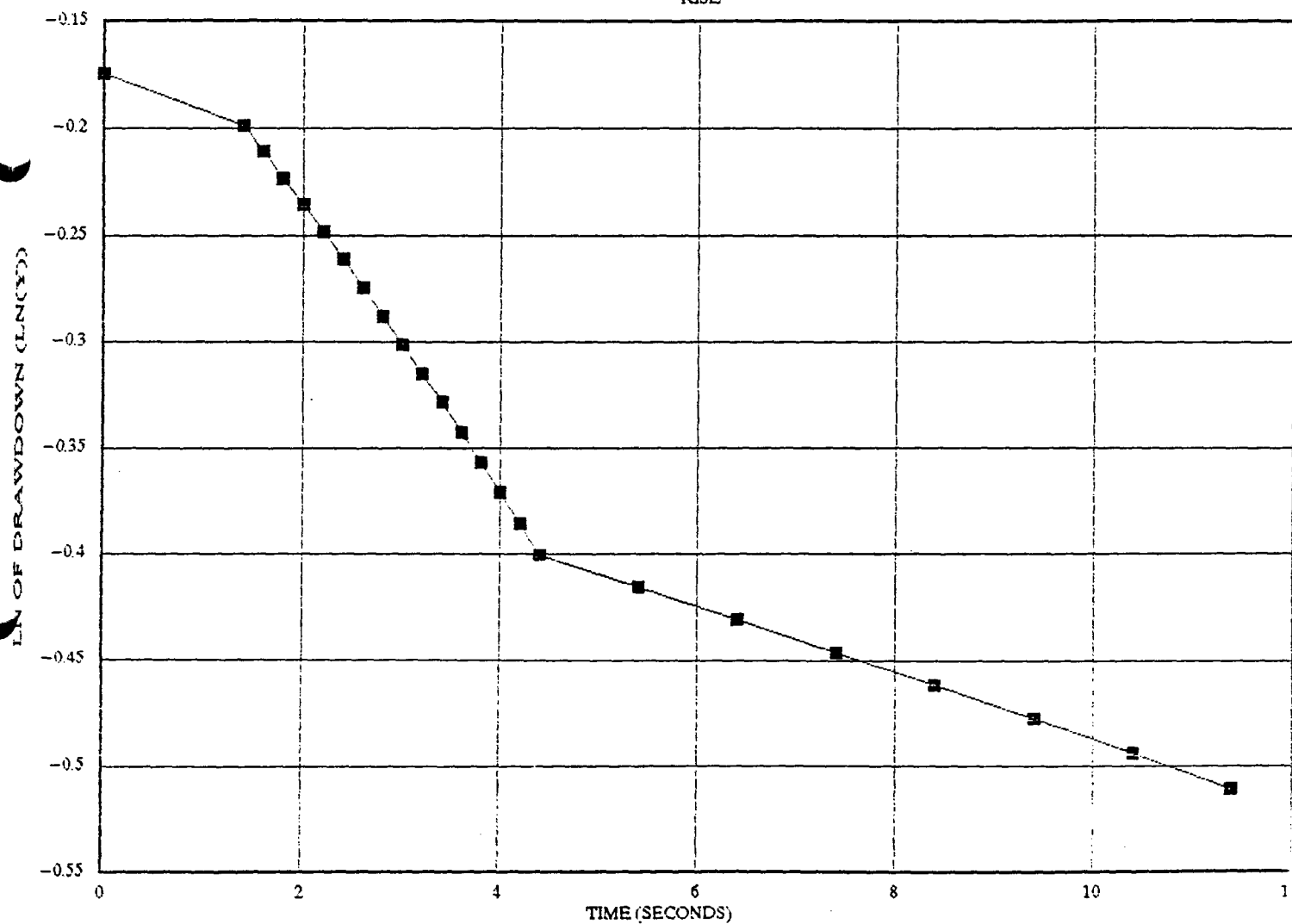
RATE OF RECOVERY TEST: WELL P102B

RISE



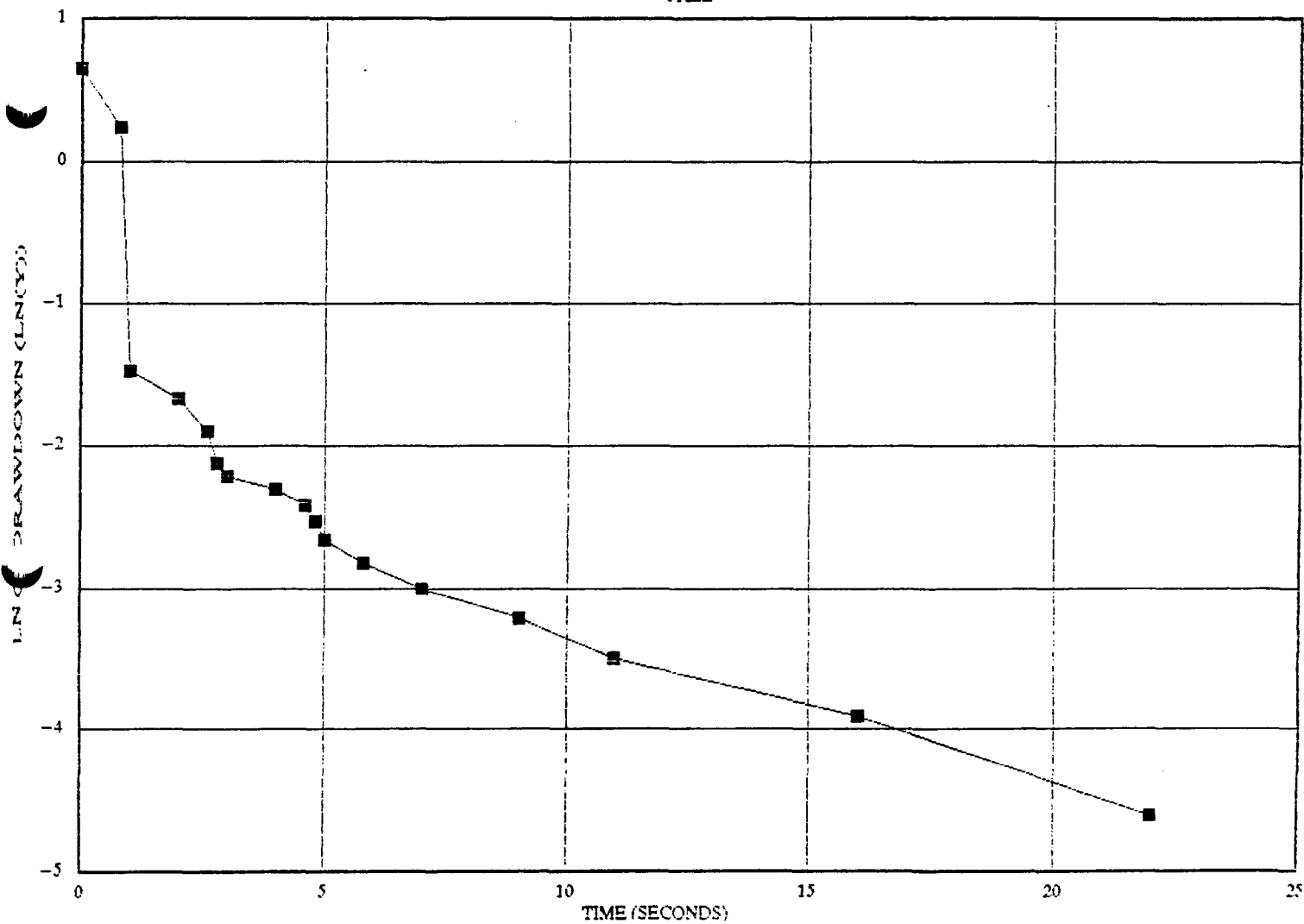
RATE OF RECOVERY TEST: WELL P102C

RISE



TIME min	DEPTH TO DRAINDOWN	TIME sec	LN	PROJECT NAME	PROJECT NO
(1)	(2)	(3)	(4)	(5)	(6)
1	6.95	1.530	0.00	WELL NO	W7-1014 FALL
2	8.30	1.280	0.80	ANALYST	SELINS
3	7.25	0.230	1.00	DATE COLLECTED	11-1-90
4	7.21	0.190	2.00	WISER PIPE (ID):	(2 r sub c) = 2.0 in. = 0.0833 (radius in ft.)
5	7.17	0.150	2.60	EFFECTIVE SCREEN DIAMETER:(2 r sub w) =	6.6 in. = 0.3333 (radius in ft.)
6	7.14	0.120	2.80	EFFECTIVE SCREEN LENGTH: (L) =	7.44 Ft.
7	7.13	0.110	3.00	MAX DRAINDOWN (IN SUBSET): (Ymax) =	-1.90 Ft.
8	7.12	0.100	4.00	STATIC WATER LEVEL: (SNL) =	7.02 Ft.
9	7.11	0.090	4.60	DEPTH FROM SNL TO EFF. SCREEN BOTTOM: (H) =	8.64 Ft.
10	7.10	0.080	4.80	TEST. AQUIFER DEPTH (SNL TO AQUIFER BOTTOM): (D) =	175.00 Ft.
11	7.09	0.070	5.00	INCLUDE SANDPACK DEWATERING (ENTER 1 IF YES, 0 IF NO)?	1
12	7.08	0.060	5.60	SANDPACK'S SPECIFIC YIELD (Sy) =	0.10
13	7.07	0.050	7.00	BOUNDARY AND RISE CURVE COEFFICIENTS:	
14	7.06	0.040	9.00	RATIO OF L/(r sub w) =	22.32
15	7.05	0.030	11.00	---LOG OF L/(r sub w) =	1.3467
16	7.04	0.020	16.00	FOR PARTIALLY PENETRATING WELLS--	
17	7.03	0.010	22.00	A =	2.17
18				B =	0.31
19				FOR FULLY PENETRATING WELLS--	
20				C =	1.59
21	7.020			---EVALUATION OF LN(Re/r sub w):	
22	7.020			CONST.1 =	0.3379
23				CONST.2 =	6.2128
24				LN(Re/r sub w) =	1.93
25					
26				EFFECTIVE r sub c (for sandpack dewatering) =	0.1318
27				(1/T)(LN(Yo/Yt)) (SLDPE) =	-1.38E-01 sec ⁻¹ -1
28					
29				HYDRAULIC CONDUCTIVITY (K) =	3.10E-04 ft/sec
30					9.45E-03 cm/sec
31					
32					
33				Regression Output:	
34				Constant	-1.80E+00
35				Std Err of Y Est	0.2057
36				R Squared	0.9411
37				No. of Observations	14
38				Degrees of Freedom	12
39					
40				X Coefficient(s)	-1.38E-01
41				Std Err of Coef.	0.0099
42					
43					

RATE OF RECOVERY TEST: WELL WT-101-A
FALL



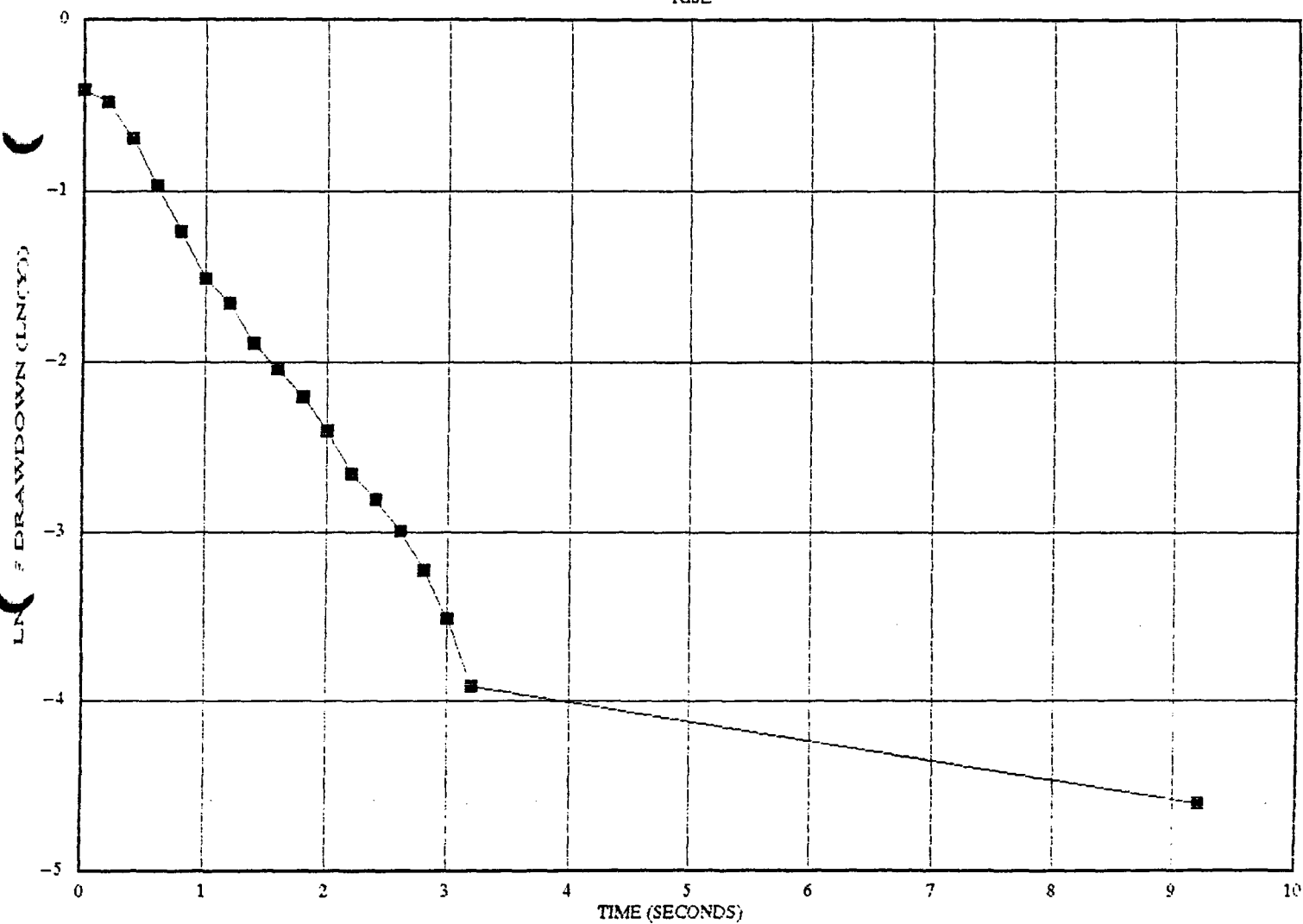
PROGRAM CAN INCLUDE EFFECTS OF SANDPACK DEWATERING (INDICATING WATER IS RISING WITHIN THE SANDPACK).

TIME min	DEPTH TO WATER ft.	DRAWDOWN (Y)	TIME sec	LN (X')	PROJECT NAME	INWCO
(X)	(Y)	(Y)	(X')	(Y)	PROJECT NO	20026.024
1	6.35	0.670	0.00	-0.4005	WELL NO	WT-101A RISE
2	6.40	0.620	0.20	-0.4780	ANALYST	ELIAS
3	6.52	0.500	0.40	-0.6931	DATE COLLECTED	12-1-96
4	6.64	0.380	0.60	-0.9676	RISE PIPE (ID):	(2 r sub c) = 2.0 in. = 0.0833 (radius in ft.)
5	6.73	0.290	0.80	-1.2379	EFFECTIVE SCREEN DIAMETER:	(2 r sub w) = 8.0 in. = 0.3333 (radius in ft.)
6	6.80	0.220	1.00	-1.5141	EFFECTIVE SCREEN LENGTH:	(L) = 7.44 Ft.
7	6.83	0.190	1.20	-1.6607	MAX DRAWDOWN (IN SUBSET):	(Ymax) = 0.67 Ft.
8	6.87	0.150	1.40	-1.8971	STATIC WATER LEVEL:	(SWL) = 7.02 Ft.
9	6.89	0.130	1.60	-2.0400	DEPTH FROM SWL TO EFF. SCREEN BOTTOM:	(H) = 6.64 Ft.
10	6.91	0.110	1.80	-2.2070	TEST. AQUIFER DEPTH (SWL TO AQUIFER BOTTOM):	(D) = 175.00 Ft.
11	6.92	0.090	2.00	-2.4075	INCLUDE SANDPACK DEWATERING (ENTER 1 IF YES, 0 IF NO)	0
12	6.95	0.070	2.20	-2.6575	SANDPACK'S SPECIFIC YIELD (SY) =	0.10
13	6.96	0.060	2.40	-2.8134	BOUMER AND RICE CURVE COEFFICIENTS:	
14	6.97	0.050	2.60	-2.9957	RATIO OF L/r sub w) =	20.32
15	6.98	0.040	2.80	-3.2189	---LOG OF L/r sub w) =	1.3487
16	6.99	0.030	3.00	-3.5066	FOR PARTIALLY PENETRATING WELLS--	
17	7.00	0.020	3.20	-3.9120	A =	2.17
18	7.01	0.010	3.40	-4.6052	B =	0.31
19	7.02	0.000	3.60	ERR	FOR FULLY PENETRATING WELLS--	
20					C =	1.59
21					---EVALUATION OF LN(Ho/r sub w):	
22					CONST.1 =	0.3379
23					CONST.2 =	6.2128 (MAX. OF 6.0) = 6.0000
24					LN(Ho/r sub w) =	1.93
25					EFFECTIVE r sub c (for sandpack dewatering) =	
26					(1/T)(LN(Yo/Yt)) (SLOPE) =	-9.77E-01 sec ⁻¹ (-1)
27					HYDRAULIC CONDUCTIVITY (K) =	
28					8.61E-04 ft/sec	<*****
29					2.69E-02 cm/sec	<*****
30					Regression Outputs:	
31					Constant	-4.94E-01
32					Std Err of Y Est	0.0425
33					R Squared	0.9961
34					No. of Observations	11
35					Degrees of Freedom	9
36					I Coefficient(s)	
37					Std Err of Coef.	-9.77E-01
38						0.0202
39						
40						
41						
42						
43						

t=1-35

RATE OF RECOVERY TEST: WELL WT-101-A

RISE



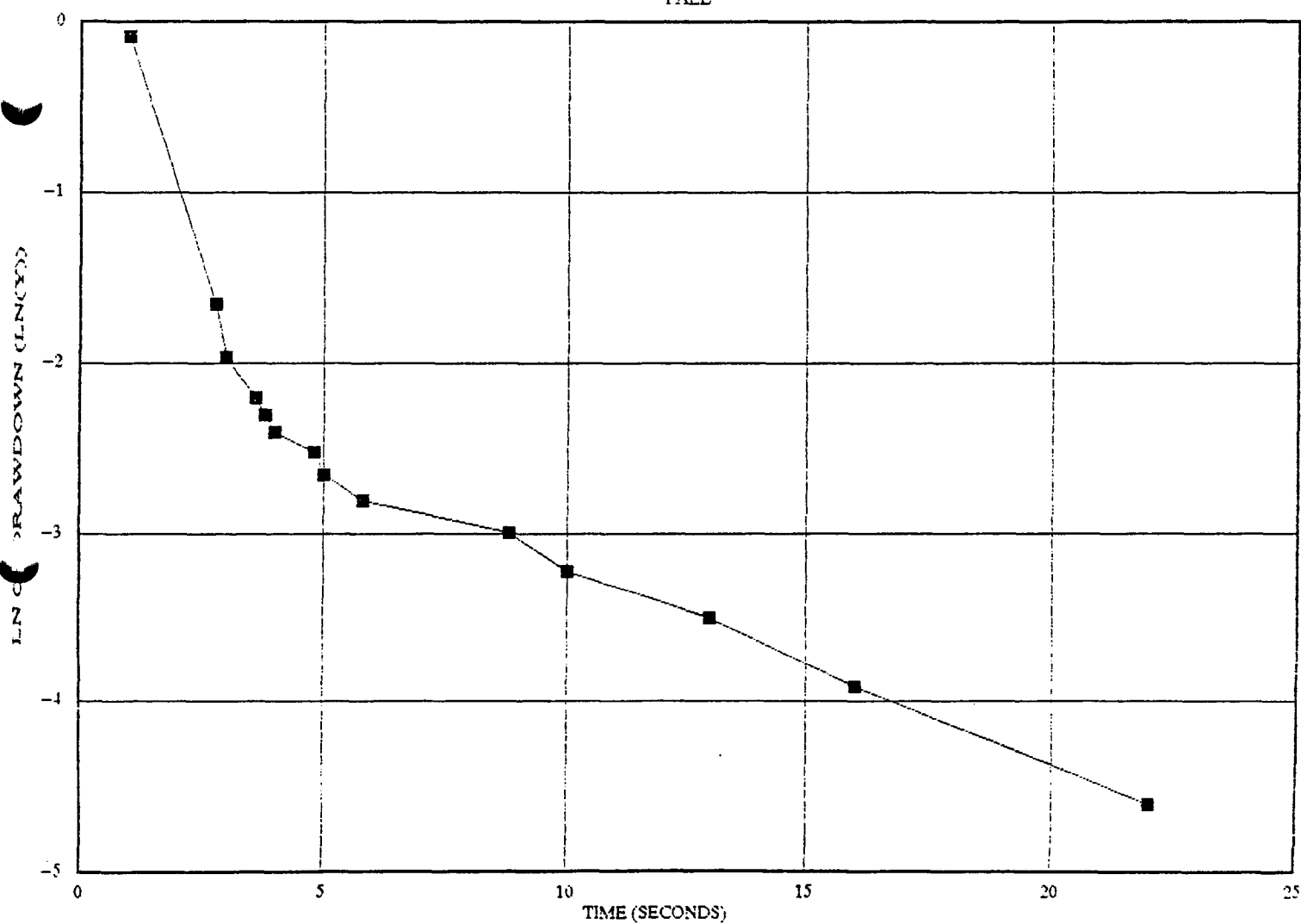
BOUMER AND RICE METHOD FOR INTERPRETATION OF SLUG TESTS: FOR UNCONFINED AND LEAKY CONFINED AQUIFERS.
 TO UTILIZE THIS WORKSHEET, ENTER YOUR DATA AT LOCATIONS MARKED BY AN "X".
 PROGRAM CAN INCLUDE EFFECTS OF SANDPACK DEWATERING (ASSUMING WATER IS RISING WITHIN THE SANDPACK).

TIME min	DEPTH TO: DRAWDOWN	TIME sec	LN	PROJECT NAME	PROJECT NO	WELL NO	ANALYST	DATE COLLECTED	WELL NO	ANALYST	DATE COLLECTED
(X)	(Y)	(X)	(Y)								
1	7.02	0.000	0.00	ERR	ANALYST	ELIHS					
2	7.14	0.920	1.00	-0.0524	DATE COLLECTED	12-1-90					
3	7.21	0.190	2.80	-1.6607	WISER PIPE (ID):	(2 r sub c) = 2.0 in. = 0.0833 (radius in ft.)					
4	7.16	0.140	3.00	-1.9661	EFFECTIVE SCREEN DIAMETER: (2 r sub w) =	8.0 in. = 0.3333 (radius in ft.)					
5	7.17	0.110	3.60	-2.2073	EFFECTIVE SCREEN LENGTH: (L)	= 10.29 Ft.					
6	7.12	0.190	3.80	-2.3026	MAX DRAWDOWN: (IN SUBSET) (max)	= -0.01 Ft.					
7	7.11	0.090	4.00	-2.4079	STATIC WATER LEVEL: (SAL)	= 7.02 Ft.					
8	7.10	0.080	4.80	-2.5287	DEPTH FROM SWL TO EFF. SCREEN BOTTOM: (H)	= 10.29 Ft.					
9	7.09	0.070	5.00	-2.6593	REST. AQUIFER DEPTH (SWL TO AQUIFER BOTTOM): (H)	= 175.00 Ft.					
10	7.09	0.060	5.80	-2.8134	INCLUDE SANDPACK DEWATERING (ENTER 1 IF YES, 0 IF NO):	1					
11	7.07	0.050	8.80	-2.9957	SANDPACK'S SPECIFIC YIELD (Sy)	= 0.10					
12	7.06	0.040	10.00	-3.2189							
13	7.05	0.030	13.00	-3.5066	BOUMER AND RICE CURVE COEFFICIENTS:						
14	7.04	0.020	16.00	-3.9120	RATIO OF L/(r sub w) =	30.87					
15	7.03	0.010	22.00	-4.6052	LOG OF L/(r sub w) =	1.4895					
16		7.020			FOR PARTIALLY PENETRATING WELLS--						
17		7.020			A =	2.47					
18		7.020			B =	0.34					
19		7.020			FOR FULLY PENETRATING WELLS--						
20		7.020			C =	1.86					
21		7.020									
22					---EVALUATION OF LNRe/(r sub w):						
23					CONST.1 =	0.3207					
24					CONST.2 =	6.2028 (MAX. OF 6.0) = 6.0000					
25					LNRe/(r sub w) =	2.14					
26											
27					EFFECTIVE r sub c (for sandpack dewatering) =	0.1318					
28					(1/T)/(LN(Yo/Yt)) (SLOPE) =	-1.23E-01 sec ⁻¹					
29											
30					HYDRAULIC CONDUCTIVITY (K) =	2.23E-04 ft/sec					
31						6.80E-05 cm/sec					
32											
33					Regression Output:						
34					Constant	-1.93E+00					
35					Std Err of Y Est	0.0966					
36					R Squared	0.9849					
37					No. of Observations	11					
38					Degrees of Freedom	9					
39											
40					X Coefficient(s)	-1.23E-01					
41					Std Err of Coef.	0.0051					
42											
43											

t = 3.6-22 s

RATE OF RECOVERY TEST: WELL WT-102-A

FALL



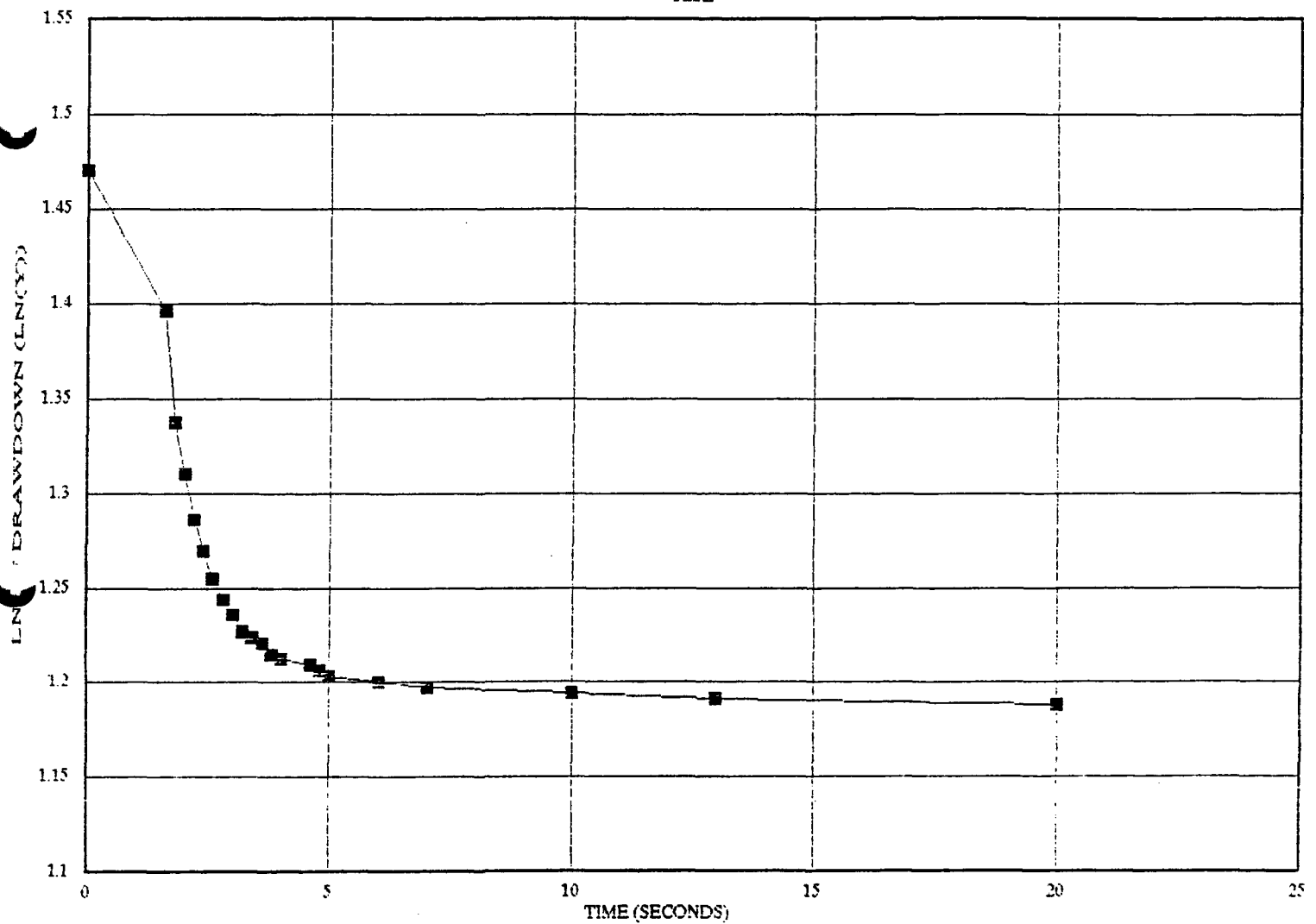
BOUNER AND RICE METHOD FOR INTERPRETATION OF SLUG TESTS: FOR UNCONFINED AND LEAKY CONFINED AQUIFERS.
 TO UTILIZE THIS WORKSHEET, ENTER YOUR DATA AT LOCATIONS MARKED BY AN "X".
 PROGRAM CAN INCLUDE EFFECTS OF SANDPACK DEWATERING (RESUMING WATER IS RISING WITHIN THE SANDPACK).

TIME min	DEPTH TO WATER Ft.	DEPTH TO DRAINAGE (Y)	TIME sec	LN	PROJECT NAME	HIMCO
(X)	(X)	(Y)	(X)	(Y)	PROJECT NO	20026.024
1	5.94	4.350	0.00	1.4702	WELL NO	INT-100P RISE
2	6.25	4.040	1.80	1.7962	ANALYST	ELIAS
3	6.42	3.510	1.80	1.2376	DATE COLLECTED	11-14-90
4	6.55	3.710	2.00	1.3110	RISE RISE (IS)	(2 r sub c) = 2.0 in. = 0.0625 (radius in ft.)
5	6.67	3.620	2.20	1.2865	EFFECTIVE SCREEN DIAMETER (2 r sub w) =	8.0 in. = 0.3333 (radius in ft.)
6	6.73	3.560	2.40	1.2696	EFFECTIVE SCREEN LENGTH: (L) =	11.09 ft.
7	6.78	3.510	2.60	1.2556	MAX DRAINAGE (IN SUBSET): (Ymax) =	4.04 ft.
8	6.82	3.470	2.80	1.2442	STATIC WATER LEVEL: (SNL) =	10.29 ft.
9	6.85	3.440	3.00	1.2355	DEPTH FROM SNL TO EFF. SCREEN BOTTOM: (W) =	9.53 ft.
10	6.88	3.410	3.20	1.2267	EST. AQUIFER DEPTH (SNL TO AQUIFER BOTTOM): (D) =	12.33 ft.
11	6.89	3.400	3.40	1.2238	INCLUDE SANDPACK DEWATERING (ENTER 1 IF YES, 0 IF NO)?	1
12	6.90	3.390	3.60	1.2208	SANDPACK'S SPECIFIC YIELD (Sy) =	0.10
13	6.92	3.376	3.80	1.2149	BOUNER AND RICE CURVE COEFFICIENTS:	
14	6.93	3.360	4.00	1.2119	RATIO OF L/(r sub w) =	33.27
15	6.94	3.350	4.20	1.2090	LOG OF L/(r sub w) =	1.5221
16	6.95	3.340	4.40	1.2060	FOR PARTIALLY PENETRATING WELLS--	
17	6.96	3.330	4.60	1.2030	A =	2.35
18	6.97	3.320	4.80	1.2000	B =	0.35
19	6.98	3.310	5.00	1.1969	FOR FULLY PENETRATING WELLS--	
20	6.99	3.300	5.20	1.1939	C =	1.97
21	7.00	3.290	5.40	1.1909	---EVALUATION OF LN(re/r sub w):	
22	7.01	3.280	5.60	1.1878	CONST.1 =	0.3281
23					CONST.2 =	2.1282 (MAX. OF 6.0) = 2.1282
24					LN(re/r sub w) =	2.34
25					EFFECTIVE r sub c (for sandpack dewatering) = 0.1318	
26					(1/T)(LN(Yo/Yt)) (SLOPE) = -7.41E-02 sec ⁻¹ (-1)	
27					HYDRAULIC CONDUCTIVITY (K) = 1.36E-04 ft/sec	
28					4.14E-03 cm/sec	
29					Regression Output:	
30					Constant	1.45E+00
31					Std Err of Y Est	0.0056
32					R Squared	0.9686
33					No. of Observations	6
34					Degrees of Freedom	4
35					X Coefficient(s)	-7.41E-02
36					Std Err of Coef.	0.0067

t = 2-45

RATE OF RECOVERY TEST: WELL WT-102A

RISE



BOUMER AND RICE METHOD FOR INTERPRETATION OF SLUG TESTS: FOR UNCONFINED AND LEAKY CONFINED AQUIFERS.
 TO UTILIZE THIS WORKSHEET, ENTER YOUR DATA AT LOCATIONS MARKED BY AN "X".
 PROGRAM CAN INCLUDE EFFECTS OF SANDPACK DEWATERING (ASSUMING WATER IS RISING WITHIN THE SANDPACK).

TIME min	DEPTH TO: WATER Ft.	DEPTH TO: DRAWDOWN (Y)	TIME sec	LN	PROJECT NAME	PROJECT NO	WELL NO	ANALYST	DATE COLLECTED	WELLER PIPE ID	EFFECTIVE SCREEN DIAMETER	EFFECTIVE SCREEN LENGTH	MAX DRAWDOWN (IN SUBSET)	STATIC WATER LEVEL	DEPTH FROM SML TO EFF. SCREEN BOTTOM	TEST. AQUIFER DEPTH (SML TO AQUIFER BOTTOM)	INCLUDE SANDPACK DEWATERING (ENTER 1 IF YES, 0 IF NO)	SANDPACK'S SPECIFIC YIELD (SY)
1	7.95	0.000	0.00	ERR	20026.024	20026.024	INT-103A FALL	ELIAS	12-14-90									
2	8.30	0.320	0.20	-1.1394														
3	8.26	0.280	0.60	-1.2730														
4	8.21	0.230	0.80	-1.4697														
5	8.18	0.200	1.00	-1.6094														
6	8.15	0.170	1.20	-1.7720														
7	8.07	0.090	1.40	-2.4075														
8	8.06	0.080	1.60	-2.3257														
9	8.03	0.050	1.80	-2.8957														
10	8.00	0.020	2.00	-3.9120														
11	7.98	0.000	2.20	ERR														
12																		
13																		
14																		
15																		
16																		
17																		
18																		
19																		
20																		
21																		
22																		
23																		
24																		
25																		
26																		
27																		
28																		
29																		
30																		
31																		
32																		
33																		
34																		
35																		
36																		
37																		
38																		
39																		
40																		
41																		
42																		
43																		

BOUMER AND RICE CURVE COEFFICIENTS:

RATIO OF $L/(r \text{ sub } w)$ = 19.38

---LOG OF $L/(r \text{ sub } w)$ = 1.2874

FOR PARTIALLY PENETRATING WELLS--

A = 2.07

B = 0.30

FOR FULLY PENETRATING WELLS--

C = 1.50

---EVALUATION OF $LN(Re/(r \text{ sub } w))$:

CONST.1 = 0.3711

CONST.2 = 2.8685

$LN(Re/(r \text{ sub } w))$ = 1.92

EFFECTIVE $r \text{ sub } w$ (for sandpack dewatering) = 0.0833

$(1/7)(LN(Yo/Yt))$ (SLOPE) = -5.92E-01 sec^{-1}

HYDRAULIC CONDUCTIVITY (K) = 6.10E-04 ft/sec

1.66E-02 cm/sec

Regression Output:

Constant = -9.88E-01

Std Err of Y Est = 0.0590

R Squared = 0.9464

No. of Observations = 4

Degrees of Freedom = 2

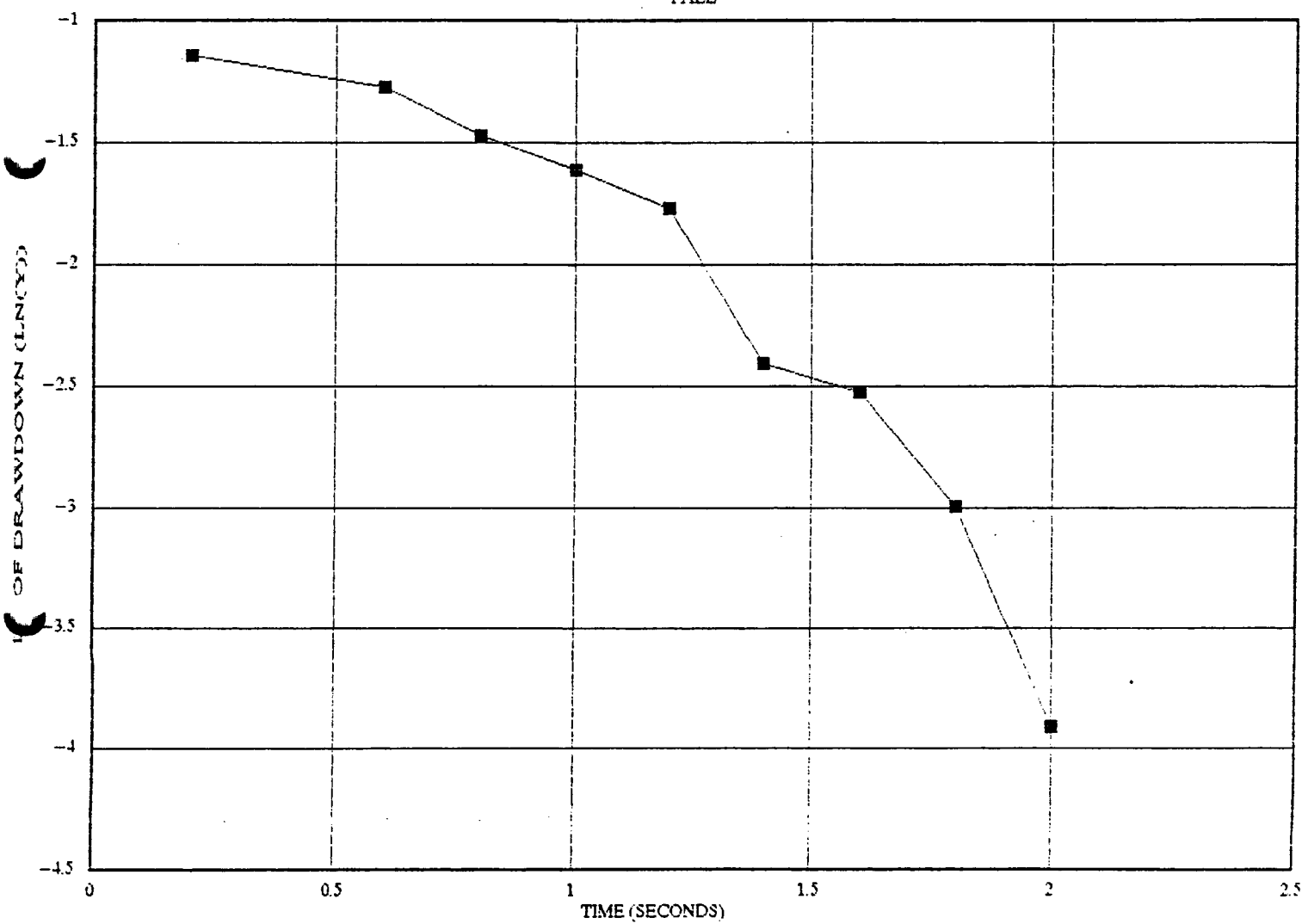
X Coefficient(s) = -5.92E-01

Std Err of Coef. = 0.0997

t=0.2-1s

RATE OF RECOVERY TEST: WELL WT-103A

FALL



FORMER AND RICE METHOD FOR INTERPRETATION OF SLUG TESTS, FOR UNCONFINED AND LEAKY CONFINED AQUIFERS.
 TO UTILIZE THIS WORKSHEET, ENTER YOUR DATA AT LOCATIONS MARKED BY AN "X".
 PROGRAM CAN INCLUDE EFFECTS OF SANDPACK DEWATERING, ASSUMING WATER IS RISING WITHIN THE SANDPACK.

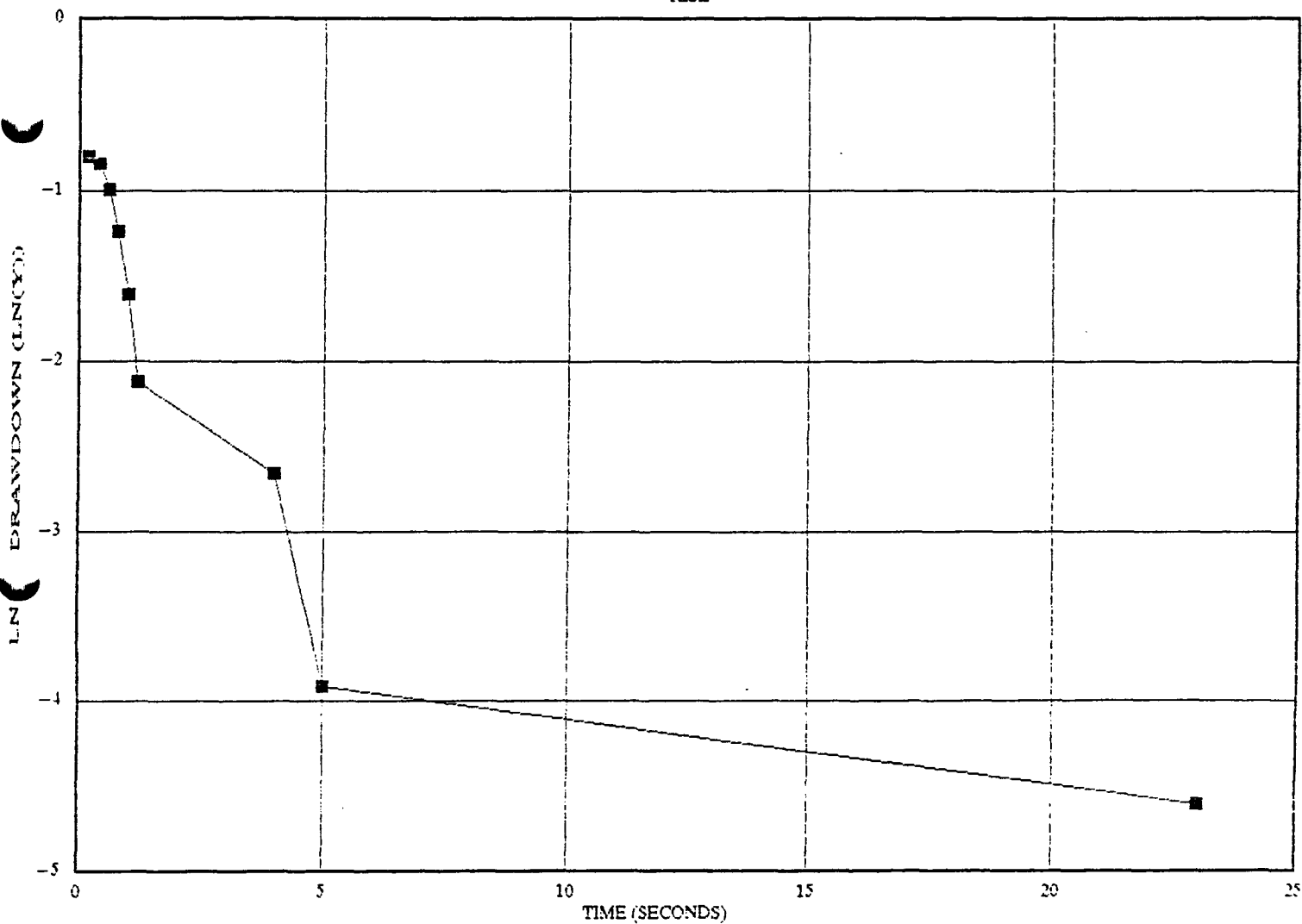
LINE	DATE	DEPTH TO WATER (ft.)	TIME SEC.	LN	PROJECT NAME	WELL NO.	DATE COLLECTED	WELL NO.	DATE
1		7.55	1.950	0.06	2.0765	2002b.024	December 14, 1990	19.38	0.0833 (radius in ft.)
2		7.55	0.450	0.20	-0.7925			1.2574	0.0833 (radius in ft.)
3		7.61	0.450	0.40	-0.9144				
4		7.65	0.270	0.60	-0.5145				
5		7.78	0.290	0.80	-1.1375				
6		7.85	0.200	1.00	-1.6095				
7		7.91	0.120	1.20	-2.1205				
8		7.96	0.070	4.00	-2.6593				
9		7.97	0.020	5.00	-2.9120				
10		7.98	0.010	23.00	-4.6052				
11									
12									
13									
14									
15									
16									
17									
18									
19									
20									
21									
22									
23									
24									
25									
26									
27									
28									
29									
30									
31									
32									
33									
34									
35									
36									
37									
38									
39									
40									
41									
42									
43									

FORMER AND RICE CURVE COEFFICIENTS:	
RATIO OF L/(r SUB W) =	19.38
LOG OF L/(r SUB W) =	1.2874
FOR PARTIALLY PENETRATING WELLS--	
A =	2.07
B =	0.30
C =	1.50
FOR FULLY PENETRATING WELLS--	
EVALUATION OF LN(RW/(r SUB W)):	
CONST. 1 =	0.3711
CONST. 2 =	2.8485
LN(RW/(r SUB W)) =	1.92
EFFECTIVE r SUB C (for sandpack dewatering) = 0.0833	
(1/17)(LN(RW/(r SUB W))) (SLOPE) = -1.31E+00 SEC ⁻¹	
HYDRAULIC CONDUCTIVITY (K) = 1.35E-03 ft/sec	
= 4.10E-02 cm/sec	
Regression Output:	
Constant	-3.53E-01
Std Err of Y Est	0.1756
R Squared	0.7065
No. of Observations	6
Degrees of Freedom	4
T Coefficients	-1.31E+00
Std Err of Coef.	0.2098

L = 2-1.25

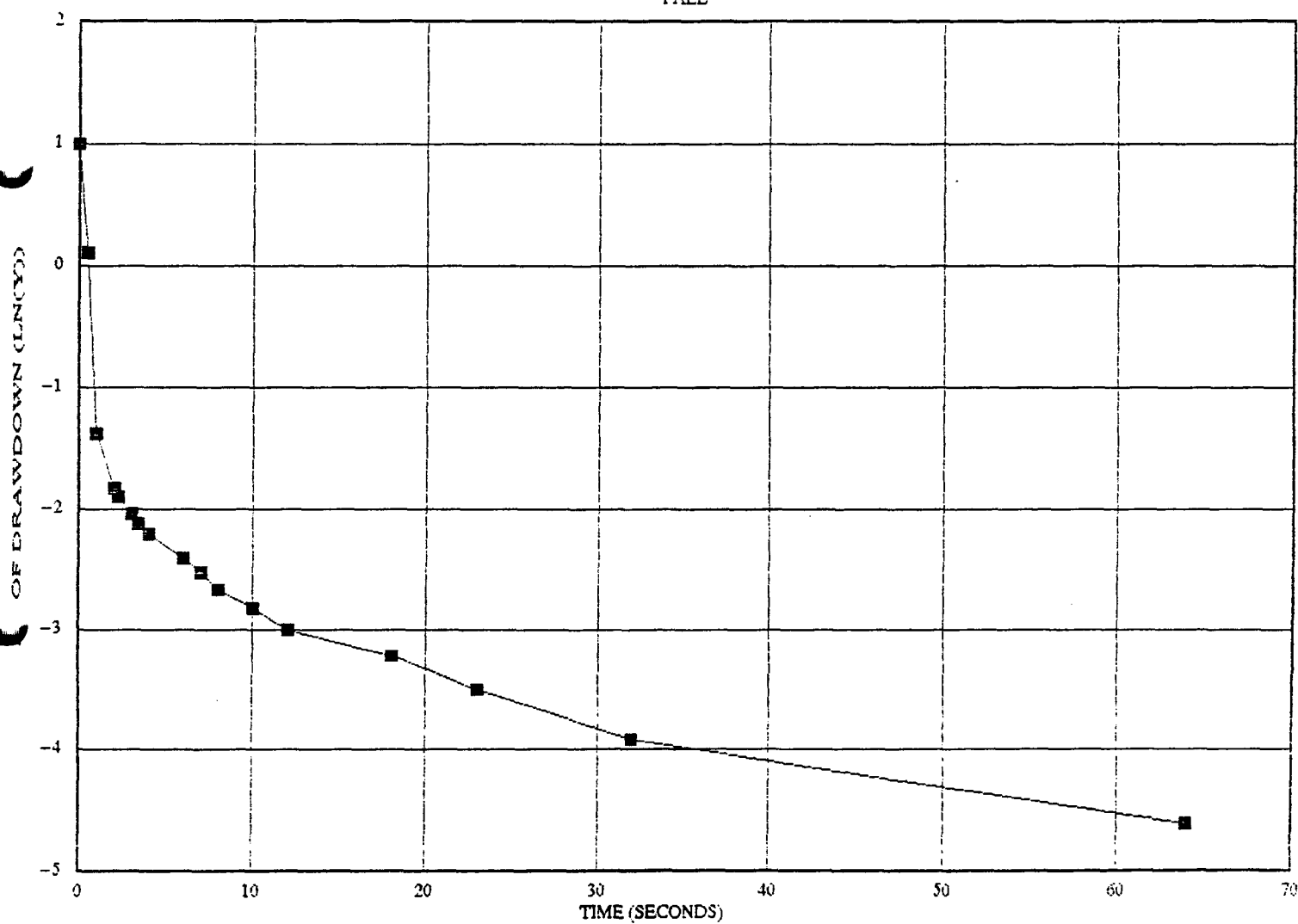
RATE OF RECOVERY TEST: WELL WT - 103A

RISE



RATE OF RECOVERY TEST: WELL WT-104A

FALL

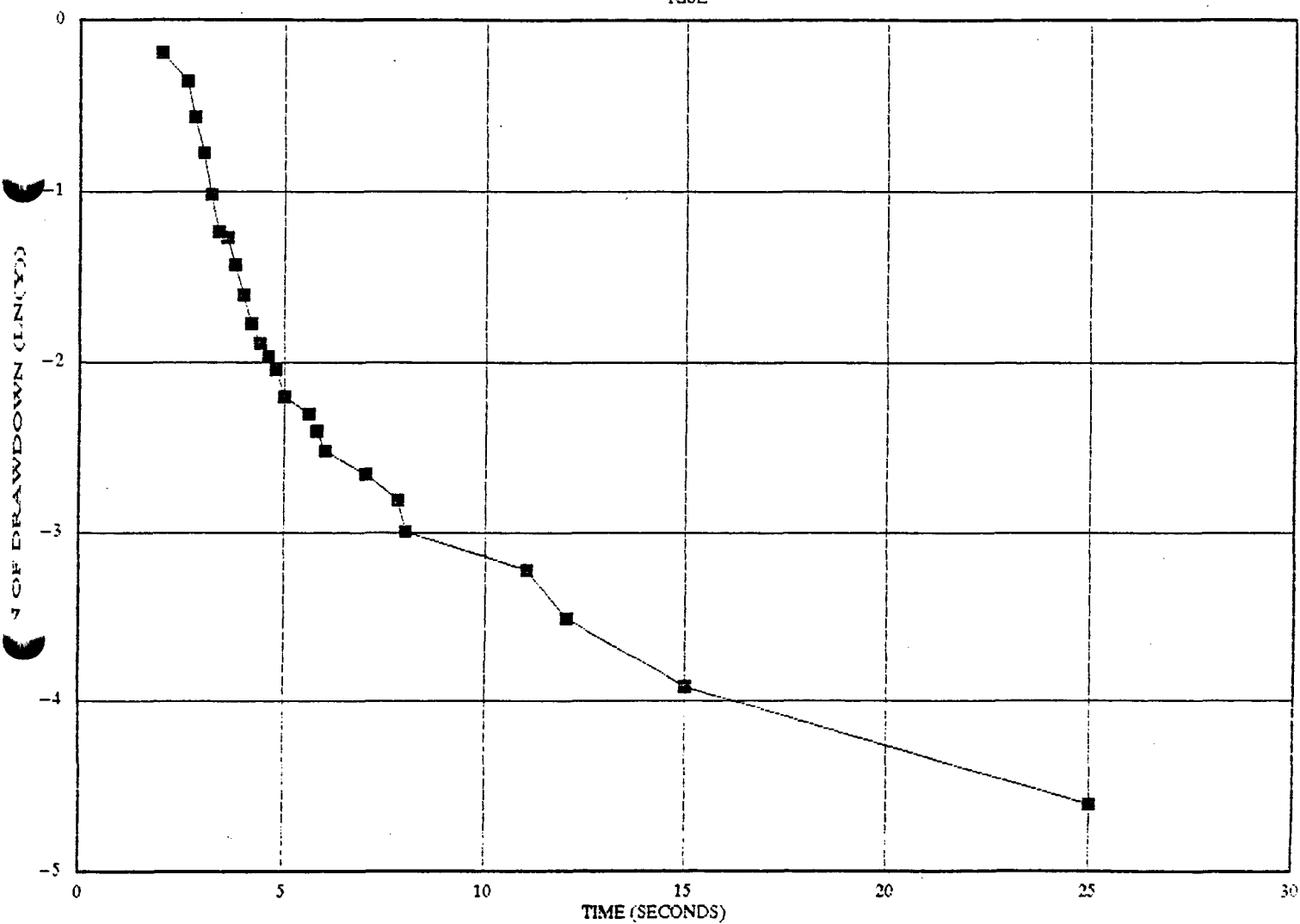


BOUWER AND RICE METHOD FOR INTERPRETATION OF SLUG TESTS: FOR UNCONFINED AND LEAKY CONFINED AQUIFERS.
 TO UTILIZE THIS WORKSHEET, ENTER YOUR DATA AT LOCATIONS MARKED BY AN "X".
 PROGRAM CAN INCLUDE EFFECTS OF SANDPACK DEWATERING (ASSUMING WATER IS RISING WITHIN THE SANDPACK).

TIME min	DEPTH TO: DRAWDOWN	TIME sec	LN	PROJECT NAME	WIMCO
(X)	(Y)	(X)	(Y)	PROJECT NO	20026.024
				WELL NO	WT-104A RISE
1	6.02	0.010	0.00	ANALYST	ELIAS
2	5.18	0.830	2.00	DATE COLLECTED	12-14-90
3	5.31	0.700	2.60	RISER PIPE (ID):	(2 r sub c) = 2.0 in. = 0.0833 (radius in ft.)
4	5.44	0.570	2.80	EFFECTIVE SCREEN DIAMETER:	(2 r sub w) = 8.0 in. = 0.3333 (radius in ft.)
5	5.55	0.460	3.00	EFFECTIVE SCREEN LENGTH: (L)	= 12.67 Ft.
6	5.65	0.360	3.20	MAX DRAWDOWN (IN SUBSET): (Ymax)	= 0.70 Ft.
7	5.72	0.290	3.40	STATIC WATER LEVEL: (SWL)	= 6.01 Ft.
8	5.73	0.280	3.60	DEPTH FROM SWL TO EFF. SCREEN BOTTOM: (H)	= 12.67 Ft.
9	5.77	0.240	3.80	TEST. AQUIFER DEPTH (SWL TO AQUIFER BOTTOM): (D)	= 175.00 Ft.
10	5.81	0.200	4.00	INCLUDE SANDPACK DEWATERING (ENTER 1 IF YES, 0 IF NO):	1
11	5.84	0.170	4.20	SANDPACK'S SPECIFIC YIELD (Sv)	= 0.10
12	5.86	0.150	4.40		
13	5.87	0.140	4.60	BOUWER AND RICE CURVE COEFFICIENTS:	
14	5.88	0.130	4.80	RATIO OF L/(r sub w) = 38.01	
15	5.90	0.110	5.00	---LOG OF L/(r sub w) = 1.5799	
16	5.91	0.100	5.60	FOR PARTIALLY PENETRATING WELLS--	
17	5.92	0.090	5.80	A = 2.71	
18	5.93	0.080	6.00	B = 0.37	
19	5.94	0.070	7.00	FOR FULLY PENETRATING WELLS--	
20	5.95	0.060	7.80	C = 2.16	
21	5.96	0.050	8.00	---EVALUATION OF LN(Re/(r sub w)):	
22	5.97	0.040	11.00	CONST.1 = 0.3024	
23	5.98	0.030	12.00	CONST.2 = 6.1882 = (MAX. OF 6.0) = 6.0000	
24	5.99	0.020	15.00	LN(Re/(r sub w)) = 2.31	
25	6.00	0.010	25.00		
26	6.01	0.000	39.00	ERR	
27				EFFECTIVE r sub c (for sandpack dewatering) = 0.1318	
28				(1/T)(LN(Yo/Yt)) (SLOPE) = -8.06E-01 sec ⁻¹	
29					
30				HYDRAULIC CONDUCTIVITY (K) = 1.28E-03 ft/sec	
31				3.89E-02 cm/sec	
32				t=2.6-4.65	
33				Regression Output:	
34				Constant 1.64E+00	
35				Std Err of Y Est 0.0748	
36				R Squared 0.9827	
37				No. of Observations 11	
38				Degrees of Freedom 9	
39					
40				1 Coefficient(s) -8.06E-01	
41				Std Err of Coef. 0.0356	
42					
43					

RATE OF RECOVERY TEST: WELL WT-104A

RISE



POWNER AND RICE METHOD FOR INTERPRETATION OF SLUG TESTS FOR UNCONFINED AND LEAKY CONFINED AQUIFERS.

TO UTILIZE THIS WORKSHEET, ENTER YOUR DATA AT LOCATIONS MARKED BY AN "X".

PROGRAM CAN INCLUDE EFFECTS OF SANDPACK DEWATERING (ASSUMING WATER IS RISING WITHIN THE SANDPACK).

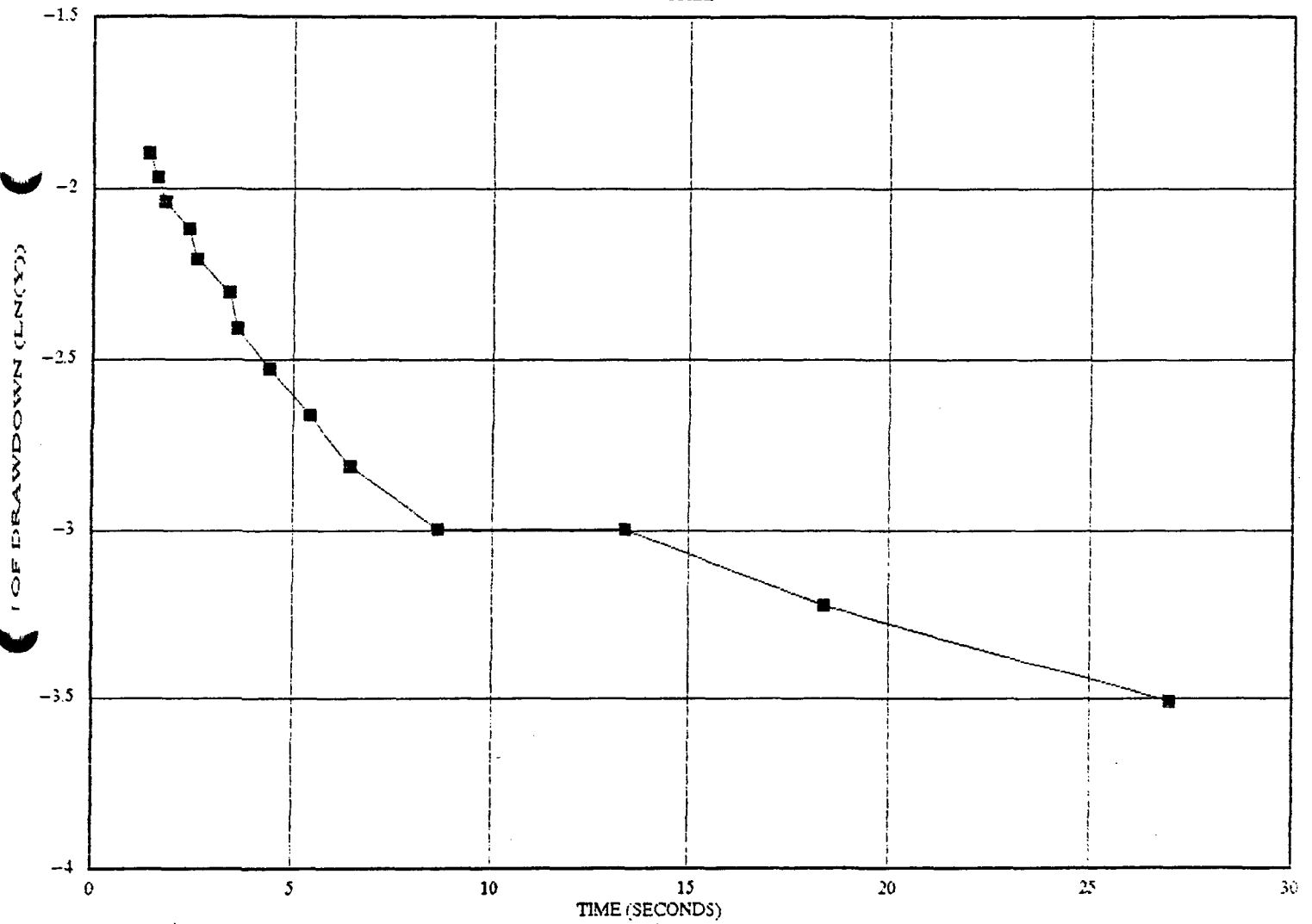
TIME min	DEPTH TO DRAWDOWN	TIME sec	LW	PROJECT NAME	WELL NO	ANALYST	DATE COLLECTED	WELL NO	ANALYST	DATE COLLECTED
1	9.56	1.980	0.00	0.6831	WELL NO	ANALYST	DATE COLLECTED	WELL NO	ANALYST	DATE COLLECTED
2	9.42	1.440	0.20	0.3646	WELL NO	ANALYST	DATE COLLECTED	WELL NO	ANALYST	DATE COLLECTED
3	8.13	0.150	1.40	1-1.8971	WELL NO	ANALYST	DATE COLLECTED	WELL NO	ANALYST	DATE COLLECTED
4	8.12	0.140	1.60	1-1.9681	WELL NO	ANALYST	DATE COLLECTED	WELL NO	ANALYST	DATE COLLECTED
5	8.11	0.130	1.80	1-2.0490	WELL NO	ANALYST	DATE COLLECTED	WELL NO	ANALYST	DATE COLLECTED
6	8.10	0.120	2.00	1-2.1299	WELL NO	ANALYST	DATE COLLECTED	WELL NO	ANALYST	DATE COLLECTED
7	8.09	0.110	2.20	1-2.2108	WELL NO	ANALYST	DATE COLLECTED	WELL NO	ANALYST	DATE COLLECTED
8	8.08	0.100	2.40	1-2.2917	WELL NO	ANALYST	DATE COLLECTED	WELL NO	ANALYST	DATE COLLECTED
9	8.07	0.090	2.60	1-2.3726	WELL NO	ANALYST	DATE COLLECTED	WELL NO	ANALYST	DATE COLLECTED
10	8.06	0.080	2.80	1-2.4535	WELL NO	ANALYST	DATE COLLECTED	WELL NO	ANALYST	DATE COLLECTED
11	8.05	0.070	3.00	1-2.5344	WELL NO	ANALYST	DATE COLLECTED	WELL NO	ANALYST	DATE COLLECTED
12	8.04	0.060	3.20	1-2.6153	WELL NO	ANALYST	DATE COLLECTED	WELL NO	ANALYST	DATE COLLECTED
13	8.03	0.050	3.40	1-2.6962	WELL NO	ANALYST	DATE COLLECTED	WELL NO	ANALYST	DATE COLLECTED
14	8.02	0.040	3.60	1-2.7771	WELL NO	ANALYST	DATE COLLECTED	WELL NO	ANALYST	DATE COLLECTED
15	8.01	0.030	3.80	1-2.8580	WELL NO	ANALYST	DATE COLLECTED	WELL NO	ANALYST	DATE COLLECTED
16	8.00	0.020	4.00	1-2.9389	WELL NO	ANALYST	DATE COLLECTED	WELL NO	ANALYST	DATE COLLECTED
17					WELL NO	ANALYST	DATE COLLECTED	WELL NO	ANALYST	DATE COLLECTED
18					WELL NO	ANALYST	DATE COLLECTED	WELL NO	ANALYST	DATE COLLECTED
19					WELL NO	ANALYST	DATE COLLECTED	WELL NO	ANALYST	DATE COLLECTED
20					WELL NO	ANALYST	DATE COLLECTED	WELL NO	ANALYST	DATE COLLECTED
21					WELL NO	ANALYST	DATE COLLECTED	WELL NO	ANALYST	DATE COLLECTED
22					WELL NO	ANALYST	DATE COLLECTED	WELL NO	ANALYST	DATE COLLECTED
23					WELL NO	ANALYST	DATE COLLECTED	WELL NO	ANALYST	DATE COLLECTED
24					WELL NO	ANALYST	DATE COLLECTED	WELL NO	ANALYST	DATE COLLECTED
25					WELL NO	ANALYST	DATE COLLECTED	WELL NO	ANALYST	DATE COLLECTED
26					WELL NO	ANALYST	DATE COLLECTED	WELL NO	ANALYST	DATE COLLECTED
27					WELL NO	ANALYST	DATE COLLECTED	WELL NO	ANALYST	DATE COLLECTED
28					WELL NO	ANALYST	DATE COLLECTED	WELL NO	ANALYST	DATE COLLECTED
29					WELL NO	ANALYST	DATE COLLECTED	WELL NO	ANALYST	DATE COLLECTED
30					WELL NO	ANALYST	DATE COLLECTED	WELL NO	ANALYST	DATE COLLECTED
31					WELL NO	ANALYST	DATE COLLECTED	WELL NO	ANALYST	DATE COLLECTED
32					WELL NO	ANALYST	DATE COLLECTED	WELL NO	ANALYST	DATE COLLECTED
33					WELL NO	ANALYST	DATE COLLECTED	WELL NO	ANALYST	DATE COLLECTED
34					WELL NO	ANALYST	DATE COLLECTED	WELL NO	ANALYST	DATE COLLECTED
35					WELL NO	ANALYST	DATE COLLECTED	WELL NO	ANALYST	DATE COLLECTED
36					WELL NO	ANALYST	DATE COLLECTED	WELL NO	ANALYST	DATE COLLECTED
37					WELL NO	ANALYST	DATE COLLECTED	WELL NO	ANALYST	DATE COLLECTED
38					WELL NO	ANALYST	DATE COLLECTED	WELL NO	ANALYST	DATE COLLECTED
39					WELL NO	ANALYST	DATE COLLECTED	WELL NO	ANALYST	DATE COLLECTED
40					WELL NO	ANALYST	DATE COLLECTED	WELL NO	ANALYST	DATE COLLECTED
41					WELL NO	ANALYST	DATE COLLECTED	WELL NO	ANALYST	DATE COLLECTED
42					WELL NO	ANALYST	DATE COLLECTED	WELL NO	ANALYST	DATE COLLECTED
43					WELL NO	ANALYST	DATE COLLECTED	WELL NO	ANALYST	DATE COLLECTED

EFFECTIVE r sub c (for sandpack dewatering) =		0.1318
(1/r) * (LN(Ye/Yi)) / (SLOPE) =		-1.81E-01 sec ⁻¹
HYDRAULIC CONDUCTIVITY (K) =		3.32E-04 ft/sec
		1.01E-02 cm/sec
Regression Output:		
Constant	-1.73E+00	
Std Err of Est	0.0257	
R Squared	0.9545	
Nc. of Observations	4	
Degrees of Freedom	2	
t Coefficients	-1.81E-01	
Std Err of Coef.	0.0279	

t = 2.6 - 4.4 s

RATE OF RECOVERY TEST: WELL WT-105A

FALL



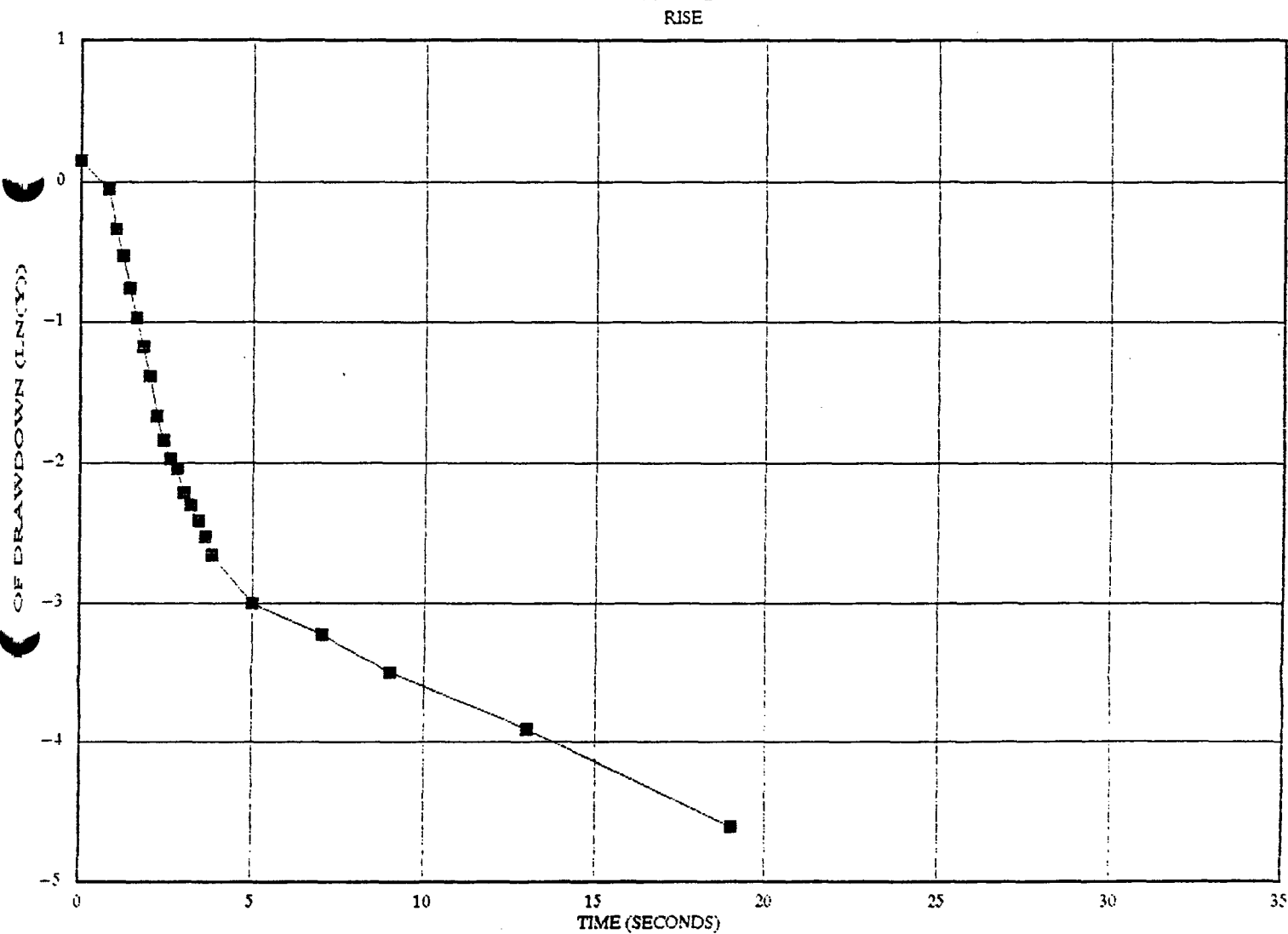
BOUNER AND RICE METHOD FOR INTERPRETATION OF SLUG TESTS FOR UNCONFINED AND LEAKY CONFINED AQUIFERS.
 TO UTILIZE THIS WORKSHEET, ENTER YOUR DATA AT LOCATIONS MARKED BY AN "X".
 PROGRAM CAN INCLUDE EFFECTS OF SANDPACK DEWATERING (ASSUMING WATER IS RISING WITHIN THE SANDPACK).

TIME min	DEPTH TO DRAWDOWN	TIME sec	LN	PROJECT NAME	PROJECT NO	ANALYST	DATE COLLECTED	WELL NO	WELL TYPE
(X)	(Y)	(X)	(Y)						
1	6.82	1.160	0.00	IMCO	20026.024	ELIAS	12-14-96	MT-105A	RISE
2	7.03	0.950	0.00						
3	7.26	0.720	1.00						
4	7.39	0.590	1.20						
5	7.51	0.470	1.40						
6	7.60	0.380	1.60						
7	7.67	0.310	1.80						
8	7.73	0.250	2.00						
9	7.79	0.190	2.20						
10	7.82	0.160	2.40						
11	7.84	0.140	2.60						
12	7.85	0.130	2.80						
13	7.87	0.110	3.00						
14	7.89	0.100	3.20						
15	7.89	0.090	3.40						
16	7.90	0.080	3.60						
17	7.91	0.070	3.80						
18	7.93	0.050	5.00						
19	7.94	0.040	7.00						
20	7.95	0.030	9.00						
21	7.96	0.020	13.00						
22	7.97	0.010	19.00						
23	7.98	0.000	32.00						
24									
25									
26									
27									
28									
29									
30									
31									
32									
33									
34									
35									
36									
37									
38									
39									
40									
41									
42									
43									

BOUNER AND RICE CURVE COEFFICIENTS:			
RATIO OF $L/(r \text{ sub } w)$	=	30.24	
---LOG OF $L/(r \text{ sub } w)$	=	1.4806	
FOR PARTIALLY PENETRATING WELLS--			
A =	2.45		
B =	0.34		
FOR FULLY PENETRATING WELLS--			
C =	1.86		
---EVALUATION OF $LN(Re/(r \text{ sub } w))$:			
CONST.1 =	0.3227		
CONST.2 =	6.2041	=(MAX. OF 6.0) =	6.0000
$LN(Re/(r \text{ sub } w))$	=	2.13	
EFFECTIVE $r \text{ sub } c$ (for sandpack dewatering) = 0.0633			
$(1/T)/(LN(Yo/Yt))$ (SLOPE) =	-8.62E-01	sec ⁻¹	(-1)
HYDRAULIC CONDUCTIVITY (K) = 6.32E-04 ft/sec			
1.93E-02 cm/sec			
Regression Output:			
Constant	4.33E-01		
Std Err of Y Est	0.1316		
R Squared	0.9766		
No. of Observations	16		
Degrees of Freedom	14		
T Coefficient(s)	-8.62E-01		
Std Err of Coef.	0.6257		

t = 2.2-3.8 s

RATE OF RECOVERY TEST: WELL WT-105A



BOWEN AND RICE METHOD FOR INTERPRETATION OF SLUG TESTS: FOR UNCONFINED AND LEAKY CONFINED AQUIFERS.
 TO UTILIZE THIS WORKSHEET, ENTER YOUR DATA AT LOCATIONS MARKED BY AN "X".
 PROGRAM CAN INCLUDE EFFECTS OF SANDPACK DEWATERING (ASSUMING WATER IS RISING WITHIN THE SANDPACK).

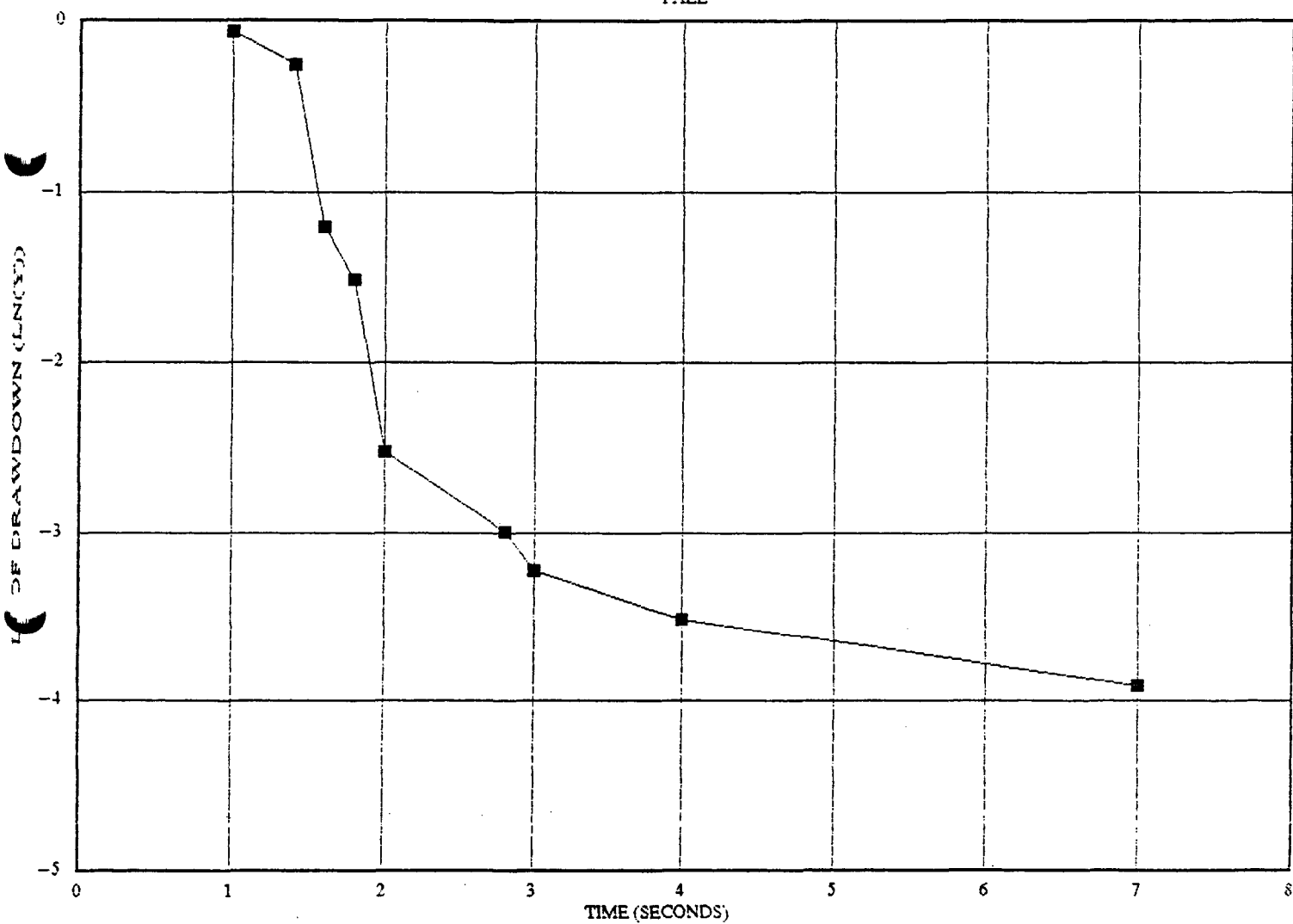
LINE NO.	DEPTH TO: (X)	BRANDOWN TIME (X)	LN	PROJECT NAME	MINCO
1	9.62	0.000	0.00	ERB	20026.024
2	9.96	0.340	1.00	DATE COLLECTED	12-1-90
3	9.80	0.780	1.40	WATER PIPE (ID)	5.0 in. = 0.0833 (radius in ft.)
4	9.32	0.500	1.60	RESPECTIVE SCREEN DIAMETER (ID)	5.0 in. = 0.0833 (radius in ft.)
5	9.24	0.220	1.80	RESPECTIVE SCREEN LENGTH (L)	5.25 ft.
6	9.10	0.020	2.00	DATE BRANDOWN (IN SUBJECT)	-0.78 ft.
7	9.07	0.050	2.60	STATIC WATER LEVEL (SWL)	9.02 ft.
8	9.06	0.000	3.00	DEPTH FROM SURF TO EFF. SCREEN BOTTOM (IN)	5.25 ft.
9	9.05	0.020	4.00	TEST, AQUIFER DEPTH (SML TO AQUIFER BOTTOM) (ID)	175.00 ft.
10	9.04	0.020	7.00	INCLUDE SANDPACK DEWATERING (ENTER 1 IF YES, 0 IF NO)?	0
11				SANDPACK'S SPECIFIC YIELD (SY) =	0.10
12					
13					
14					
15					
16					
17					
18					
19					
20					
21					
22					
23					
24					
25					
26					
27					
28					
29					
30					
31					
32					
33					
34					
35					
36					
37					
38					
39					
40					
41					
42					
43					

BOWEN AND RICE CURVE COEFFICIENTS:	
RATIO OF L/r SUB M =	27.75
LOG OF L/r SUB M =	1.4433
FOR PARTIALLY PENETRATING WELLS--	
A =	2.36
B =	0.32
FOR FULLY PENETRATING WELLS--	
C =	1.77
---EVALUATION OF LN(hg/r sub m):	
CONST. 1 =	0.3210
CONST. 2 =	6.2091
LN(hg/r sub m) =	2.06
EFFECTIVE P SUB C (FOR SANDPACK DEWATERING) = 0.0833	
1/(7)(LN(ho/r)) (SLOPE) =	-3.57E+00 sec ⁻¹
HYDRAULIC CONDUCTIVITY (K) =	
	2.76E-03 ft/sec
	8.40E-02 cm/sec
Regression Outputs:	
Constant	4.70E+00
Std Err of Y Est	0.2139
R Squared	0.9534
No. of Observations	4
Degrees of Freedom	2
X Coefficient(s)	-3.57E+00
Std Err of Const.	0.4782

t=14-30 s

RATE OF RECOVERY TEST: WELL WT-106A

FALL

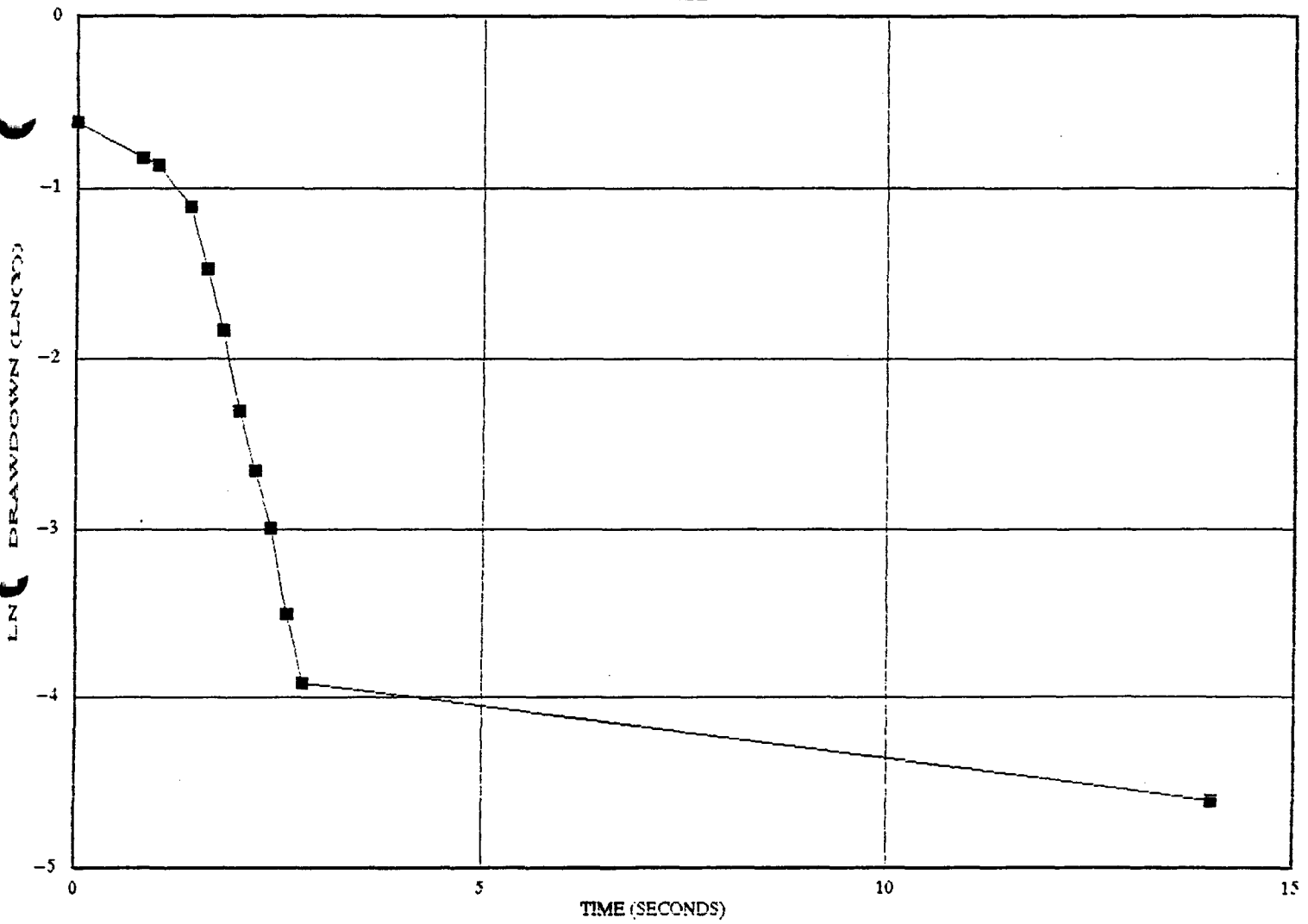


BOUMER AND RICE METHOD FOR INTERPRETATION OF SLUG TESTS: FOR UNCONFINED AND LEAKY CONFINED AQUIFERS.
 TO UTILIZE THIS WORKSHEET, ENTER YOUR DATA AT LOCATIONS MARKED BY AN "X".
 PROGRAM CAN INCLUDE EFFECTS OF SANDPACK DEWATERING (ASSUMING WATER IS RISING WITHIN THE SANDPACK).

TIME min	DEPTH TO WATER Ft.	DEPTH TO DRAINAGE Ft.	TIME sec	LN	PROJECT NAME	DATE COLLECTED
(X)	(Y)	(X)	(Y)			
1	8.45	0.540	0.00	-0.6162	ANALYST	ELIAG
2	8.52	0.440	0.20	-0.8210	DATE COLLECTED	10-1-90
3	8.60	0.420	1.00	-0.6875	WISER PIPE (ID)	2.0 in. = 0.0833 (radius in ft.)
4	8.69	0.330	1.40	-1.1067	EFFECTIVE SCREEN DIAMETER (ID)	5.0 in. = 0.3333 (radius in ft.)
5	8.79	0.230	1.60	-1.4697	EFFECTIVE SCREEN LENGTH (L)	9.25 Ft.
6	8.86	0.160	1.80	-1.8326	MAX DRAINAGE (IN SUBSET): (Ymax)	0.33 Ft.
7	8.92	0.100	2.00	-2.3026	STATIC WATER LEVEL (SWL)	9.02 Ft.
8	8.95	0.070	2.20	-2.6593	DEPTH FROM SWL TO EFF. SCREEN BOTTOM (H)	9.25 Ft.
9	8.97	0.050	2.40	-2.9957	TEST, AQUIFER DEPTH (SWL TO AQUIFER BOTTOM): (D)	175.00 Ft.
10	8.99	0.030	2.60	-3.5066	INCLUDE SANDPACK DEWATERING (ENTER 1 IF YES, 0 IF NO)?	0
11	9.00	0.020	2.80	-3.9120	SANDPACK'S SPECIFIC YIELD (Sy)	0.10
12	9.01	0.010	14.00	-4.6052		
13					BOUMER AND RICE CURVE COEFFICIENTS:	
14					RATIO OF $L/(r \text{ sub } w)$	27.75
15					LOG OF $L/(r \text{ sub } w)$	1.4433
16					FOR PARTIALLY PENETRATING WELLS--	
17					A	2.36
18					B	0.32
19					FOR FULLY PENETRATING WELLS--	
20					C	1.77
21					---EVALUATION OF $LN[Re/(r \text{ sub } w)]$:	
22					CONST. 1	0.3310
23					CONST. 2	6.2091
24					*(MAX. OF 6.0) =	6.0000
25					$LN[Re/(r \text{ sub } w)]$	2.06
26					EFFECTIVE $r \text{ sub } c$ (for sandpack dewatering) =	0.0833
27					$(1/T)(LN(Yc/Yt))$ (SLOPE) =	-2.00E+00 \sec^{-1}
28					HYDRAULIC CONDUCTIVITY (K)	1.55E-03 ft/sec
29						4.71E-02 cm/sec
30					Regression Output:	$t=1.4-2.85$
31					Constant	1.73E+00
32					Std Err of Y Est	0.0458
33					R Squared	0.9981
34					No. of Observations	8
35					Degrees of Freedom	6
36					X Coefficient(s)	-2.00E+00
37					Std Err of Coef.	0.0353

RATE OF RECOVERY TEST: WELL WT-106A

RISE

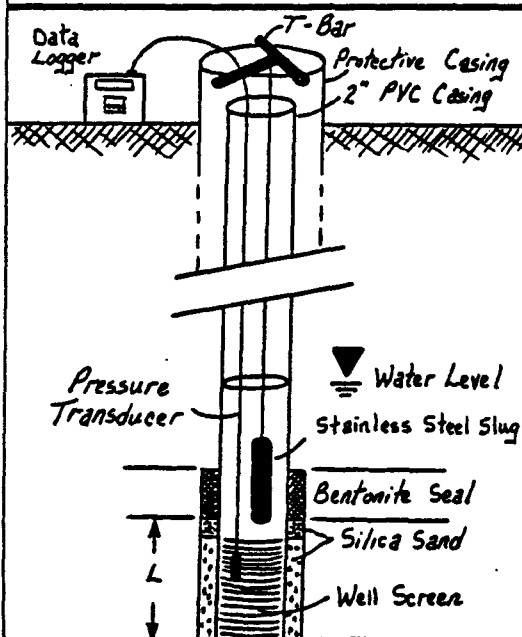


APPENDIX B

IN-FIELD HYDRAULIC CONDUCTIVITY SLUG TEST FIELD FORMS



INFIELD HYDRAULIC CONDUCTIVITY SLUG TEST

SHEET 1 OF 1PROJECT NO.: 20026.023
SITE: HIMCO DUMPWELL NUMBER: P102B
LOGGER ID NUMBER: 04CLIENT: USEPA
WELL DRILLED BY: John Mathos & Assoc
DATE TEST PERFORMED: Jan 4, 1991
TIME TEST PERFORMED: 1300
TOP OF PIPE ELEVATION: _____
OBSERVATION WELL/PIEZOMETER (circle): _____
FALL/RISE TEST (circle) BOTH
FORMATION WELL SCREENED IN: OUTWASH
STATIC WATER LEVEL (T.C.P.): 8.87TOTAL DEPTH OF WELL: 67.33'
DEPTH OF WATER IN WELL: 58.45'
INITIAL TRANSDUCER WATER LEVEL: 9.76
STATIC TRANSDUCER WATER LEVEL: _____
DIAMETER OF BOREHOLE: 8"
DIAMETER OF PIPE: 2"
SCREEN LENGTH: 5 feet
EFFECTIVE SCREEN LENGTH* "L": 9 feet

*"L" length is less than the sand pack length if the water table intersects sand pack; where "L" will equal distance between water table and bottom of sand pack.

SILOG II LOGGING SEQUENCE

SEGMENT NUMBER	NUMBER OF READINGS	INTERVAL (SEC.)	SEGMENT DURATION (SEC.)	ELAPSED TIME (SEC.)
1				
2				
3				
4				
5				
6				
7				
8				
9				
10				
11				
12				
13				
14				
15				
16				

PRESSURE TRANSDUCER PSI: _____

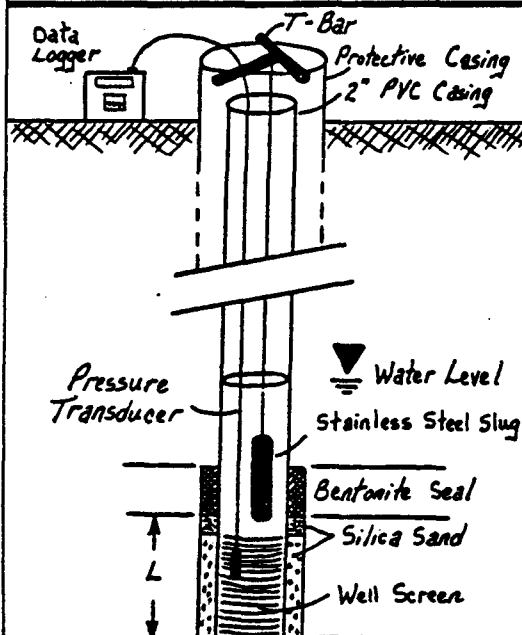
STAINLESS STEEL SLUG LENGTH: _____

NOTES: _____

_____TEST PERFORMED BY: TOM PUCHALSKI
LOGGER DOWNLOADED BY: K. Elan
CALCULATIONS BY: _____
COMPUTER FILE NAME: P102BDATE: Jan, 4, 1991
DATE: 1/14/91
DATE: _____



INFIELD HYDRAULIC CONDUCTIVITY SLUG TEST

SHEET 1 OF 1PROJECT NO.: 20026.023
SITE: HIMCO DUMPWELL NUMBER: P101B
LOGGER ID NUMBER: 02CLIENT: USEPA
WELL DRILLED BY: John Mathes & Assoc, Inc.
DATE TEST PERFORMED: 1/4/91
TIME TEST PERFORMED: 1140
TOP OF PIPE ELEVATION: _____
OBSERVATION WELL PIEZOMETER (circle): _____
FALL/RISE TEST (circle) _____
FORMATION WELL SCREENED IN: Anturash
STATIC WATER LEVEL (T.C.P.): 9.05TOTAL DEPTH OF WELL: 100.57
DEPTH OF WATER IN WELL: 91.00
INITIAL TRANSDUCER WATER LEVEL: 10.46
STATIC TRANSDUCER WATER LEVEL: _____
DIAMETER OF BOREHOLE: 8"
DIAMETER OF PIPE: 2"
SCREEN LENGTH: 5'
EFFECTIVE SCREEN LENGTH * "L": 5'

*"L" length is less than the sand pack length if the water table intersects sand pack, where "L" will equal distance between water table and bottom of sand pack.

SILOG II LOGGING SEQUENCE

SEGMENT NUMBER	NUMBER OF READINGS	INTERVAL (SEC.)	SEGMENT DURATION (SEC.)	ELAPSED TIME (SEC.)
1	25	1/5	5	5
2	25	1	25	30
3	10	2	30	50
4	30	5	150	200
5				
6				
7				
8				
9				
10				
11				
12				
13				
14				
15				
16				

PRESSURE TRANSDUCER PSI: 5
STAINLESS STEEL SLUG LENGTH: 4 feet

NOTES: _____

TEST PERFORMED BY: TAM PUCHALSKI
LOGGER DOWNLOADED BY: VE
CALCULATIONS BY: VE
COMPUTER FILE NAME: P101BDATE: 1/4/91
DATE: 1/11/91
DATE: _____

INFIELD HYDRAULIC CONDUCTIVITY SLUG TEST

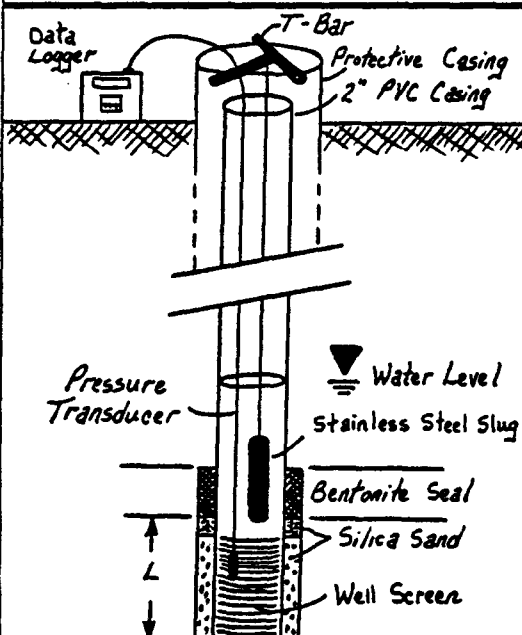
SHEET 1 OF 1

PROJECT NO.: 20026.023
SITE: HIMCO DUMP

WELL NUMBER: P101C
LOGGER ID NUMBER: 01

CLIENT: USEPA
WELL DRILLED BY: John Mathes & Assoc. Inc.
DATE TEST PERFORMED: 1/4/91
TIME TEST PERFORMED: 1040
TOP OF PIPE ELEVATION: _____
OBSERVATION WELL (PIEZOMETER (circle): _____
FALL/RISE TEST (circle) _____
FORMATION WELL SCREENED IN: Outwash SP
STATIC WATER LEVEL (T.C.P.): _____

TOTAL DEPTH OF WELL: 162.67'
DEPTH OF WATER IN WELL: 9.33' 9.57'
INITIAL TRANSDUCER WATER LEVEL: 9.55
STATIC TRANSDUCER WATER LEVEL: 10.88
DIAMETER OF BOREHOLE: 8 inches
DIAMETER OF PIPE: 2 inches
SCREEN LENGTH: 5 feet
EFFECTIVE SCREEN LENGTH * "L": 5 feet



*"L" length is less than the sand pack length if the water table intersects sand pack, where "L" will equal distance between water table and bottom of sand pack.

SILOG II LOGGING SEQUENCE				
SEGMENT NUMBER	NUMBER OF READINGS	INTERVAL (SEC.)	SEGMENT DURATION (SEC.)	ELAPSED TIME (SEC.)
1	5	11.5	1	11.5
2	5	11.5	1	23.0
3				34.5
4				46.0
5				57.5
6				69.0
7				80.5
8				92.0
9				103.5
10				115.0
11	25	11.5	5	120.5
12	25	1	25	145.5
13	10	2	20	165.5
14	30	5	150	315.5
15				
16				

PRESSURE TRANSDUCER PSI: 5
STAINLESS STEEL SLUG LENGTH: 4

NOTES: Reran test at 1241 Station 03 transducer static 9.98
11.43 - static start rising test - Poor test

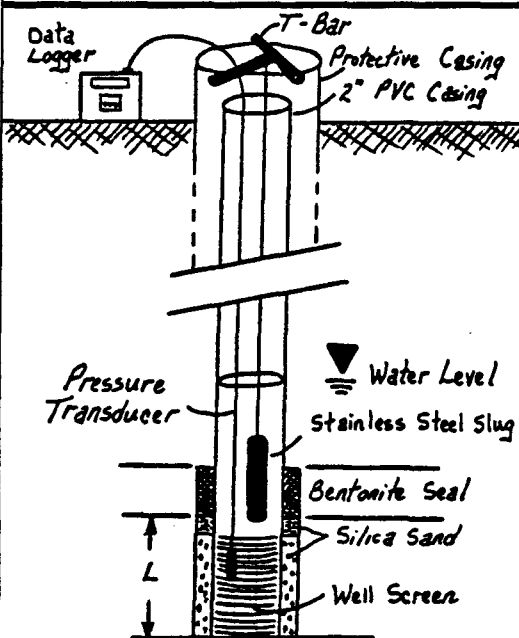
TEST PERFORMED BY: TOM PUCHALSKI
LOGGER DOWNLOADED BY: C. Elias
CALCULATIONS BY: KE
COMPUTER FILE NAME: P101C R
1

DATE: 1/4/91
DATE: 1/4/91
DATE: _____



INFIELD HYDRAULIC CONDUCTIVITY SLUG TEST

SHEET ____ OF ____

PROJECT NO.: 20026.023
SITE: HimcoWELL NUMBER: E-3
LOGGER ID NUMBER: 719021CLIENT: USEPA
WELL DRILLED BY: _____
DATE TEST PERFORMED: 12-14-90
TIME TEST PERFORMED: 11:15
TOP OF PIPE ELEVATION: _____
OBSERVATION WELL/PIEZOMETER (circle): _____
FALL/RISE TEST (circle) Both
FORMATION WELL SCREENED IN: _____
STATIC WATER LEVEL (T.C.P.): _____TOTAL DEPTH OF WELL: 175.58'
DEPTH OF WATER IN WELL: 11.60'
INITIAL TRANSDUCER WATER LEVEL: 7.96'
STATIC TRANSDUCER WATER LEVEL: 7.96'
DIAMETER OF BOREHOLE: _____
DIAMETER OF PIPE: 5" ID
SCREEN LENGTH: _____
EFFECTIVE SCREEN LENGTH * "L": _____

"L" length is less than the sand pack length if the water table intersects sand pack, where "L" will equal distance between water table and bottom of sand pack.

SILOG II LOGGING SEQUENCE

SEGMENT NUMBER	NUMBER OF READINGS	INTERVAL (SEC.)	SEGMENT DURATION (SEC.)	ELAPSED TIME (SEC.)
1	50	0.2	10	10
2	15	1	15	15
3	15	5	75	75
4	15	30	450	450
5				
6				
7	50	0.2	10	10
8	15	1	15	15
9	15	5	75	75
10	15	30	450	450
11				
12				
13				
14				
15				
16				

F.H.

R.H.

PRESSURE TRANSDUCER PSI: 15
STAINLESS STEEL SLUG LENGTH: 4'NOTES: Identified as 53TEST PERFORMED BY: T. Knecht & F. Seussger
LOGGER DOWNLOADED BY: T. Knecht
CALCULATIONS BY: _____
COMPUTER FILE NAME: _____DATE: 12-14-90
DATE: 12-14-90
DATE: _____

INFIELD HYDRAULIC CONDUCTIVITY SLUG TEST

SHEET 1 OF 1

PROJECT NO.: 20020-023

WELL NUMBER: F-2

SITE: HIMCO

LOGGER ID NUMBER: 719021

CLIENT: EPA

TOTAL DEPTH OF WELL: > 150'

WELL DRILLED BY: _____

DEPTH OF WATER IN WELL: 13.95'

DATE TEST PERFORMED: 12-2-90

INITIAL TRANSDUCER WATER LEVEL: _____

TIME TEST PERFORMED: 0950

STATIC TRANSDUCER WATER LEVEL: 10.06'

TOP OF PIPE ELEVATION: _____

DIAMETER OF BOREHOLE: _____

OBSERVATION WELL PIEZOMETER (circle): _____

DIAMETER OF PIPE: 5"

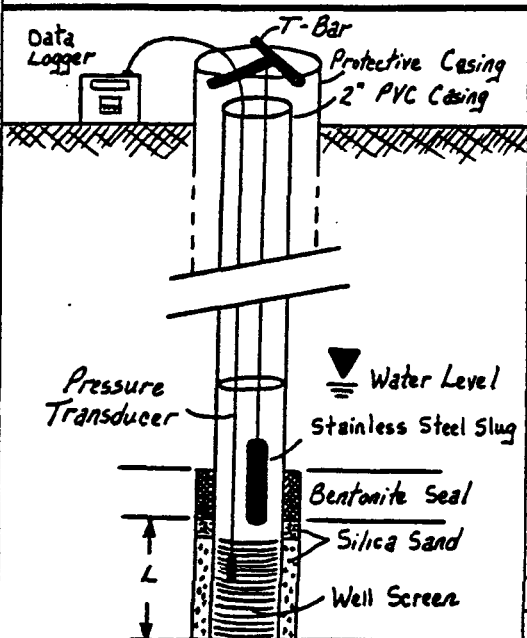
FALL/RISE TEST (circle) Rise

SCREEN LENGTH: _____

FORMATION WELL SCREENED IN: _____

EFFECTIVE SCREEN LENGTH* "L": _____

STATIC WATER LEVEL (T.C.P.): _____



*"L" length is less than the sand pack length if the water table intersects sand pack, where "L" will equal distance between water table and bottom of sand pack.

SILOG II LOGGING SEQUENCE

SEGMENT NUMBER	NUMBER OF READINGS	INTERVAL (SEC.)	SEGMENT DURATION (SEC.)	ELAPSED TIME (SEC.)
1	50	0.2	10	10
2	15	1	15	15
3	15	5	75	75
4	15	30	450	450
5				
6				
7				
8				
9				
10				
11				
12				
13				
14				
15				
16				

PRESSURE TRANSDUCER PSI: 15

STAINLESS STEEL SLUG LENGTH: 4'

NOTES: Identified AS 02

TEST PERFORMED BY: C. Feneke, T. Kach

DATE: 12-2-90

LOGGER DOWNLOADED BY: C. Feneke

DATE: 12-2-90

CALCULATIONS BY: _____

DATE: _____

COMPUTER FILE NAME: _____



INFIELD HYDRAULIC CONDUCTIVITY SLUG TEST

SHEET ____ OF ____

PROJECT NO.: 20024-013WELL NUMBER: F-7SITE: HIMCOLOGGER ID NUMBER: 719021CLIENT: EPATOTAL DEPTH OF WELL: 31.3'

WELL DRILLED BY: _____

DEPTH OF WATER IN WELL: 8.45'DATE TEST PERFORMED: 12-2-90

INITIAL TRANSDUCER WATER LEVEL: _____

TIME TEST PERFORMED: 0915STATIC TRANSDUCER WATER LEVEL: 10.05'

TOP OF PIPE ELEVATION: _____

DIAMETER OF BOREHOLE: _____

OBSERVATION WELL/PIEZOMETER (circle): _____

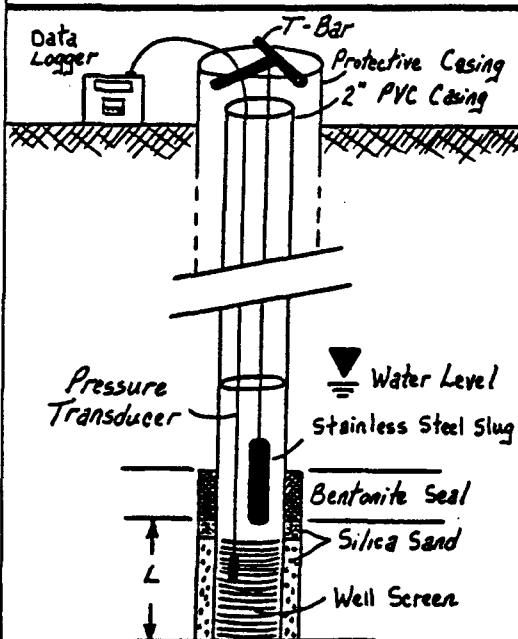
DIAMETER OF PIPE: 2"FALL/RISE TEST (circle) Both

SCREEN LENGTH: _____

FORMATION WELL SCREENED IN: _____

EFFECTIVE SCREEN LENGTH* "L": _____

STATIC WATER LEVEL (T.C.P.): _____



*"L" length is less than the sand pack length if the water table intersects sand pack, where "L" will equal distance between water table and bottom of sand pack.

SILOG II LOGGING SEQUENCE

SEGMENT NUMBER	NUMBER OF READINGS	INTERVAL (SEC.)	SEGMENT DURATION (SEC.)	ELAPSED TIME (SEC.)
1	50	0.2	10	10
2	15	1	30	30
3	15	2	30	30
4				
5				
6				
7				
8				
9				
10				
11				
12				
13				
14				
15				
16				

PRESSURE TRANSDUCER PSI: 15STAINLESS STEEL SLUG LENGTH: 4'NOTES: Identified as O1- Well Not LockedTEST PERFORMED BY: CFRIDA, J. KRACHDATE: 12-2-90

LOGGER DOWNLOADED BY: _____

DATE: _____

CALCULATIONS BY: _____

DATE: _____

COMPUTER FILE NAME: _____

INFIELD HYDRAULIC CONDUCTIVITY SLUG TEST

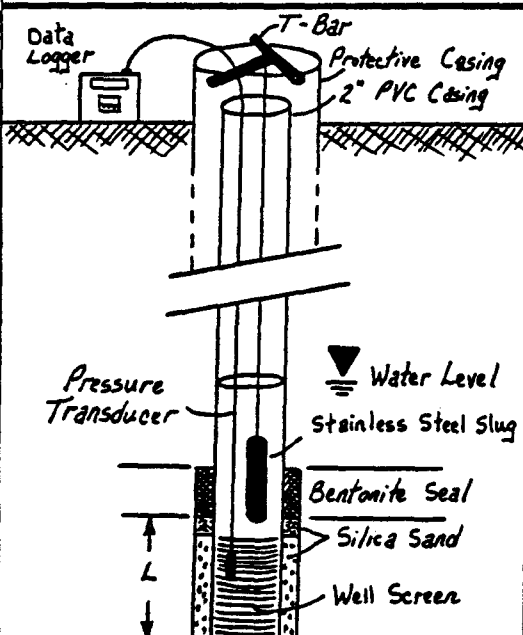
SHEET 1 OF 1

PROJECT NO.: 20020 023
SITE: HIMCO

WELL NUMBER: M-1
LOGGER ID NUMBER: 719021

CLIENT: EPA
WELL DRILLED BY: _____
DATE TEST PERFORMED: 12-2-90
TIME TEST PERFORMED: 1130
TOP OF PIPE ELEVATION: _____
CF OBSERVATION WELL/PIEZOMETER (circle): _____
FALL/RISE TEST (circle) Both
FORMATION WELL SCREENED IN: _____
STATIC WATER LEVEL (T.C.P.): _____

TOTAL DEPTH OF WELL: 104.50'
DEPTH OF WATER IN WELL: 16.10'
INITIAL TRANSDUCER WATER LEVEL: _____
STATIC TRANSDUCER WATER LEVEL: 9.98'
DIAMETER OF BOREHOLE: _____
DIAMETER OF PIPE: 2"
SCREEN LENGTH: _____
EFFECTIVE SCREEN LENGTH * "L": _____



*"L" length is less than the sand pack length if the water table intersects sand pack, where "L" will equal distance between water table and bottom of sand pack.

SILOG II LOGGING SEQUENCE				
SEGMENT NUMBER	NUMBER OF READINGS	INTERVAL (SEC.)	SEGMENT DURATION (SEC.)	ELAPSED TIME (SEC.)
1	50	0.2	10	10
2	15	1	15	15
3	15	5	75	75
4	15	30	450	450
5				
6	50	0.2	10	10
7	15	1	15	15
8	15	2	30	30
9	15	10	150	150
10	6	10	60	60
11				
12				
13				
14				
15				
16				

Falling Head
Rising Head

PRESSURE TRANSDUCER PSI: 15
STAINLESS STEEL SLUG LENGTH: 4'

NOTES: Falling Head test stopped - returned to static before segment 4 was completed

Station ID #3

TEST PERFORMED BY: C. F. R. & T. K. R. DATE: 12-2-90
LOGGER DOWNLOADED BY: _____ DATE: _____
CALCULATIONS BY: _____ DATE: _____
COMPUTER FILE NAME: _____

INFIELD HYDRAULIC CONDUCTIVITY SLUG TEST

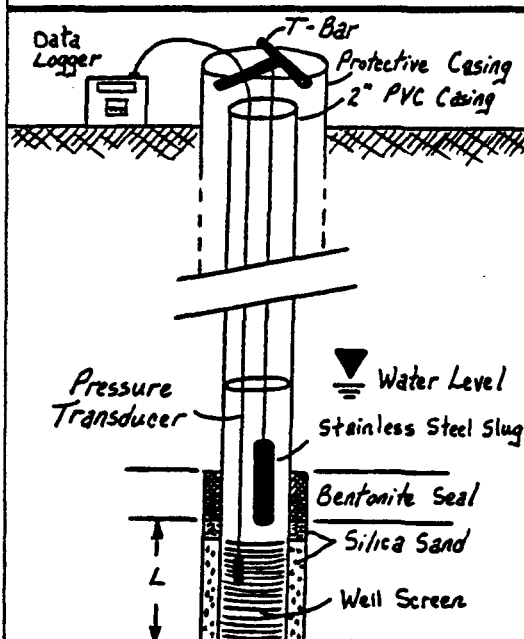
SHEET ____ OF ____

PROJECT NO.: 20026.023
SITE: HIMCO

WELL NUMBER: M-2
LOGGER ID NUMBER: 719021

CLIENT: EPA
WELL DRILLED BY: _____
DATE TEST PERFORMED: 12-2-90
TIME TEST PERFORMED: 11:35 12-2-90
TOP OF PIPE ELEVATION: _____
OBSERVATION WELL/PIEZOMETER (circle): _____
FALL/RISE TEST (circle) Rise
FORMATION WELL SCREENED IN: _____
STATIC WATER LEVEL (T.C.P.): _____

TOTAL DEPTH OF WELL: 24.80'
DEPTH OF WATER IN WELL: 15.25'
INITIAL TRANSDUCER WATER LEVEL: _____
STATIC TRANSDUCER WATER LEVEL: 8.03'
DIAMETER OF BOREHOLE: _____
DIAMETER OF PIPE: 2"
SCREEN LENGTH: _____
EFFECTIVE SCREEN LENGTH* "L": _____



*"L" length is less than the sand pack length if the water table intersects sand pack, where "L" will equal distance between water table and bottom of sand pack.

SILOG II LOGGING SEQUENCE

SEGMENT NUMBER	NUMBER OF READINGS	INTERVAL (SEC.)	SEGMENT DURATION (SEC.)	ELAPSED TIME (SEC.)
1				
2				
3				
4				
5				
6				
7				
8				
9				
10				
11				
12				
13				
14				
15				
16				

PRESSURE TRANSDUCER PSI: _____
STAINLESS STEEL SLUG LENGTH: _____

NOTES: SHOWN ID # 4
Obstruction At ~ 16' Slug could not go down
well - Redone on 12-14-90 with 2' slug; form attached

TEST PERFORMED BY: C. Frawley, T. Kucha DATE: 12-2-90
LOGGER DOWNLOADED BY: _____ DATE: _____
CALCULATIONS BY: _____ DATE: _____
COMPUTER FILE NAME: _____

INFIELD HYDRAULIC CONDUCTIVITY SLUG TEST

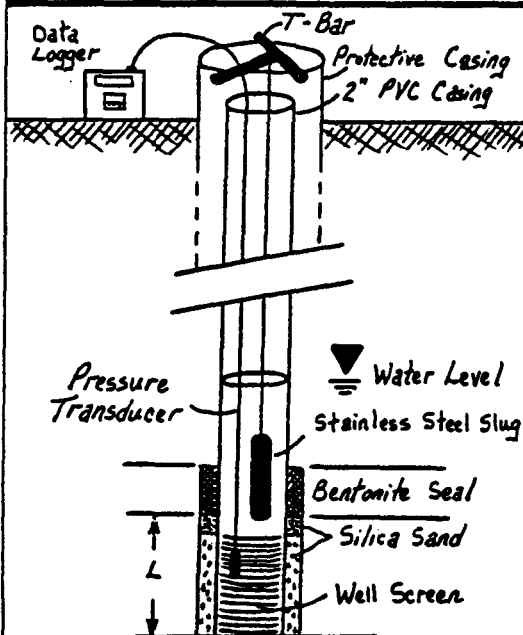
SHEET ____ OF ____

PROJECT NO.: 20026.023
SITE: Hmco

WELL NUMBER: M-2
LOGGER ID NUMBER: 219021

CLIENT: _____
WELL DRILLED BY: _____
DATE TEST PERFORMED: 12-14-90
TIME TEST PERFORMED: _____
TOP OF PIPE ELEVATION: _____
OBSERVATION WELL/PIEZOMETER (circle): _____
FALL/RISE TEST (circle): _____
FORMATION WELL SCREENED IN: _____
STATIC WATER LEVEL (T.C.P.): _____

TOTAL DEPTH OF WELL: 24.80
DEPTH OF WATER IN WELL: 15.27
INITIAL TRANSDUCER WATER LEVEL: _____
STATIC TRANSDUCER WATER LEVEL: 7.01
DIAMETER OF BOREHOLE: _____
DIAMETER OF PIPE: 2"
SCREEN LENGTH: _____
EFFECTIVE SCREEN LENGTH* "L": _____



SILOG II LOGGING SEQUENCE				
SEGMENT NUMBER	NUMBER OF READINGS	INTERVAL (SEC.)	SEGMENT DURATION (SEC.)	ELAPSED TIME (SEC.)
1	50	0.2	10	10
2	15	1	15	15
3	15	5	75	75
4	15	30	450	450
5				
6	50	0.2	10	10
7	15	1	15	15
8	15	5	75	75
9	15	30	450	450
10				
11				
12				
13				
14				
15				
16				

*"L" length is less than the sand pack length if the water table intersects sand pack, where "L" will equal distance between water table and bottom of sand pack.

PRESSURE TRANSDUCER PSI: 15
STAINLESS STEEL SLUG LENGTH: 2'

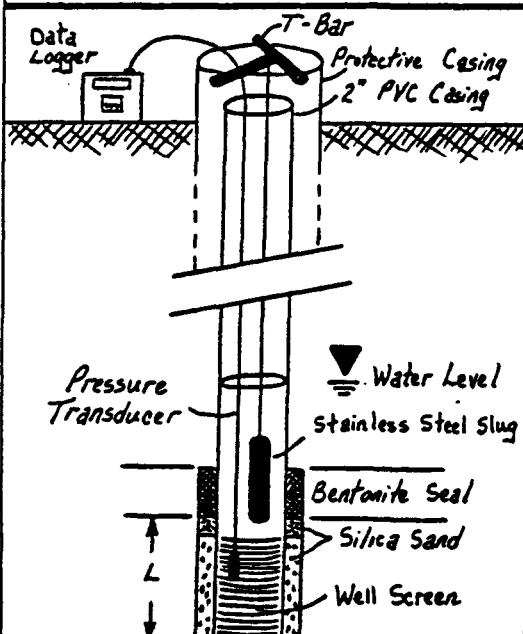
NOTES: Indicated @ 22

TEST PERFORMED BY: A. Krach; E. Slusser
LOGGER DOWNLOADED BY: A. Krach
CALCULATIONS BY: _____
COMPUTER FILE NAME: _____

DATE: 12-14-90
DATE: 12-14-90
DATE: _____



INFIELD HYDRAULIC CONDUCTIVITY SLUG TEST

SHEET 1 OF 1PROJECT NO.: 20026.023
SITE: HIMCOWELL NUMBER: WT 101A
LOGGER ID NUMBER: 719021CLIENT: EPA
WELL DRILLED BY: Donohue ¹²⁻¹⁹⁰ NATICS
DATE TEST PERFORMED: 12/1/90
TIME TEST PERFORMED: 1428 + 1430
TOP OF PIPE ELEVATION: _____
OBSERVATION WELL/PIEZOMETER (circle): _____
FALL/RISE TEST (circle) Both
FORMATION WELL SCREENED IN: _____
STATIC WATER LEVEL (T.C.P.): -TOTAL DEPTH OF WELL: -18.70
DEPTH OF WATER IN WELL: -11.26 } 1 1/2
INITIAL TRANSDUCER WATER LEVEL: _____
STATIC TRANSDUCER WATER LEVEL: 7.02'
DIAMETER OF BOREHOLE: _____
DIAMETER OF PIPE: 2"
SCREEN LENGTH: _____
EFFECTIVE SCREEN LENGTH* "L": _____

*"L" length is less than the sand pack length if the water table intersects sand pack, where "L" will equal distance between water table and bottom of sand pack.

SILOG II LOGGING SEQUENCE				
SEGMENT NUMBER	NUMBER OF READINGS	INTERVAL (SEC.)	SEGMENT DURATION (SEC.)	ELAPSED TIME (SEC.)
1	50	0.2 seconds	10	10
2	60	1 second	60	60
3				
4				
5				
6				
7				
8				
9				
10				
11				
12				
13				
14				
15				
16				

PRESSURE TRANSDUCER PSI: 15
STAINLESS STEEL SLUG LENGTH: 4'NOTES: Rising & Falling Head tests manually stopped due to very fast recoveryTEST PERFORMED BY: Cathy Fruehe
LOGGER DOWNLOADED BY: Cathy Fruehe
CALCULATIONS BY: _____
COMPUTER FILE NAME: _____DATE: 12/1/90
DATE: 12/1/90
DATE: _____

INFIELD HYDRAULIC CONDUCTIVITY SLUG TEST

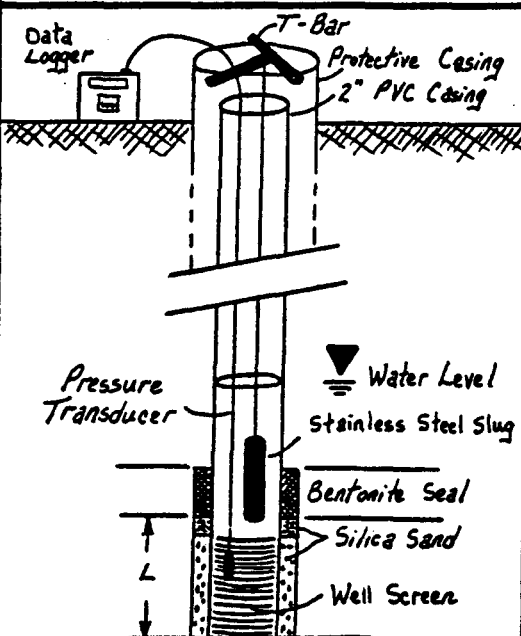
SHEET ____ OF ____

PROJECT NO.: 20026.023
SITE: Himco

WELL NUMBER: WT102A
LOGGER ID NUMBER: 719021

CLIENT: USEPA
WELL DRILLED BY: _____
DATE TEST PERFORMED: 12-14-90
TIME TEST PERFORMED: 14:30
TOP OF PIPE ELEVATION: _____
OBSERVATION WELL/PIEZOMETER (circle): _____
FALL/RISE TEST (circle) BOTH
FORMATION WELL SCREENED IN: _____
STATIC WATER LEVEL (T.C.P.): _____

TOTAL DEPTH OF WELL: 18.16
DEPTH OF WATER IN WELL: 10.29'
INITIAL TRANSDUCER WATER LEVEL: _____
STATIC TRANSDUCER WATER LEVEL: 7.01
DIAMETER OF BOREHOLE: _____
DIAMETER OF PIPE: 2"
SCREEN LENGTH: _____
EFFECTIVE SCREEN LENGTH* "L": _____



*"L" length is less than the sand pack length if the water table intersects sand pack, where "L" will equal distance between water table and bottom of sand pack.

SILOG II LOGGING SEQUENCE				
SEGMENT NUMBER	NUMBER OF READINGS	INTERVAL (SEC.)	SEGMENT DURATION (SEC.)	ELAPSED TIME (SEC.)
1	50	0.2	10	10
2	15	1	15	15
3	15	5	75	75
4	15	30	450	450
5				
1	50	0.2	10	10
2	15	1	15	15
3	15	5	75	75
4	15	30	450	450
10				
11				
12				
13				
14				
15				
16				

PRESSURE TRANSDUCER PSI: 15"
STAINLESS STEEL SLUG LENGTH: 4"

NOTES: Identified as 12

TEST PERFORMED BY: T. Koach E. Shusser
LOGGER DOWNLOADED BY: T. Koach
CALCULATIONS BY: _____
COMPUTER FILE NAME: _____

DATE: 12-14-90
DATE: 12-14-90
DATE: _____

F.H.
R.H.

INFIELD HYDRAULIC CONDUCTIVITY SLUG TEST

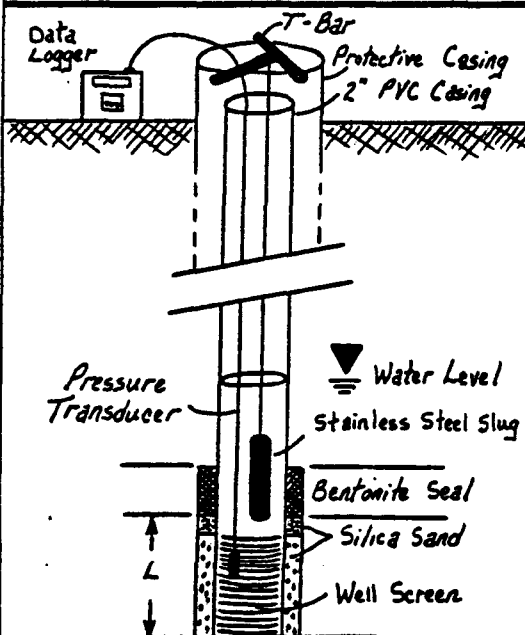
SHEET ____ OF ____

PROJECT NO.: 20026.023
SITE: Himer

WELL NUMBER: WT103A
LOGGER ID NUMBER: 719021

CLIENT: USEPA
WELL DRILLED BY: _____
DATE TEST PERFORMED: 12-14-90
TIME TEST PERFORMED: 13:59
TOP OF PIPE ELEVATION: _____
☒ OBSERVATION WELL/PIEZOMETER (circle): _____
FALL/RISE TEST (circle) BOTH
FORMATION WELL SCREENED IN: _____
STATIC WATER LEVEL (T.C.P.): _____

TOTAL DEPTH OF WELL: 18.48
DEPTH OF WATER IN WELL: 5.46
INITIAL TRANSDUCER WATER LEVEL: _____
STATIC TRANSDUCER WATER LEVEL: 7.98'
DIAMETER OF BOREHOLE: 2"
DIAMETER OF PIPE: _____
SCREEN LENGTH: _____
EFFECTIVE SCREEN LENGTH * "L": _____



*"L" length is less than the sand pack length if the water table intersects sand pack, where "L" will equal distance between water table and bottom of sand pack.

SILOG II LOGGING SEQUENCE				
SEGMENT NUMBER	NUMBER OF READINGS	INTERVAL (SEC.)	SEGMENT DURATION (SEC.)	ELAPSED TIME (SEC.)
1	50	0.2	10	10
2	15	1	15	15
3	15	5	75	75
4	15	30	450	450
5				
6				
7				
8				
9				
10				
11				
12				
13				
14				
15				
16				

PRESSURE TRANSDUCER PSI: 15
STAINLESS STEEL SLUG LENGTH: 4'

NOTES: Identified as L3

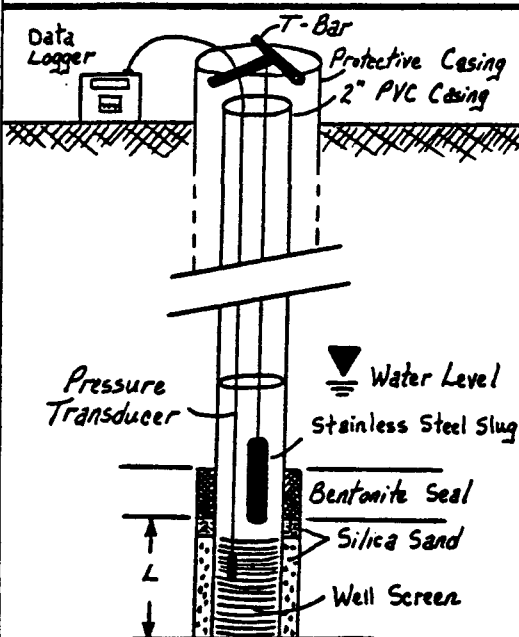
TEST PERFORMED BY: T. Kneel, E. Shusser
LOGGER DOWNLOADED BY: T. Poach
CALCULATIONS BY: _____
COMPUTER FILE NAME: _____

DATE: 12-14-90
DATE: 12-14-90
DATE: _____



INFIELD HYDRAULIC CONDUCTIVITY SLUG TEST

SHEET ____ OF ____

PROJECT NO.: 20026.023
SITE: HimcoWELL NUMBER: WT104A
LOGGER ID NUMBER: 719021CLIENT: USEPA
WELL DRILLED BY: _____
DATE TEST PERFORMED: 12-14-90
TIME TEST PERFORMED: 1200
TOP OF PIPE ELEVATION: _____
OBSERVATION WELL/PIEZOMETER (circle): _____
FALL/RISE TEST (circle) F.H.
FORMATION WELL SCREENED IN: _____
STATIC WATER LEVEL (T.C.P.): _____TOTAL DEPTH OF WELL: 13.69'
DEPTH OF WATER IN WELL: 11.67'
INITIAL TRANSDUCER WATER LEVEL: _____
STATIC TRANSDUCER WATER LEVEL: 6.01'
DIAMETER OF BOREHOLE: _____
DIAMETER OF PIPE: 2" ID
SCREEN LENGTH: _____
EFFECTIVE SCREEN LENGTH* "L": _____

SILOG II LOGGING SEQUENCE

SEGMENT NUMBER	NUMBER OF READINGS	INTERVAL (SEC.)	SEGMENT DURATION (SEC.)	ELAPSED TIME (SEC.)
1	50	0.2	10	10
2	15	1	15	15
3	15	5	75	75
4	15	30	450	450
5				
6 1	50	0.2	10	10
7 2	15	1	15	15
8 3	15	5	75	75
9 4	15	30	450	450
10				
11				
12				
13				
14				
15				
16				

*"L" length is less than the sand pack length if the water table intersects sand pack, where "L" will equal distance between water table and bottom of sand pack.

PRESSURE TRANSDUCER PSI: 1.5
STAINLESS STEEL SLUG LENGTH: 4'NOTES: Identified as 14TEST PERFORMED BY: T. Knoch, E. Shuman
LOGGER DOWNLOADED BY: T. Knoch
CALCULATIONS BY: _____
COMPUTER FILE NAME: _____DATE: 12-14-90
DATE: 12-14-90
DATE: _____



INFIELD HYDRAULIC CONDUCTIVITY SLUG TEST

SHEET 1 OF 1PROJECT NO.: Z0026.023WELL NUMBER: WT105ASITE: HIMCOLOGGER ID NUMBER: 719021CLIENT: EPATOTAL DEPTH OF WELL: 18.55'WELL DRILLED BY: MATHESDEPTH OF WATER IN WELL: 9.28'DATE TEST PERFORMED: 12-1-90

INITIAL TRANSDUCER WATER LEVEL: _____

TIME TEST PERFORMED: 1600STATIC TRANSDUCER WATER LEVEL: 7.98'

TOP OF PIPE ELEVATION: _____

DIAMETER OF BOREHOLE: _____

OBSERVATION WELL PIEZOMETER (circle): _____

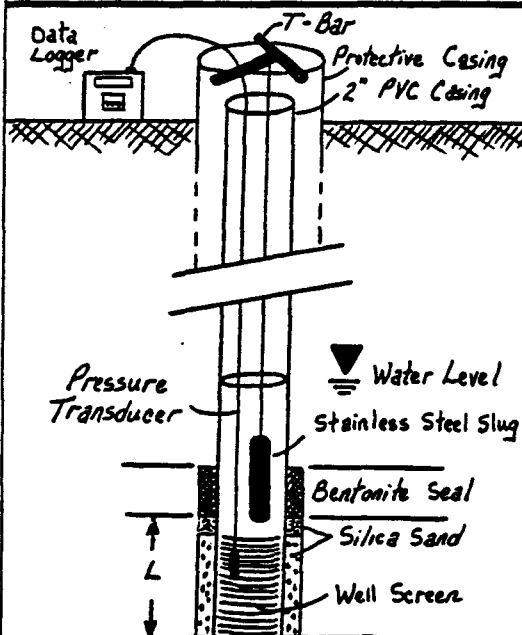
DIAMETER OF PIPE: 2"FALL/RISE TEST (circle) Both

SCREEN LENGTH: _____

FORMATION WELL SCREENED IN: _____

EFFECTIVE SCREEN LENGTH * "L": _____

STATIC WATER LEVEL (T.C.P.): _____



"L" length is less than the sand pack length if the water table intersects sand pack, where "L" will equal distance between water table and bottom of sand pack.

SILOG II LOGGING SEQUENCE

SEGMENT NUMBER	NUMBER OF READINGS	INTERVAL (SEC.)	SEGMENT DURATION (SEC.)	ELAPSED TIME (SEC.)
1	50	0.2	10	10
2	15	1	15	15
3	15	2	30	30
4				
5				
6				
7				
8				
9				
10				
11				
12				
13				
14				
15				
16				

PRESSURE TRANSDUCER PSI: 15STAINLESS STEEL SLUG LENGTH: 4'

NOTES: _____

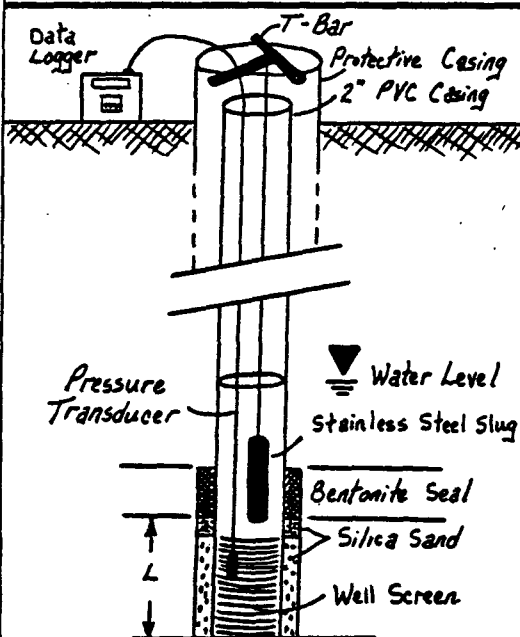
TEST PERFORMED BY: C. FRUEHE, S. SPIELWAG, E. SASSER DATE: 12-1-90LOGGER DOWNLOADED BY: C. FRUEHE DATE: 12-1-90

CALCULATIONS BY: _____ DATE: _____

COMPUTER FILE NAME: _____



INFIELD HYDRAULIC CONDUCTIVITY SLUG TEST

SHEET 1 OF 1PROJECT NO.: 20024.023
SITE: HINCOWELL NUMBER: WT 106A
LOGGER ID NUMBER: 719021CLIENT: EPA
WELL DRILLED BY: MATHES
DATE TEST PERFORMED: 12-1-90
TIME TEST PERFORMED: 1530
TOP OF PIPE ELEVATION: _____
OBSERVATION WELL/PIEZOMETER (circle): _____
FALL/RISE TEST (circle) Both
FORMATION WELL SCREENED IN: _____
STATIC WATER LEVEL (T.C.P.): _____TOTAL DEPTH OF WELL: 18.50'
DEPTH OF WATER IN WELL: 8.45'
INITIAL TRANSDUCER WATER LEVEL: 9.02
STATIC TRANSDUCER WATER LEVEL: 9.02
DIAMETER OF BOREHOLE: _____
DIAMETER OF PIPE: 2"
SCREEN LENGTH: _____
EFFECTIVE SCREEN LENGTH* "L": _____

*"L" length is less than the sand pack length if the water table intersects sand pack, where "L" will equal distance between water table and bottom of sand pack.

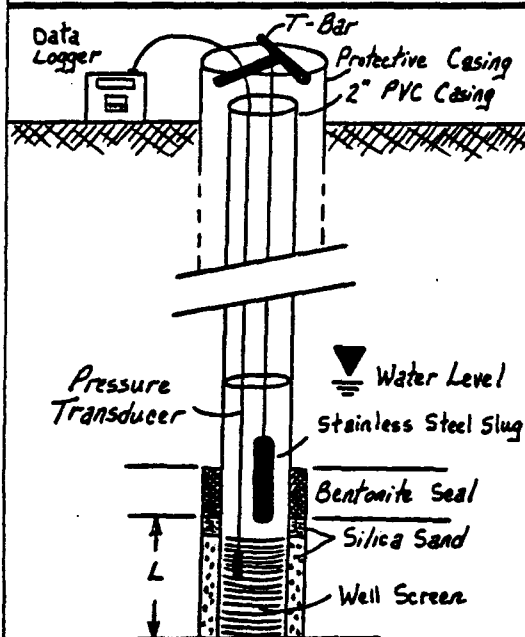
SILOG II LOGGING SEQUENCE				
SEGMENT NUMBER	NUMBER OF READINGS	INTERVAL (SEC.)	SEGMENT DURATION (SEC.)	ELAPSED TIME (SEC.)
1	50	0.2	10	10
2	15	1	15	15
3	15	2	30	30
4				
5				
6				
7				
8				
9				
10				
11				
12				
13				
14				
15				
16				

PRESSURE TRANSDUCER PSI: 15
STAINLESS STEEL SLUG LENGTH: 4'NOTES: _____

_____TEST PERFORMED BY: C. FEUER, S. SPINAK, E. SLUSSER DATE: 12-1-90
LOGGER DOWNLOADED BY: C. FEUER DATE: 12-1-90
CALCULATIONS BY: _____ DATE: _____
COMPUTER FILE NAME: _____



INFIELD HYDRAULIC CONDUCTIVITY SLUG TEST

SHEET 1 OF 1PROJECT NO.: 20026-023
SITE: HIMCO DUMPWELL NUMBER: P102C
LOGGER ID NUMBER: 05CLIENT: USEPA
WELL DRILLED BY: John Mathies & Assoc
DATE TEST PERFORMED: Jan 4, 1991
TIME TEST PERFORMED: 1336
TOP OF PIPE ELEVATION: _____
OBSERVATION WELL/PIEZOMETER (circle): _____
(FALL/RISE TEST (circle) BOTH)
FORMATION WELL SCREENED IN: OUTWASH
STATIC WATER LEVEL (T.C.P.): 9.41'TOTAL DEPTH OF WELL: 158.81
DEPTH OF WATER IN WELL: 149.40
INITIAL TRANSDUCER WATER LEVEL: 11.29'
STATIC TRANSDUCER WATER LEVEL: 10.88'
DIAMETER OF BOREHOLE: 8"
DIAMETER OF PIPE: 2"
SCREEN LENGTH: 5'
EFFECTIVE SCREEN LENGTH * "L": 5'

*"L" length is less than the sand pack length if the water table intersects sand pack, where "L" will equal distance between water table and bottom of sand pack.

SILOG II LOGGING SEQUENCE				
SEGMENT NUMBER	NUMBER OF READINGS	INTERVAL (SEC.)	SEGMENT DURATION (SEC.)	ELAPSED TIME (SEC.)
1				
2				
3				
4				
5				
6				
7				
8				
9				
10				
11				
12				
13				
14				
15				
16				

PRESSURE TRANSDUCER PSI: 5
STAINLESS STEEL SLUG LENGTH: 4NOTES: Water level did not drop during falling head testTEST PERFORMED BY: JOHN PUCHALSKI
LOGGER DOWNLOADED BY: KIM ELIAS
CALCULATIONS BY: KE
COMPUTER FILE NAME: P102CR
" FDATE: Jan 4, 1991
DATE: 1/14/91
DATE: _____

ORIGINAL

TECHNICAL MEMORANDUM NUMBER 12

DATE: February 17, 1991

TO: Vanessa Harris, Site Manager

CC: Roman Gau, Project Manager
Mike Crosser, TSQAM

FROM: Marcia A. Kuehl

SUBJECT: EPA ARCS Region V Contract No. 68-W8-0093
EPA Work Assignment No. 17-5L4J
Donohue Project No. 20026.024
Himco Dump Site, Elkhart, Indiana

Waste Mass Gas Sampling

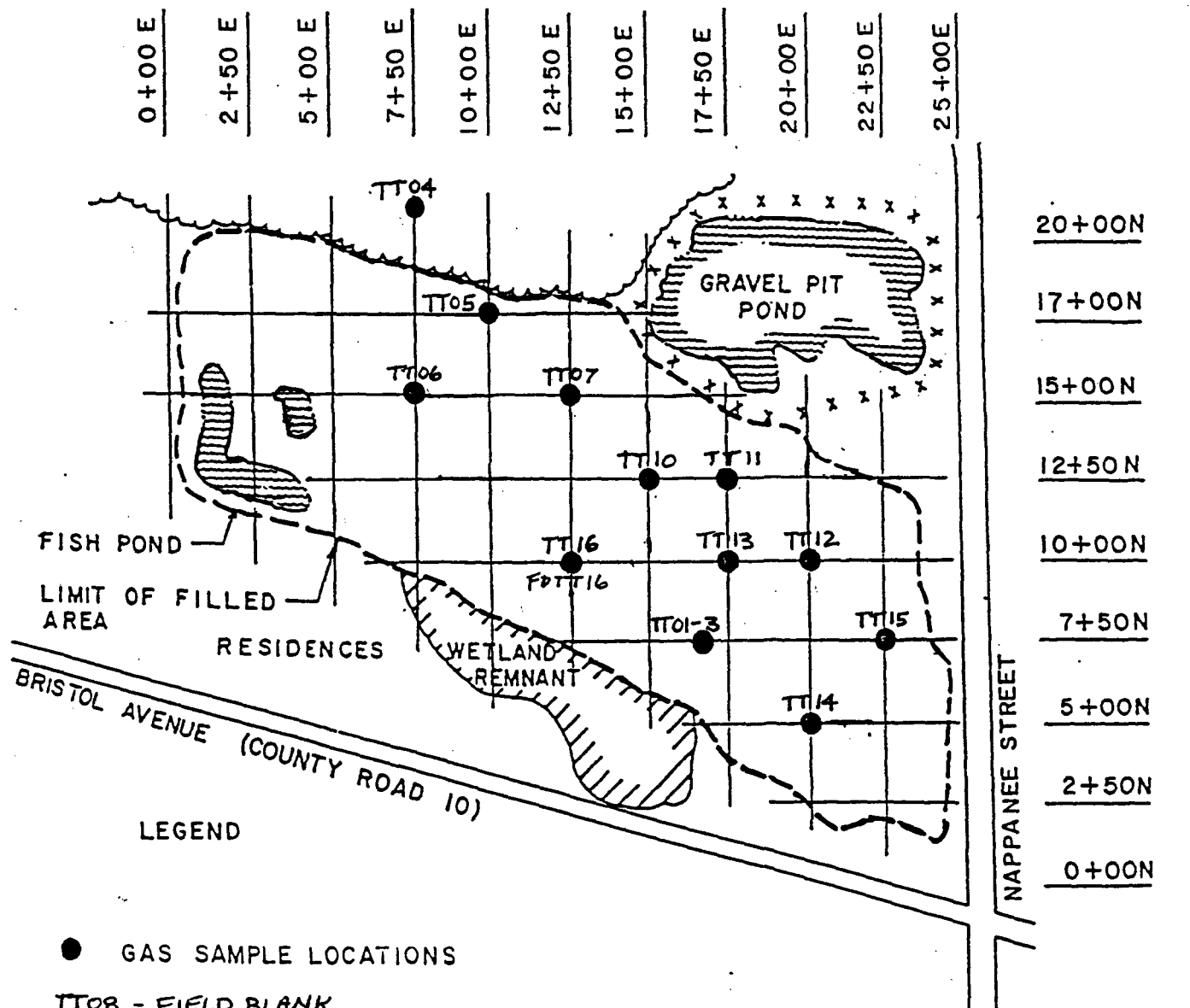
This technical memorandum presents the waste mass gas sampling method and the analytical results from three initial samples which were used to establish sample collection times and pump rates.

Introduction

Characterization of the Himco Dump Site waste mass gas was necessary to select appropriate remedial alternatives and develop the risk assessment. Typical municipal landfill gas consists primarily of methane, carbon dioxide, and a small amount of hydrogen sulfide. If volatile organic solvents have been disposed in the landfill, the gas will also contain volatile organic compounds (VOCs). Historical site groundwater data indicates the presence of acetone, trans-1,2-dichloroethene, chloroethane, chlorofluoromethane, and dichlorodifluoromethane in shallow groundwater. No historical waste mass gas or ambient air data exists for the site. Accordingly, samples were collected and analyzed for the EPA Target Compound List VOCs and up to 10 tentatively identified VOCs.

Twelve cap soil sampling locations, as shown in Figure 1, were selected for waste mass gas collection. These locations were chosen based on the highest field VOC readings, as measured by the HNu, or where the highest methane or hydrogen sulfide ambient concentrations, as measured by the Lumidor Gasponder IV meter, were noted in the 0- to 18-inch soil sample headspace.

Two sampling events were conducted. On November 7, 1990, three samples were collected at location G-20 by Marcia Kuehl and Dorothea Downs (Ebasco) in order to establish pump rates and sample collection times. The collection time and pump rate must be sufficient to collect enough sample volume for analysis yet not saturate the Tenax[®] adsorbent. On November 13 and 14, 1990, the remaining locations were sampled by Marcia Kuehl, Tom Puchalski, and Dorothea Downs. One trip blank, one field blank, one field duplicate, two matrix spikes, and two matrix spike duplicates were also collected on November 13 and 14, 1990, for a total of 18 samples sent for analysis.



SOURCE: US EPA, AUGUST, 1986

0 500 1000
SCALE: FEET
SCALE IS APPROXIMATE

Donohue

WASTE GAS SAMPLING LOCATIONS



20026

1990

FIELD SAMPLING PLAN
HIMCO DUMP SITE
ELKHART, INDIANA

FIGURE 1

Engineers • Architects • Scientists

Methods

The following equipment and materials were used during the waste mass gas sampling:

1. Lumidor Gasponder IV Model PGM-14 (for measurement of methane and hydrogen sulfide).
2. Hollow perforated nickel plated alloy steel soil probe, 10 feet maximum length x 5/8 inch OD.
3. KVA Macho portable soil gas probe system.
4. Gilian Gilair peristaltic sampling pump.
5. Digital soap bubble flow meter - EZ Cal Sensidyne.
6. HNu photoionization detector.
7. Stop watch.
8. Teflon tubing.
9. Tenax/charcoal sorbent tubes (supplied by CLP SAS lab).
10. Tenax sorbent tubes (supplied by CLP SAS lab).
11. Culture tubes (supplied by CLP SAS lab).
12. Friction-top can with charcoal for packaging.
13. Freezer.
14. Water, deionized and tap.
15. Isopropanol (A.C.S.).
16. Five-gallon pail with cover to contain isopropanol rinses.
17. Liquinox soap.
18. Brushes.
19. EPA Region V sample tags and SMO traffic report labels.
20. Plastic bags.
21. Camera and film.
22. Polyester gloves.
23. Generator (20 amp, 120 volt), gas powered.

The local weather station was called each morning prior to sample collection to get the current temperature, wind speed and direction, humidity, and barometric pressure. Sampling was done when winds were below 10 mph and no rain or snow was present. High winds disperse vapors emanating from the borehole, and moisture in the tenax and charcoal sorbents interfere with the chemical analysis.

The pump and a dummy sorbent tube assembly was calibrated daily prior to sample collection with the EZ Cal Sensidyne digital soap bubble flow meter using seven readings. Multiple readings are recommended by the flow meter calibrator manufacturer due to the inherent variability of the bubbles generated. The mean value of readings was used as the actual pump rate because the pump rotameter reading scale was not readable to within 0.10 liters/minute.

The KVA Macho® System 13-pound air rotary hammer, powered by a gas powered generator, was used to drive the stainless steel probe into the ground. A 3-foot sampling interval was attempted at each location. Gas inlets were at the bottom 3 inches of the probe. Refusal occurred prior to 3 feet at some locations due to the presence of waste and/or compacted calcium sulfate. The borehole with the probe inserted was allowed to equilibrate for 15 minutes prior to sample collection.

The SAS laboratory prepared and preanalyzed the sorbent tubes prior to sample collection. Results of the analysis are contained in Attachment A. Acceptable levels of volatile organics with boiling points less than 110°C (acetone, benzene, hexane, tetrachloroethylene, and toluene) were reported. Amounts detected were 0.4 to 12.9 ng per pair of tubes which was not of sufficient magnitude to prevent accurate determination of the sample components expected. It should be noted that the compound levels reported for the preanalysis verify that the sorbent tubes are purged of these compounds and are considered "clean" for subsequent sample collection.

The sorbent tubes were contained in sealed culture tubes, removed from the freezer, and opened only just before actual sample collection. The sorbent tubes were handled with polyester-gloved hands and did not contact any other surfaces. It was important to keep the sorbent tubes themselves free from fingerprints and dust as the tubes are placed directly in the desorption unit for analysis at the lab.

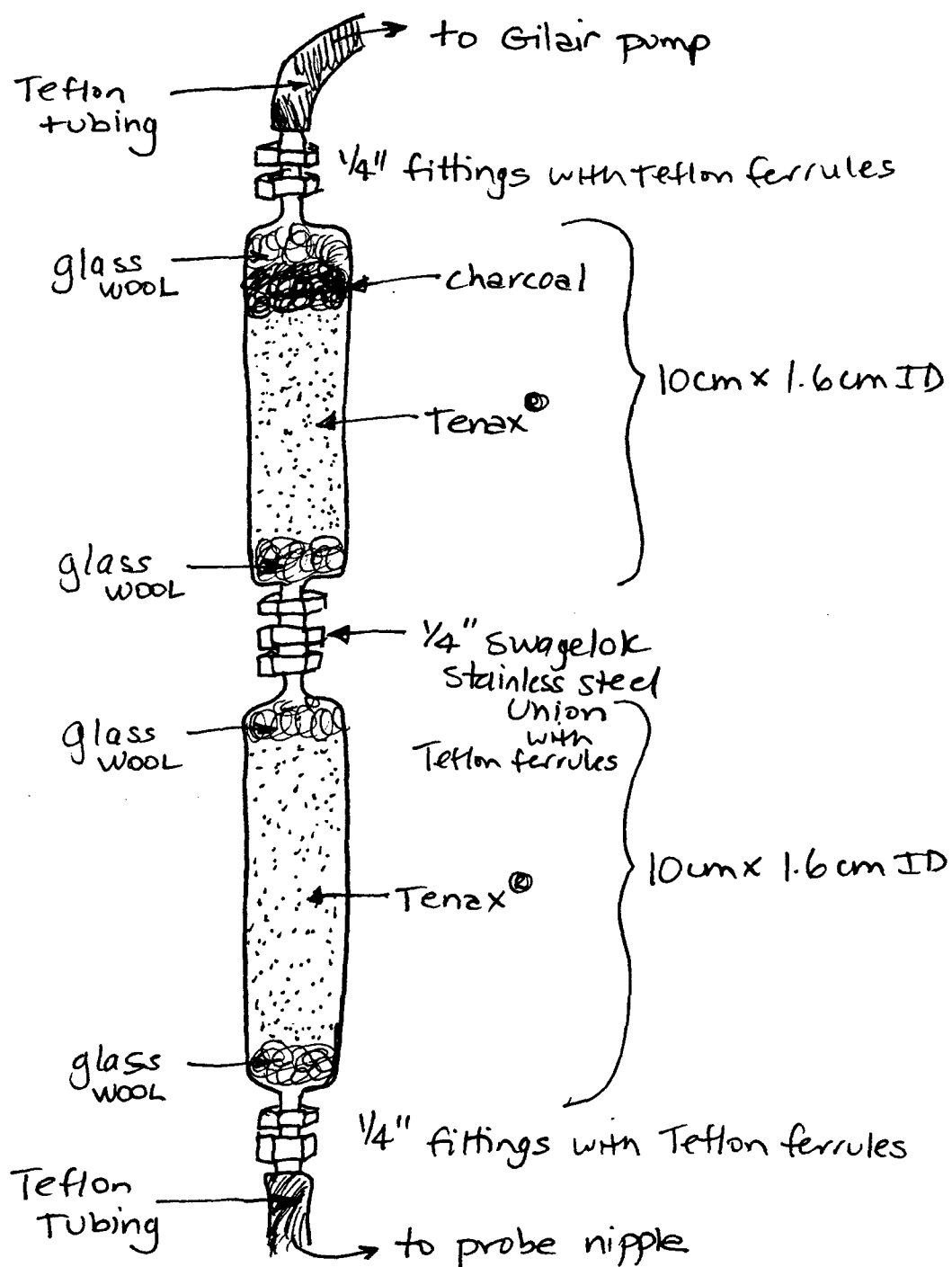
Figure 2 presents the sampling train used in the field. Teflon tubing was connected from the probe nipple to the end of the sorbent tube assembly. The sorbent tube assembly consisted of the tenax tube and then the tenax/charcoal tube connected in series using teflon ferrules and stainless steel Swagelok® fittings. The tube assembly was connected to the Gilian/Gilair precalibrated pump using teflon tubing.

After the pump was started, the start time, rotameter reading, sorbent tube numbers, and collection conditions were recorded on the Soil Gas Survey Form (Attachment B). At the end of the sampling period, the flow rate was checked using the rotameter and recorded on the Soil Gas Survey Form (Attachment B). The flows at the beginning and end of all sampling periods did not vary by more than 10 percent, so all tubes used were considered valid samples. The end time was then recorded, and the sorbent tube assembly disconnected with polyester-gloved hands, replaced in the culture tubes, and the tubes labeled with EPA tags and SAS labels. The culture tubes were sealed in a paint can containing a layer of charcoal on the bottom and packaged with ice for next day shipment to IT Corporation laboratory, Cincinnati, Ohio.

Decontamination of the steel soil probe was done between borings using liquinox and tap water wash, followed by a tap water rinse, an isopropanol rinse, and two rinses with deionized water. The sampling pump was decontaminated by pumping several liters of ambient air through it. Decontamination rinses containing isopropanol were containerized for eventual discharge to the municipal wastewater treatment system.

FIGURE 2
SAMPLING TRAIN
HIMCO DUMP

I/I DESIGN



The total volumetric flow for each cartridge was calculated and recorded on the Soil Gas Survey Form using the following equation:

$$V_m = \frac{T \times Q_A}{1000}$$

where:

V_m = Total volume sampled in liters at measured temperature and pressure

Q_A = Flow rate in ml/minute

T = Sampling time = $T_2 - T_1$, minutes

T_2 = Stop time

T_1 = Start time

The total volume (V_S) at standard conditions, 25°C and 760 mmHg, was then calculated from the following equation and included on the chain-of-custody form so the lab could report results in ng/l.

$$V_S = V_m \times \frac{P_A}{760} \times \frac{298}{273 + t_A}$$

where:

P_A = Average barometric pressure, mmHg

t_A = Average ambient temperature, °C

Summary of Results

Samples as listed in Table TM12-1 were collected. Field trial sample analytical results are in Attachment C and detected compounds are summarized in Table TM12-2. No Time Weighted Averages (TWA) were exceeded.

Compounds detected were 1,1,2-trichloro-, 1,2,2-trifluoroethane, methylene chloride, acetone, benzene, toluene, 1,1,1-trichloroethane, and carbon disulfide.

Deviations

The following deviations from the Field Sampling Plan occurred, but were not judged by the Site QC officer and Site Manager as negatively impacting data quality:

1. Borehole equilibration was done for 15 minutes rather than the 5 minutes specified in the FSP. The time was extended after evaluation of the data collected on November 7, 1990, which indicated that the greatest concentration of 1,1,2-trichloro - 1,2,2-trifluoroethane was measured in the sample collected after the borehole was open for 15 minutes.

2. The initial sampling rate specified in the FSP was 1 liter/min for 20 minutes. Based on conversations with other ARCS contractors familiar with use of the VOST sorbent tube assembly for gas sampling and the analytical laboratory, a rate of approximately 4 liters/minute was selected. Sampling times of 16.87 minutes, 12.18 minutes, and 5.00 minutes were used on November 7, 1990, during the field trial. Based on these results, a sample volume (V_s) of approximately 2 liters was selected using a pump flow rate of approximately 4 liters/minute for 10 minutes, and the bore-hole was left open to equilibrate for 15 minutes after probe insertion. Remaining samples, HDTT04-HDTT07, HDTT10-HHFDTT16, were collected using these operating parameters.
3. The FSP indicated that two sampling locations were to be sampled during the field trial. Only one location was sampled as the weather was threatening, and rain was expected.
4. The Corporate Health and Safety Manager reviewed the sampling and documentation during the initial field trial.
5. A bottle blank, as specified by the FSP, was not collected. A field blank consisting of a pair of sorbent tubes uncapped and exposed to site ambient air for the sampling period (10 minutes) was collected based on advice from the CLP laboratory and other ARCS contractors.
6. Two sets of matrix spike and matrix spike duplicate sorbent tubes were collected and consisted of four sets of unexposed tubes. These samples were added as the SAS method specified this QC requirement at a frequency of 1 per 10 field samples.
7. Refusal occurred during sampling due to the 3-foot sample interval could not be achieved for all samples, as indicated in Table TM12-1.

A/R/HIMCO/AAS

TABLE TM12-1

VOLATILE MASS GAS SAMPLES COLLECTED
Himco Dump Site
Elkhart, Indiana

<u>Grid Point Location</u>	<u>Borehole equil. time (min.)</u>	<u>Sample Number</u>	<u>Sample Depth (ft.)</u>	<u>Mean Pump Flow Rate L/min.</u>	<u>Sample Time (min.)</u>	<u>Total Volumetric Flow (V_m) (liters)</u>
G-20	5	HD-TT01	0.75	4.21	16.87	71.0
G-20	17	HD-TT02	0.75	4.21	12.18	51.3
G-20	30	HD-TT03	0.75	4.21	5.00	21.0
OFF-SITE	15	HD-TT04	3.0	4.17	10.00	41.7
R-12	15	HD-TT05	2.4	4.17	10.00	41.7
Q-8	15	HD-TT06	2.7	4.17	10.00	41.7
O-15	15	HD-TT07	3.0	4.17	10.00	41.7
FIELD BLANK	--	HD-FBTT08	0	--	10.00	--
TRIP BLANK	--	HD-TBTT09	--	--	--	--
L-18	15	HD-TT10	2.0	4.17	10.00	41.7
L-21	15	HD-TT11	2.6	4.17	10.00	41.7
I-22	15	HD-TT12	3.0	4.17	10.00	41.7
D-24	15	HD-TT14	3.0	4.17	10.00	41.7
F-25	15	HD-TT15	3.0	4.17	10.00	41.7
K-14	15	HD-TT16	3.0	4.17	10.00	41.7
K-14	15	HD-FDTT16	3.0	4.17	10.00	41.7
Matrix Spike	--	HD-TTMS01	--	--	--	--
Matrix Spike	--	HD-TTMS02	--	--	--	--
Matrix Spike	--	HD-TTMSD01	--	--	--	--
Duplicate						
Matrix Spike	--	HD-TTMSD02	--	--	--	--
Duplicate						

A/R/HIMCO/AA5

TABLE TM12-2

WASTE MASS GAS FIELD TRIAL ANALYTICAL RESULTS
Himco Dump Site
Elkhart, Indiana

<u>Detected Volatile Organic</u>	<u>HD-TT01</u> <u>ng/L</u>	<u>HD-TT02</u> <u>ng/L</u>	<u>HD-TT03</u> <u>ng/L</u>	<u>TWA</u> <u>ng/L</u>
Methylene Chloride	2.66 B	7.83 B	14.6	350,000
Acetone	5.31	8.29	17.9	1,780,000
Benzene	0.66 J	1.84	2.25	30,000
Toluene	23.9	30.9	21.3	375,000
1,1,2-Trichloroethane-	19.9	138	225	NE
1,2,2-Trifluoroethane				
Unknown Hydrocarbon (RT 11.26)	3.32	9.22	ND	NE
Carbon Disulfide	ND	3.22	ND	30,000
1,1,1-Trichloroethane	ND	2.30	ND	1,900,000
Unknown Hydrocarbon (RT 16.22)	ND	3.69	ND	NE

Legend:

B - Detected in unexposed lab blank tubes.

J - Estimated concentration, below detection limit.

ND - Not detected.

RT - Retention Time, in units.

TWA = Time Weighted Average for normal 8-hour workday. and a 40-hour workweek.

NE = Not Established.

A/R/HIMCO/AA5

ATTACHMENT A

VOST BLANK CHECK RESULTS

VOST Blank Check Results
ITAS
Cincinnati

Client I.D. USEPA - VIAR

W.O. # X0-10-293

Date	Analyst	Tube No.s	Batch	Acetone	Benzene	Hexane	Perc	Toluene	Donohue #	SITE		Unknown (1)	Can No.
10/24	VR	T4161 Tc 1555	301	—	1.3	—	9.0	0.8	TT10	L-18		<5ng	1
		T3262 Tc 35		3.3	1.9	1.0	12.0	0.7	TT12	I-22			
		T14 Tc x 4241		6.0	3.9	0.5	11.4	0.9	TT09	TB			
		T60 Tc 4640		4.5	2.2	1.3	12.9	0.8	TT08	FB	Tube say 4648		
		TT-100 Tc 47		5.3	3.0	1.1	10.0	0.9	TT05	R-12			
		T2154 Tc 4602		6.1	2.1	1.5	7.7	0.6	TT04	UPWIND			
10/26		T4721 Tc 4752	302	—	0.8	—	—	—					
		T4488 Tc 4741		1.4	1.9	1.3	4.2	0.7	TT06	Q-8			
		T4211 Tc 4754		7.3	2.3	4.0	8.2	0.9	TT11	L-21			
		T3907 Tc 4744		1.0	1.3	1.4	4.5	0.6	TT07	O-15			
		T4717 Tc 4484		2.6	1.3	1.6	3.0	0.5	M501				2
		T4673 Tc 4735		—	1.1	0.5	3.7	0.4	M5001				
		T4694 Tc 4141		1.1	0.9	0.8	0.8	0.5	M5002				
		T4727 Tc 4126		2.5	1.5	0.9	—	—	TT16	F-14			
		T4698 Tc 4742		—	1.4	1.2	—	0.6	F0TT16	F-14			
		T4713 Tc 4748		2.6	1.0	1.2	—	0.4					
		T4716 Tc 4648		6.8	2.2	0.6	9.7	0.5	TT14	D-24			
10/28		T4715 Tc 3148		8.8	3.3	0.6	—	0.7	M502				
		T42 Tc 3182		6.0	1.9	1.1	—	0.5	TT15	F-25			
		T4670 Tc 4538		5.1	1.4	2.4	—	—					
		T4723 Tc 3619		7.6	1.5	0.8	—	0.6	TT13	I-21			

(1) based on benzene response factor for the largest unknown peak in run. All targets are listed as NG per pair.

ATTACHMENT B
SOIL GAS SURVEY FORMS

SOIL GAS SURVEY FORM

CLIENT: EPA ARCS DATE: 11/7/90 EPA SAS NO.: 5798 E-1/E-2
SITE: Hmco DONOHUE SPL NO.: HDIT01
PROJECT NO.: 20026
SAMPLING TEAM: Marcia Kuehl, Dorothea Downs

SAMPLING CONDITIONS

TEMPERATURE: 40 °F - 32 x 5/9 = 4.4 °C (1A) Gastech 6X86 (cal 11/7/90)
BAROMETRIC PRESSURE (PA): 30.05 mm Hg at 0800 (AM/PM) H2S: 0 ppm
RELATIVE HUMIDITY: 92 % CH4: 0 % LEL
WIND: 5-10 mph from SW
WEATHER: cloudy, sleet

SAMPLE GRID COORDINATES.: _____ N _____ E Grid point G-20 near
SAMPLING INTERVAL: 18-24" fr frac tank
SOIL CONDITIONS AT SURFACE: wet, moss growing on soil

PUMP CALIBRATION

PUMP MFG/MODEL/SN: Giljan SN2961 (Gilair) cal readings
CALIBRATOR MFG/MODEL/SN: E2cal/sensidyne 1251222 4.208 4.208 4.208
INITIAL CALIBRATION (QA) TO 4.2057 (n=7) L/MIN AT TIME: 0900 4.208 4.198
CALIBRATION VERIFICATION: 4.21 4.218 4.208
ROTAMETER READING 4.0 L/min TIME: 0900 4.208
ROTAMETER READING 4.0 L/min TIME: 1330
% DIFFERENCE 0

*IF > 10%, SAMPLE TUBES SUSPECT, RESAMPLE

SAMPLE COLLECTION

TENAX ✓
CHARCOAL TUBE NUMBER: TC4490 E-1 max CHARCOAL TENAX TUBE NUMBER: T4629 E-2
STOP TIME: 11:53:52 COLLECTION CONDITIONS: driving ~ 3"
START TIME: 11:37:00 refusal at 18", calcium sulfate
TIME ELAPSED (T) 16:57 sec MINUTES underneath refusal at 18"
16:37 min

TOTAL VOLUMETRIC FLOW CALCULATION

$$V_m = T \times QA = \frac{16.87}{760} \times \frac{4.21}{273 + 1A} = \frac{71.02}{760} \text{ LITERS (V}_m\text{)}$$

$$V_s = V_m \times PA = \frac{71.02}{273 + 1A} \times \frac{298}{4.4} = 3.01 \text{ LITERS (V}_s\text{)}$$

*RECORD Vs IN LITERS ON SAS CHAIN OF CUSTODY REMARKS COLUMN.

SOIL GAS SURVEY FORM

CLIENT: EPA ARCS DATE: 11/7/90 EPA SAS NO.: 5798E-3/E-4
SITE: Himco DONOHUE SPL NO.: HD7T02
PROJECT NO.: 20026
SAMPLING TEAM: Marcia Kuehl Dorothea Downs

SAMPLING CONDITIONS

See 11/7/90,

TEMPERATURE: _____ °F - 32 x 5/9 = _____ °C (tA) HNu: _____ ppm
BAROMETRIC PRESSURE (PA): _____ mm Hg at _____ AM/PM H₂S: _____ ppm
RELATIVE HUMIDITY: _____ % CH₄: _____ % LEL
WIND: _____ mph from _____
WEATHER: _____

SAMPLE GRID COORDINATES: _____ N _____ E *Same borehole as T101*
SAMPLING INTERVAL: _____ ft
SOIL CONDITIONS AT SURFACE: _____

PUMP CALIBRATION

See 11/7/90

PUMP MFG/MODEL/SN: _____
CALIBRATOR MFG/MODEL/SN: _____ *T101*
INITIAL CALIBRATION (QA) TO _____ L/MIN AT TIME: _____
CALIBRATION VERIFICATION: ROTAMETER READING _____ TIME: _____
*IF > 10%, SAMPLE ROTAMETER READING _____ TIME: _____
TUBES SUSPECT, RESAMPLE % DIFFERENCE _____

SAMPLE COLLECTION

TENAX
CHARCOAL TUBE NUMBER: TC 4475 E-3 *with* CHARCOAL TENAX TUBE NUMBER: T 2322 E-4
STOP TIME: 12:19:25 COLLECTION CONDITIONS: _____
START TIME: 12:07:14
TIME ELAPSED (T) 12:11 sec MINUTES _____
12:18 min

TOTAL VOLUMETRIC FLOW CALCULATION

$$V_m = T \times QA = \frac{12.18}{4.21} \times \frac{51.28}{4.206} = 57.33 \text{ LITERS (V}_m\text{)}$$

$$V_s = V_m \times \frac{PA}{760} \times \frac{298}{273 + tA} = \frac{2.17}{4.4} \text{ LITERS (V}_s\text{)*}$$

*RECORD V_s IN LITERS ON SAS CHAIN OF CUSTODY REMARKS COLUMN.

SOIL GAS SURVEY FORM

CLIENT: EPA ARCS DATE: 11/7/90 EPA SAS NO.: 5748E-5/E-6
 SITE: Hinco DONOHUE SPL NO.: HD T103
 PROJECT NO.: 20026
 SAMPLING TEAM: Marcia Kerch Dorothea Downs

SAMPLING CONDITIONS

see 11/7/90 T101

TEMPERATURE: _____ °F - 32 x 5/9 = _____ °C (tA)
 BAROMETRIC PRESSURE (PA): _____ mm Hg at _____ AM/PM
 RELATIVE HUMIDITY: _____ %
 WIND: _____ mph from _____
 WEATHER: _____
 SAMPLE GRID COORDINATES: _____ N _____ E
 SAMPLING INTERVAL: _____ ft
 SOIL CONDITIONS AT SURFACE: _____

HNu: _____ ppm
 H₂S: _____ ppm
 CH₄: _____ % LEL

PUMP CALIBRATION

see 11/7/90 T101

PUMP MFG/MODEL/SN: _____
 CALIBRATOR MFG/MODEL/SN: _____
 INITIAL CALIBRATION (QA) TO _____ L/MIN AT TIME: _____
 CALIBRATION VERIFICATION: ROTAMETER READING _____ TIME: _____
 IF > 10%, SAMPLE ROTAMETER READING _____ TIME: _____
 TUBES SUSPECT, RESAMPLE % DIFFERENCE _____

SAMPLE COLLECTION

E-5 TENAX + CHARCOAL TUBE NUMBER: TC 438 E-6 CHARCOAL TENAX TUBE NUMBER: T 4131
 STOP TIME: 12:28:23 COLLECTION CONDITIONS: see 11/7/90 T101
 START TIME: 12:23:23
 TIME ELAPSED (T) 5.00 MINUTES

TOTAL VOLUMETRIC FLOW CALCULATION

$$V_m = T \times Q_A = \frac{5.00}{1} \times \frac{4.21}{1} = 21.05 \text{ LITERS (V}_m\text{)}$$

$$V_s = V_m \times \frac{PA}{760} \times \frac{298}{273 + t_A} = \frac{21.05}{1} \times \frac{298}{273 + 4.4} = 0.89 \text{ LITERS (V}_s\text{)*}$$

*RECORD V_s IN LITERS ON SAS CHAIN OF CUSTODY REMARKS COLUMN.

SOIL GAS SURVEY FORM

0900 Am

CLIENT: EPA ARCS DATE: 11/13/90 EPA SAS NO.: 5798E ^{E-12, E-1} ~~E-7, E-8~~
SITE: Himco DONOHUE SPL NO.: HD104
PROJECT NO.: 20026 ^{UPWIND OFFSITE}
SAMPLING TEAM: M. Kuchl / D. Downs / T. Puchalski

SAMPLING CONDITIONS

TEMPERATURE: 25 °F - 32 x 5/9 = °C (tA) HNu: 0 ppm
BAROMETRIC PRESSURE (PA): 30.23 mm Hg at 0715 ^(AM)PM H₂S: 0 ppm
RELATIVE HUMIDITY: 92 % CH₄: 0 % LEL
WIND: 0 mph from N-NE ^{max}
WEATHER: sunny

SAMPLE GRID COORDINATES: 50' N of S-10E ^{max}
SAMPLING INTERVAL: 3.0 ft
SOIL CONDITIONS AT SURFACE: frosty, leaves moist (in woods)

PUMP CALIBRATION

PUMP MFG/MODEL/SN: Gilian/Gilair / 2196 ^{cal reading: 4.211 4.028}
CALIBRATOR MFG/MODEL/SN: Ecal Sensidyne / 251222 ^{(L/min) 4.181 4.218}
INITIAL CALIBRATION (QA) TO $\bar{x} = 4.17$ (n=7) L/MIN AT TIME: 0530 ^{4.226 4.15}
CALIBRATION VERIFICATION: ROTAMETER READING 4.4/min TIME: 0950
*IF > 10%, SAMPLE ROTAMETER READING 4.4/min TIME: 0915
TUBES SUSPECT, RESAMPLE % DIFFERENCE 0 *

SAMPLE COLLECTION

TENAX + ^{E-12} ~~E-7~~ ^{turn} CHARCOAL TUBE NUMBER: TC4602 ^{max} ~~E-8~~ ^{turn} CHARCOAL/TENAX TUBE NUMBER: T2154
STOP TIME: used stopwatch COLLECTION CONDITIONS: may have hit
START TIME: water table, suction created at
TIME ELAPSED (T) 10.00.06 MINUTES T = 2min

TOTAL VOLUMETRIC FLOW CALCULATION

$$V_m = T \times QA = \frac{10.00}{760} \times \frac{4.17}{273 + tA} = 41.7 \text{ LITERS (V}_m\text{)}$$

$$V_s = V_m \times \frac{PA}{273 + tA} = \frac{298}{273 + tA} = 1.34 \text{ LITERS (V}_s\text{)*}$$

*RECORD V_s IN LITERS ON SAS CHAIN OF CUSTODY REMARKS COLUMN.

SOIL GAS SURVEY FORM

10:45 AM

CLIENT: EPA ARCS DATE: 11/13/90 EPA SAS NO.: 5798E
SITE: Hmco DONOHUE SPL NO.: TT05 ~~E-14, E-15~~
PROJECT NO.: 20026
SAMPLING TEAM: M Kuenl / D Downs / Tom Puchalski

SAMPLING CONDITIONS

TEMPERATURE: 25 °F - 32 x 5/9 = °C (1A) HNu: 0 ppm
BAROMETRIC PRESSURE (PA): 30.23 mm Hg at 0715 (AM/PM) H₂S: 0 ppm
RELATIVE HUMIDITY: 92 % CH₄: 0 % LEL
WIND: 0 mph from
WEATHER: Sunny

SAMPLE GRID COORDINATES: N E R-12
SAMPLING INTERVAL: 2'5" ft, refusal
SOIL CONDITIONS AT SURFACE: visible CaSO₄ sand H₂S odor ambient

PUMP CALIBRATION

PUMP MFG/MODEL/SN: Gilman/Gilair/2196 *see also TT04 for cal. readings*
CALIBRATOR MFG/MODEL/SN: E2 Cal Sensidyne/251222
INITIAL CALIBRATION (QA) TO X = 4.17 (n=7) L/MIN AT TIME: 0530
CALIBRATION VERIFICATION: ROTAMETER READING 4.04 L/MIN TIME: 10:30
ROTAMETER READING 4.04 L/MIN TIME: 11:05
*IF > 10%, SAMPLE TUBES SUSPECT, RESAMPLE % DIFFERENCE 0 %

SAMPLE COLLECTION

E-14 *E-15* *used* *made to E-15*
CHARCOAL TUBE NUMBER: TC47 CHARCOAL/TENAX TUBE NUMBER: TT100
STOP TIME: used 10:55 COLLECTION CONDITIONS: Vacuum created at T=2 min
START TIME: stopwatch 10:45 am CaSO₄ with yellow labels subsurface
TIME ELAPSED (T) 10:00:00 MINUTES

TOTAL VOLUMETRIC FLOW CALCULATION

$$V_m = T \times Q_A = \frac{10.00}{1} \times \frac{4.17}{1} = 41.7 \text{ LITERS (V}_m\text{)}$$

$$V_s = V_m \times \frac{PA}{760} \times \frac{298}{273 + 1A} = \frac{1.34}{1} \text{ LITERS (V}_s\text{)*}$$

*RECORD V_s IN LITERS ON SAS CHAIN OF CUSTODY REMARKS COLUMN.

SOIL GAS SURVEY FORM

11:50 AM

CLIENT: EPA ARCS DATE: 11/13/90 EPA SAS NO.: 5798E ^{E-16, E-17} ~~E-11, E-12~~
SITE: Hmco DONOHUE SPL NO.: HD1106
PROJECT NO.: 20026
SAMPLING TEAM: M. Kuehl / D. Downs / T. Puchalski

SAMPLING CONDITIONS

TEMPERATURE: 25 °F - 32 x 5/9 = °C (tA) HNu: 0 ppm
BAROMETRIC PRESSURE (PA): 30.23 mm Hg at 0715 AM/PM H₂S: 0 ppm
RELATIVE HUMIDITY: 92 % CH₄: 0 % LEL
WIND: 0 mph from
WEATHER: Sunny

SAMPLE GRID COORDINATES: N E QB
SAMPLING INTERVAL: 2' 8" ft
SOIL CONDITIONS AT SURFACE: grassy

PUMP CALIBRATION

See also T104 for cal. readings

PUMP MFG/MODEL/SN: Gilian / Gilair / 2196
CALIBRATOR MFG/MODEL/SN: E2Cal / Sensidyne / 251222
INITIAL CALIBRATION (QA) TO X=4.17 (n=7) L/MIN AT TIME: 0530
CALIBRATION VERIFICATION: ROTAMETER READING 4.0 TIME: 11:32
ROTAMETER READING 4.0 TIME: 12:05
*IF > 10%, SAMPLE TUBES SUSPECT, RESAMPLE % DIFFERENCE 0

SAMPLE COLLECTION

^{E-11} TENAX + CHARCOAL TUBE NUMBER: TC4741 ^{E-12} CHARCOAL TENAX TUBE NUMBER: T4488
STOP TIME: 12:00 COLLECTION CONDITIONS:
START TIME: 11:50
TIME ELAPSED (T) 10.00.00 MINUTES

TOTAL VOLUMETRIC FLOW CALCULATION

$$V_m = T \times Q_A = 10.00 \times 4.17 = 41.7 \text{ LITERS (V}_m\text{)}$$

$$V_s = V_m \times \frac{PA}{760} \times \frac{298}{273 + tA} = 1.84 \text{ LITERS (V}_s\text{)*}$$

*RECORD V_s IN LITERS ON SAS CHAIN OF CUSTODY REMARKS COLUMN.

SOIL GAS SURVEY FORM

TIME: 11:45 AM 1/10/90

CLIENT: EPA ARCS DATE: 11/13/90 EPA SAS NO.: 5798E E18, E19
SITE: Hmco DONOHUE SPL NO.: HD TT07
PROJECT NO.: 20026
SAMPLING TEAM: M. Kuehl / D. Downs / T. Puchalski

SAMPLING CONDITIONS

TEMPERATURE: 40 °F - 32 x 5/9 = 4.4 °C (1A) HNu: 0 ppm
BAROMETRIC PRESSURE (PA): 30.23 mm Hg at 12:15 AM 12:15 PM H₂S: 0 ppm
RELATIVE HUMIDITY: % CH₄: 0 % LEL
WIND: 0 mph from
WEATHER: Sunny

SAMPLE GRID COORDINATES: N E 0-15
SAMPLING INTERVAL: 3.0 ft
SOIL CONDITIONS AT SURFACE: H₂S odor - intermittent ambient moist, moss

PUMP CALIBRATION

PUMP MFG/MODEL/SN: Gilian / Gilair / 2196
CALIBRATOR MFG/MODEL/SN: EZ cal / sensidyne / 1251222
INITIAL CALIBRATION (QA) TO X = 4.17 (n=7) L/MIN AT TIME: 0530
CALIBRATION VERIFICATION: ROTAMETER READING 4.0 TIME: 1340
ROTAMETER READING 4.0 TIME: 1510
*IF > 10%, SAMPLE TUBES SUSPECT, RESAMPLE % DIFFERENCE 0

SAMPLE COLLECTION

E-18 TENAX 4 CHARCOAL TUBE NUMBER: TC 4744 E-19 CHARCOAL/TENAX TUBE NUMBER: T3907
STOP TIME: used COLLECTION CONDITIONS: vacuum created at T=1min
START TIME: stop watch took field blank at this location
TIME ELAPSED (T) 10.00.00 MINUTES

TOTAL VOLUMETRIC FLOW CALCULATION

$$V_m = T \times QA = \frac{10.00}{60} \times 4.17 = \text{LITERS (V}_m\text{)}$$

$$V_s = V_m \times \frac{PA}{760} \times \frac{298}{273 + tA} = 1.75 \text{ LITERS (V}_s\text{)*}$$

*RECORD V_s IN LITERS ON SAS CHAIN OF CUSTODY REMARKS COLUMN.

SOIL GAS SURVEY FORM

1405

CLIENT: EPA ARCS DATE: 11/13/90 EPA SAS NO.: 5798E / E-20, E-21
 SITE: Himco DONOHUE SPL NO.: HD TT08
 PROJECT NO.: 20026 Field Blank
 SAMPLING TEAM: M. Kuehl / D. Downs / T. Puchalski

SAMPLING CONDITIONS

TEMPERATURE: 48 °F - 32 x 5/9 = _____ °C (tA) HNu: 0 ppm
 BAROMETRIC PRESSURE (PA): 30.23 mm Hg at 1215 AM/PM H₂S: 0 ppm
 RELATIVE HUMIDITY: _____ % CH₄: 0 % LEL
 WIND: 0 mph from _____
 WEATHER: Sunny

SAMPLE GRID COORDINATES: _____ N _____ E taken at TT07
 SAMPLING INTERVAL: 0 ft ambient air only
 SOIL CONDITIONS AT SURFACE: NA

PUMP CALIBRATION

pump not used

PUMP MFG/MODEL/SN: _____
 CALIBRATOR MFG/MODEL/SN: _____
 INITIAL CALIBRATION (QA) TO _____ L/MIN AT TIME: _____
 CALIBRATION VERIFICATION: ROTAMETER READING _____ TIME: _____
 *IF > 10%, SAMPLE ROTAMETER READING _____ TIME: _____
 TUBES SUSPECT, RESAMPLE % DIFFERENCE _____

SAMPLE COLLECTION

E-20 TENAX & CHARCOAL TUBE NUMBER: TC 46480
 STOP TIME: used stopwatch COLLECTION CONDITIONS: _____
 START TIME: _____ opened end caps for 10 minutes
 TIME ELAPSED (T) 10.00 MINUTES recapped at location TT07

TOTAL VOLUMETRIC FLOW CALCULATION

$$V_m = T \times Q_A = \frac{NA}{4.17} \times \frac{NA}{70.00} = \text{LITERS (V}_m\text{)}$$

$$V_s = V_m \times \frac{PA}{760} \times \frac{298}{273 + tA} = \text{LITERS (V}_s\text{)}$$

not applicable

*RECORD V_s IN LITERS ON SAS CHAIN OF CUSTODY REMARKS COLUMN.

SOIL GAS SURVEY FORM

no time
QC

CLIENT: EPA ARCS DATE: 11/13/90 EPA SAS NO.: 5798E-22, E-23
SITE: Hmco DONOHUE SPL NO.: HD/T109
PROJECT NO.: 20026 TRIP BLANK
SAMPLING TEAM: M. Kuehl / D. Downs / T. Puchalski

SAMPLING CONDITIONS

TEMPERATURE: 48 °F - 32 x 5/9 = _____ °C (ta) HNu: 0 ppm
BAROMETRIC PRESSURE (PA): 30.23 mm Hg at 1215 AM/PM H₂S: 0 ppm
RELATIVE HUMIDITY: 92 % CH₄: 0 % LEL
WIND: 0 mph from _____
WEATHER: sunny

SAMPLE GRID COORDINATES: _____ N _____ E not applicable
SAMPLING INTERVAL: _____ ft
SOIL CONDITIONS AT SURFACE: _____

PUMP CALIBRATION

~~PUMP MFG/MODEL/SN: _____~~ not applicable
~~CALIBRATOR MFG/MODEL/SN: _____~~
~~INITIAL CALIBRATION (QA) TO _____ L/MIN AT TIME: _____~~
~~CALIBRATION VERIFICATION: _____~~
~~*IF > 10%, SAMPLE ROTAMETER READING _____ TIME: _____~~
~~TUBES SUSPECT, RESAMPLE ROTAMETER READING _____ TIME: _____~~
~~% DIFFERENCE _____~~

SAMPLE COLLECTION

E-22 TENAX CHARCOAL TUBE NUMBER: TCLX4241 E-23 CHARCOAL/TENAX TUBE NUMBER: T14
STOP TIME: _____ COLLECTION CONDITIONS: UNOPENED
START TIME: _____ ACCOMPANIED CAN 1 TUBES W/ TEN
TIME ELAPSED (T) NOT APPLICABLE MINUTES SHIPPED FROM LAB

TOTAL VOLUMETRIC FLOW CALCULATION

~~$V_m = T \times QA = \text{_____} \times \text{_____} = \text{LITERS (V}_m\text{)}$~~
 ~~$V_s = V_m \times \frac{PA}{760} \times \frac{298}{273 + t_A} = \text{LITERS (V}_s\text{)}$~~ not applicable

*RECORD V_s IN LITERS ON SAS CHAIN OF CUSTODY REMARKS COLUMN

SOIL GAS SURVEY FORM

1450

CLIENT: EPA ARCS DATE: 11/13/90 EPA SAS NO.: 5798E E-24, E-25
SITE: Hrmco DONOHUE SPL NO.: HDTT-10
PROJECT NO.: 20026
SAMPLING TEAM: M Kuehl/D. Downs/T Puchalski

SAMPLING CONDITIONS

TEMPERATURE: 28 °F - 32 x 5/9 = °C (1A) HNU: 0 ppm
BAROMETRIC PRESSURE (PA): 30.23 mm Hg at 1215 AM/PM H₂S: 0 ppm
RELATIVE HUMIDITY: 92 % CH₄: 0 % LEL
WIND: 0 mph from
WEATHER: Sunny

SAMPLE GRID COORDINATES: N E L-13

SAMPLING INTERVAL: 2.00 ft

SOIL CONDITIONS AT SURFACE: Sandy, visible CaSO₄

PUMP CALIBRATION

PUMP MFG/MODEL/SN: Gilian/Gilgir 12196
CALIBRATOR MFG/MODEL/SN: ELCAL/Sensidyne/251222
INITIAL CALIBRATION (QA) TO X=4.17 (n=7) L/MIN AT TIME: 0530
CALIBRATION VERIFICATION: ROTAMETER READING 4.0 TIME: 1440
ROTAMETER READING 4.0 TIME: 1505
*IF > 10%, SAMPLE TUBES SUSPECT, RESAMPLE % DIFFERENCE 0

SAMPLE COLLECTION

E-24 have open 1435 TENAX
CHARCOAL TUBE NUMBER: TC1555
STOP TIME: stopwatch
START TIME: stopwatch
TIME ELAPSED (T) 10.00.00 MINUTES
E-25
CHARCOAL/TENAX TUBE NUMBER: TC161
COLLECTION CONDITIONS: no unusual conditions

TOTAL VOLUMETRIC FLOW CALCULATION

$$V_m = T \times Q_A = \frac{10.00}{4.17} \times 4.17 = 417 \text{ LITERS (V}_m\text{)}$$

$$V_s = V_m \times \frac{PA}{760} \times \frac{298}{273 + 1A} = 417 \times \frac{30.23}{760} \times \frac{298}{273 + 1A} = 1.75 \text{ LITERS (V}_s\text{)*}$$

*RECORD V_s IN LITERS ON SAS CHAIN OF CUSTODY REMARKS COLUMN.

SOIL GAS SURVEY FORM

1525

CLIENT: EPA ARCS DATE: 11/13/90 EPA SAS NO.: 3798E E-26, E-27
SITE: Hmw DONOHUE SPL NO.: HDTI-11
PROJECT NO.: 20026
SAMPLING TEAM: M Kuehl / D Downs / T Puchalski

SAMPLING CONDITIONS

TEMPERATURE: 48 °F - $32 \times 5/9 =$ _____ °C (1A) HNu: 0 ppm
BAROMETRIC PRESSURE (PA): 30.23 mm Hg at 1215 AM/PM H₂S: 0 ppm
RELATIVE HUMIDITY: 92 % CH₄: 0 % LEL
WIND: 0 mph from _____
WEATHER: Sunny, cooling off

SAMPLE GRID COORDINATES.: _____ N _____ E L-21
SAMPLING INTERVAL: 2' 7" ft refusal
SOIL CONDITIONS AT SURFACE: Sandy, dry

PUMP CALIBRATION

PUMP MFG/MODEL/SN: Gilar / Gilan / 2196
CALIBRATOR MFG/MODEL/SN: Elcal / Sensidyne / 251222
INITIAL CALIBRATION (QA) TO X=4.17 (n=7) L/MIN AT TIME: 0530
CALIBRATION VERIFICATION: ROTAMETER READING 4.20um TIME: 1510
ROTAMETER READING 4.20um TIME: 1530
*IF > 10%, SAMPLE TUBES SUSPECT, RESAMPLE % DIFFERENCE 0

SAMPLE COLLECTION

hole open 1510
E-26 TENAXE CHARCOAL TUBE NUMBER: T4754
STOP TIME: used stopwatch
START TIME: _____
TIME ELAPSED (T) 10.00.00 MINUTES
E-27 CHARCOAL-TENAX TUBE NUMBER: T4211
COLLECTION CONDITIONS: Intermittent suction, rotameter
variable (in waste?)
during sampling period

TOTAL VOLUMETRIC FLOW CALCULATION

$$V_m = T \times QA = \frac{10.00}{760} \times \frac{4.17}{273 + 1A} = 41.7 \text{ LITERS (V}_m\text{)}$$

$$V_s = V_m \times \frac{PA}{760} \times \frac{298}{273 + 1A} = \frac{1.75}{273 + 1A} \text{ LITERS (V}_s\text{)*}$$

*RECORD V_s IN LITERS ON SAS CHAIN OF CUSTODY REMARKS COLUMN.

SOIL GAS SURVEY FORM

1555

CLIENT: EPA ARCS DATE: 11/13/90 EPA SAS NO.: 5748E-28, E-29
SITE: Hmco DONOHUE SPL NO.: HDTT-12
PROJECT NO.: 20026
SAMPLING TEAM: DM Kuehl/D. Downs/T Puchalski

SAMPLING CONDITIONS

TEMPERATURE: 48 °F - $32 \times 5/9 =$ °C (tA) HNu: 0 ppm
BAROMETRIC PRESSURE (PA): 30.23 mm Hg at 1215 AM/PM H₂S: 0 ppm
RELATIVE HUMIDITY: 92 % CH₄: 0 % LEL
WIND: 0 mph from _____
WEATHER: sun setting

SAMPLE GRID COORDINATES: _____ N _____ E I-22
SAMPLING INTERVAL: 3.00 ft
SOIL CONDITIONS AT SURFACE: off road - sand near asphalt piles

PUMP CALIBRATION

PUMP MFG/MODEL/SN: Gilian/Gilair/251222 2196
CALIBRATOR MFG/MODEL/SN: E2cal/Sensidyne/251222
INITIAL CALIBRATION (QA) TO X=4.17 (n=7) L/MIN AT TIME: 0530
CALIBRATION VERIFICATION: ROTAMETER READING 4.0 TIME: 1545
*IF > 10%, SAMPLE ROTAMETER READING 4.0 TIME: 1620
TUBES SUSPECT, RESAMPLE % DIFFERENCE 0

SAMPLE COLLECTION

E-28 TENAX CHARCOAL TUBE NUMBER: TC35 E-29 CHARCOAL/TENAX TUBE NUMBER: T3262
STOP TIME: used COLLECTION CONDITIONS: _____
START TIME: stopwatch intermittent vacuum conditions
TIME ELAPSED (T) 10.00 MINUTES variable rotameter readings

TOTAL VOLUMETRIC FLOW CALCULATION

$$V_m = T \times QA = \frac{10.00}{760} \times \frac{4.17}{273 + tA} = 41.7 \text{ LITERS (V}_m\text{)}$$

$$V_s = V_m \times \frac{PA}{760} \times \frac{298}{273 + tA} = 1.75 \text{ LITERS (V}_s\text{)*}$$

*RECORD V_s IN LITERS ON SAS CHAIN OF CUSTODY REMARKS COLUMN.

SOIL GAS SURVEY FORM

1700

CLIENT: EPA ARCS DATE: 11/13/90 EPA SAS NO.: 5798E E-30, E-31
SITE: Hmco DONOHUE SPL NO.: HDTT-13
PROJECT NO.: 20026
SAMPLING TEAM: M Kuehl / D Downs / T Puchalski

SAMPLING CONDITIONS

TEMPERATURE: 48 °F - 32 x 5/9 = °C (tA) HNu: 0 ppm
BAROMETRIC PRESSURE (PA): 30.23 mm Hg at 1215 AM/PM H₂S: 0 ppm
RELATIVE HUMIDITY: 92 % CH₄: 0 % LEL
WIND: 0 mph from
WEATHER: cool, dusk

SAMPLE GRID COORDINATES: N E I-21
SAMPLING INTERVAL: 3.00 ft
SOIL CONDITIONS AT SURFACE: mounded sand - high point on berm

PUMP CALIBRATION

PUMP MFG/MODEL/SN: Gilan / Gilair / 2196
CALIBRATOR MFG/MODEL/SN: Elcal / sensidyne / 251222
INITIAL CALIBRATION (QA) TO X = 4.17 (n=7) L/MIN AT TIME: 0530
CALIBRATION VERIFICATION: ROTAMETER READING 4.0 TIME: 1645
ROTAMETER READING 4.0 TIME: 1715
*IF > 10%, SAMPLE TUBES SUSPECT, RESAMPLE % DIFFERENCE 0

SAMPLE COLLECTION

E-30 TENAX + CHARCOAL TUBE NUMBER: 103419 E-31 CHARCOAL/TENAX TUBE NUMBER: 14723
STOP TIME: used stopwatch COLLECTION CONDITIONS: intermittent
START TIME: variable rotameter, suction
TIME ELAPSED (T) 10.01.00 MINUTES created - noted upon sample train removal

TOTAL VOLUMETRIC FLOW CALCULATION

$$V_m = T \times QA = \frac{10.00}{760} \times \frac{4.17}{273 + tA} = 41.7 \text{ LITERS (V}_m\text{)}$$

$$V_s = V_m \times \frac{PA}{760} \times \frac{298}{273 + tA} = 1.75 \text{ LITERS (V}_s\text{)*}$$

*RECORD V_s IN LITERS ON SAS CHAIN OF CUSTODY REMARKS COLUMN.

SOIL GAS SURVEY FORM

0905

CLIENT: EPA ARCS DATE: 11/14/90 EPA SAS NO.: 5798E E-32E-33
SITE: Hmco DONOHUE SPL NO.: HDTT-14
PROJECT NO.: 20026
SAMPLING TEAM: M. Kuehl / D. Downs / T. Puchalski

SAMPLING CONDITIONS

TEMPERATURE: 35 °F - 32 x 5/9 = 1.67 °C (tA) HNu: 0 ppm
BAROMETRIC PRESSURE (PA): 30.20 mm Hg at 0800 (AM) PM H₂S: 0 ppm
RELATIVE HUMIDITY: 81 % CH₄: 0 % LEL
WIND: 5-10 mph from SE
WEATHER: sunny, mild

SAMPLE GRID COORDINATES.: N E D-24
SAMPLING INTERVAL: 3.0 ft
SOIL CONDITIONS AT SURFACE: sandy, visible Casoy

PUMP CALIBRATION

PUMP MFG/MODEL/SN: Gilman / Gilair / 2196 pump cal readings
CALIBRATOR MFG/MODEL/SN: Erca / Sensidyne / 251222 4.17 4.19 4.25
INITIAL CALIBRATION (QA) TO X = 4.17 n = 7 L/MIN AT TIME: 0600 4.23 4.08
CALIBRATION VERIFICATION: ROTAMETER READING 4.00 TIME: 0840 4.16 4.11
*IF > 10%, SAMPLE ROTAMETER READING 4.00 TIME: 080920
TUBES SUSPECT, RESAMPLE % DIFFERENCE 0 min

SAMPLE COLLECTION

E-32 TENAX + CHARCOAL TUBE NUMBER: TC4648 max E-33
STOP TIME: used stop watch COLLECTION CONDITIONS: drilled through waste, 3 separate
START TIME: "layers" felt during probe insertion
TIME ELAPSED (T) 10.00 MINUTES

TOTAL VOLUMETRIC FLOW CALCULATION

$$V_m = T \times QA = 10.00 \times 4.17 = 41.7 \text{ LITERS (V}_m\text{)}$$

$$V_s = V_m \times \frac{PA}{760} \times \frac{298}{273 + 1.67} = 1.79 \text{ LITERS (V}_s\text{)}$$

*RECORD V_s IN LITERS ON SAS CHAIN OF CUSTODY REMARKS COLUMN.

SOIL GAS SURVEY FORM

0945

CLIENT: EPA ARCS DATE: 11/14/90 EPA SAS NO.: 5748E E-34, E-35
SITE: Himco DONOHUE SPL NO.: HD TT-15
PROJECT NO.: 20026
SAMPLING TEAM: M Kuehl / D Downs / T. Puchalski

SAMPLING CONDITIONS

TEMPERATURE: 35 °F - $32 \times 5/9 = 1.67$ °C (tA) HNu: 0 ppm
BAROMETRIC PRESSURE (PA): 30.20 mm Hg at 0800 (AM) PM H₂S: 0 ppm
RELATIVE HUMIDITY: 81 % CH₄: 0 % LEL
WIND: 5-10 mph from SE
WEATHER: sunny, mild

SAMPLE GRID COORDINATES.: _____ N _____ E F-25
SAMPLING INTERVAL: 3.0 ft
SOIL CONDITIONS AT SURFACE: _____

PUMP CALIBRATION

PUMP MFG/MODEL/SN: Gilman/Gildir / 2169
CALIBRATOR MFG/MODEL/SN: ELCAL / Sensidyne / 251222
INITIAL CALIBRATION (QA) TO X=4.17 D=7 L/MIN AT TIME: 0600
CALIBRATION VERIFICATION: ROTAMETER READING 4.00 TIME: 0935
ROTAMETER READING 4.00 TIME: 0955
*IF > 10%, SAMPLE % DIFFERENCE 0
TUBES SUSPECT, RESAMPLE

SAMPLE COLLECTION

E-34 hole open 04350 mm TENAX &
CHARCOAL TUBE NUMBER: TL3182 mm E-35 CHARCOAL/TENAX TUBE NUMBER: T42
STOP TIME: used COLLECTION CONDITIONS: _____
START TIME: stop watch suction created at 30-60 seconds
TIME ELAPSED (T) 10.00 MINUTES intermittent rotameter variability

TOTAL VOLUMETRIC FLOW CALCULATION

$$V_m = T \times QA = \frac{10.00}{760} \times \frac{4.17}{273 + tA} = 41.7 \text{ LITERS (V}_m\text{)}$$
$$V_s = V_m \times \frac{PA}{273 + tA} = \frac{298}{273 + tA} = 1.79 \text{ LITERS (V}_s\text{)*}$$

*RECORD V_s IN LITERS ON SAS CHAIN OF CUSTODY REMARKS COLUMN.

SOIL GAS SURVEY FORM

1025

CLIENT: EPA ARCS DATE: 11/14/90 EPA SAS NO.: 5798 E E-36, E-37
SITE: Hmco DONOHUE SPL NO.: HDTT16
PROJECT NO.: 20026
SAMPLING TEAM: M Kuehl / D. Downs / T. Puchalski

SAMPLING CONDITIONS

TEMPERATURE: 35 °F - $32 \times 5/9 = 1.67$ °C (tA) HNu: 0 ppm
BAROMETRIC PRESSURE (PA): 30.20 mm Hg at 0800 (AM/PM) H₂S: 0 ppm
RELATIVE HUMIDITY: 81 % CH₄: 6 % LEL
WIND: 5-10 mph from SE
WEATHER: sunny mild

SAMPLE GRID COORDINATES.: _____ N _____ E K-14
SAMPLING INTERVAL: 3.0 ft
SOIL CONDITIONS AT SURFACE: sandy, dead sumac

PUMP CALIBRATION

PUMP MFG/MODEL/SN: Gilman / Gilair / 2196
CALIBRATOR MFG/MODEL/SN: Elcal / Sensidyne / 251222
INITIAL CALIBRATION (QA) TO $\bar{x} = 4.17$ n=7 L/MIN AT TIME: 0600
CALIBRATION VERIFICATION: ROTAMETER READING 4.00 TIME: 1005
*IF > 10%, SAMPLE ROTAMETER READING 4.00 TIME: 1035
TUBES SUSPECT, RESAMPLE % DIFFERENCE 0

SAMPLE COLLECTION

CHARCOAL TUBE NUMBER: 714126 CHARGOAL/TENAX TUBE NUMBER: 74707
STOP TIME: used stop watch COLLECTION CONDITIONS: suction created, intermittent
START TIME: stop watch variable rotameter readings
TIME ELAPSED (T) 10.00 MINUTES

TOTAL VOLUMETRIC FLOW CALCULATION

$$V_m = T \times QA = \frac{10.00}{760} \times \frac{4.17}{273 + tA} = 41.7 \text{ LITERS (V}_m\text{)}$$

$$V_s = V_m \times \frac{PA}{760} \times \frac{298}{273 + tA} = 1.79 \text{ LITERS (V}_s\text{)*}$$

*RECORD V_s IN LITERS ON SAS CHAIN OF CUSTODY REMARKS COLUMN.

SOIL GAS SURVEY FORM

1040

CLIENT: EPA ARCS DATE: 11/14/90 EPA SAS NO.: 5798 E E-38, E-39
SITE: Hmico DONOHUE SPL NO.: HD FDTT16
PROJECT NO.: 20026
SAMPLING TEAM: m Kuehl / D Downes / T. Puchalski

SAMPLING CONDITIONS

TEMPERATURE: 35 °F - 32 x 5/9 = 1.67 °C (1A) HNu: 0 ppm
BAROMETRIC PRESSURE (PA): 30.20 mm Hg at 0800 AM/PM H₂S: 0 ppm
RELATIVE HUMIDITY: 91 % CH₄: 0 % LEL
WIND: 5-10 mph from SE
WEATHER: Sunny mild

SAMPLE GRID COORDINATES: _____ N _____ E K-14
SAMPLING INTERVAL: 3.0 ft
SOIL CONDITIONS AT SURFACE: Sandy, dead sumac

PUMP CALIBRATION

PUMP MFG/MODEL/SN: Gilman / Gilair / 2196
CALIBRATOR MFG/MODEL/SN: Elcal / Sensidyne / 251222
INITIAL CALIBRATION (QA) TO X=4.17 n=7 L/MIN AT TIME: 0600
CALIBRATION VERIFICATION: ROTAMETER READING 4.00 TIME: 035
ROTAMETER READING 4.00 TIME: 1100
*IF > 10%, SAMPLE TUBES SUSPECT, RESAMPLE % DIFFERENCE 0

SAMPLE COLLECTION

E-38 TENAX 8 man E-39
CHARCOAL TUBE NUMBER: TC4742 CHARCOAL/TENAX TUBE NUMBER: T4698
STOP TIME: _____ COLLECTION CONDITIONS: _____
START TIME: used stopwatch field dup at hole TT16
TIME ELAPSED (T) 10.00 MINUTES

TOTAL VOLUMETRIC FLOW CALCULATION

$$V_m = T \times QA = \frac{10.00}{4.17} \times 4.17 = 41.7 \text{ LITERS (V}_m\text{)}$$

$$V_s = V_m \times \frac{PA}{760} \times \frac{298}{273 + tA} = \frac{41.7}{760} \times \frac{298}{273 + 1A} = 1.74 \text{ LITERS (V}_s\text{)*}$$

*RECORD V_s IN LITERS ON SAS CHAIN OF CUSTODY REMARKS COLUMN.

SOIL GAS SURVEY FORM

CLIENT: EPA ARCS DATE: 11/14 EPA SAS NO.: 5798E E-40 E-41
SITE: Himco DONOHUE SPL NO.: ^{HD-11} MS01
PROJECT NO.: 20026
SAMPLING TEAM: M Kuenl

SAMPLING CONDITIONS

TEMPERATURE: _____ °F - 32 x 5/9 = _____ °C (tA) H₂O: _____ ppm
BAROMETRIC PRESSURE (PA): _____ mm Hg at _____ AM/PM H₂S: _____ ppm
RELATIVE HUMIDITY: _____ % CH₄: _____ % LEL
WIND: _____ mph from _____ *not applicable*
WEATHER: _____
SAMPLE GRID COORDINATES.: _____ N _____ E
SAMPLING INTERVAL: _____ ft
SOIL CONDITIONS AT SURFACE: _____

PUMP CALIBRATION

not applicable
PUMP MFG/MODEL/SN: _____
CALIBRATOR MFG/MODEL/SN: _____
INITIAL CALIBRATION (QA) TO _____ L/MIN AT TIME: _____
CALIBRATION VERIFICATION: ROTAMETER READING _____ TIME: _____
*IF > 10%, SAMPLE ROTAMETER READING _____ TIME: _____
TUBES SUSPECT, RESAMPLE % DIFFERENCE _____

SAMPLE COLLECTION

E-40 TENAX
CHARCOAL TUBE NUMBER: TC 4484 *max E-41* CHARGOAL/TENAX TUBE NUMBER: T4717
STOP TIME: _____ COLLECTION CONDITIONS: _____
START TIME: not applicable matrix spike
TIME ELAPSED (T) _____ MINUTES unexposed tubes

TOTAL VOLUMETRIC FLOW CALCULATION

$V_m = T \times QA = \text{_____} \times \text{_____} = \text{_____}$ LITERS (V_m) *not applicable*
 $V_s = V_m \times \frac{PA}{760} \times \frac{298}{273 + tA} = \text{_____}$ LITERS (V_s)^{*}

*RECORD V_s IN LITERS ON SAS CHAIN OF CUSTODY REMARKS COLUMN.

SOIL GAS SURVEY FORM

CLIENT: EPA ARCS DATE: 11/14/90 EPA SAS NO.: 5798E E-42, E-43
SITE: Hmncw DONOHUE SPL NO.: HD TMSD01
PROJECT NO.: 20026
SAMPLING TEAM: M Kuoh

SAMPLING CONDITIONS

TEMPERATURE: _____ °F - 32 x 5/9 = _____ °C (tA) H₂O: _____ ppm
BAROMETRIC PRESSURE (PA): _____ mm Hg at _____ AM/PM H₂S: _____ ppm
RELATIVE HUMIDITY: _____ % CH₄: _____ % LEL
WIND: _____ mph from _____ *not applicable*
WEATHER: _____

SAMPLE GRID COORDINATES: _____ N _____ E

SAMPLING INTERVAL: _____ ft

SOIL CONDITIONS AT SURFACE: _____

PUMP CALIBRATION

PUMP MFG/MODEL/SN: _____ *not applicable*
CALIBRATOR MFG/MODEL/SN: _____
INITIAL CALIBRATION (QA) TO _____ L/MIN AT TIME: _____
CALIBRATION VERIFICATION: ROTAMETER READING _____ TIME: _____
*IF > 10%, SAMPLE ROTAMETER READING _____ TIME: _____
TUBES SUSPECT, RESAMPLE % DIFFERENCE _____

SAMPLE COLLECTION

E-42 CHARCOAL TUBE NUMBER: TC 4735 *E-43* CHARCOAL TUBE NUMBER: T4673
STOP TIME: *not applicable* COLLECTION CONDITIONS: _____
START TIME: _____ *matrix spike duplicate*
TIME ELAPSED (T) _____ MINUTES *unexposed tubes*

TOTAL VOLUMETRIC FLOW CALCULATION

$V_m = T \times QA = \text{_____} \times \text{_____} = \text{_____} \text{ LITERS (V}_m\text{)}$ *not applicable*
 $V_s = V_m \times \frac{PA}{760} \times \frac{298}{273 + tA} = \text{_____} \text{ LITERS (V}_s\text{)*}$

*RECORD V_s IN LITERS ON SAS CHAIN OF CUSTODY REMARKS COLUMN.

SOIL GAS SURVEY FORM

CLIENT: EPA ARCS DATE: 11/14/90 EPA SAS NO.: 5748E E-44, E-45
SITE: Hmco DONOHUE SPL NO.: HD TM502
PROJECT NO.: 20026
SAMPLING TEAM: M Kuehl

SAMPLING CONDITIONS

TEMPERATURE: _____ °F - 32 x 5/9 = _____ °C (tA) HNu: _____ ppm
BAROMETRIC PRESSURE (Pa): _____ mm Hg at _____ AM/PM H₂S: _____ ppm
RELATIVE HUMIDITY: _____ % CH₄: _____ % LEL
WIND: _____ mph from _____ *not applicable*
WEATHER: _____

SAMPLE GRID COORDINATES.: _____ N _____ E

SAMPLING INTERVAL: _____ ft

SOIL CONDITIONS AT SURFACE: _____

PUMP CALIBRATION

PUMP MFG/MODEL/SN: _____ *not applicable*
CALIBRATOR MFG/MODEL/SN: _____
INITIAL CALIBRATION (QA) TO _____ L/MIN AT TIME: _____
CALIBRATION VERIFICATION: ROTAMETER READING _____ TIME: _____
*IF > 10%, SAMPLE ROTAMETER READING _____ TIME: _____
TUBES SUSPECT, RESAMPLE % DIFFERENCE _____

SAMPLE COLLECTION

E-44 CHARCOAL TUBE NUMBER: TL3148 *E-45* CHARCOAL/TENAX TUBE NUMBER: T 4715
STOP TIME: _____ COLLECTION CONDITIONS: _____
START TIME: not applicable matrix spike
TIME ELAPSED (T) _____ MINUTES unexposed tubes

TOTAL VOLUMETRIC FLOW CALCULATION

$V_m = T \times Q_A = \text{_____} \times \text{_____} = \text{_____}$ LITERS (V_m)
 $V_s = V_m \times \frac{PA}{760} \times \frac{298}{273 + tA} = \text{_____}$ LITERS (V_s) * *not applicable*

*RECORD V_s IN LITERS ON SAS CHAIN OF CUSTODY REMARKS COLUMN.

SOIL GAS SURVEY FORM

CLIENT: EPA ARCS DATE: 11/14/90 EPA SAS NO.: 5798E E-46, E-47
SITE: Hmld DONOHUE SPL NO.: HD TMSD02
PROJECT NO.: 20026
SAMPLING TEAM: M. Kuehl

SAMPLING CONDITIONS

TEMPERATURE: _____ °F - 32 x 5/9 = _____ °C (ta) HNu: _____ ppm
BAROMETRIC PRESSURE (Pa): _____ mm Hg at _____ AM/PM H₂S: _____ ppm
RELATIVE HUMIDITY: _____ % CH₄: _____ % LEL
WIND: _____ mph from _____ *not applicable*
WEATHER: _____

SAMPLE GRID COORDINATES.: _____ N _____ E

SAMPLING INTERVAL: _____ ft

SOIL CONDITIONS AT SURFACE: _____

PUMP CALIBRATION

PUMP MFG/MODEL/SN: _____ *not applicable*
CALIBRATOR MFG/MODEL/SN: _____
INITIAL CALIBRATION (Qa) TO _____ L/MIN AT TIME: _____
CALIBRATION VERIFICATION: ROTAMETER READING _____ TIME: _____
*IF > 10%, SAMPLE ROTAMETER READING _____ TIME: _____
TUBES SUSPECT, RESAMPLE % DIFFERENCE _____

SAMPLE COLLECTION

E-46 CHARCOAL TUBE NUMBER: TC4141 *MAX E-47* CHARCOAL/TENAX TUBE NUMBER: T4694
STOP TIME: _____ COLLECTION CONDITIONS: _____
START TIME: _____ *not applicable* *matrix spike duplicates*
TIME ELAPSED (T) _____ MINUTES *unexposed tubes*

TOTAL VOLUMETRIC FLOW CALCULATION

$V_m = T \times Q_A = \text{_____} \times \text{_____} = \text{_____ LITERS (V}_m\text{)}$
 $V_s = V_m \times \frac{PA}{760} \times \frac{298}{273 + t_A} = \text{_____ LITERS (V}_s\text{)}$ *not applicable*

*RECORD V_s IN LITERS ON SAS CHAIN OF CUSTODY REMARKS COLUMN.

ATTACHMENT C

LABORATORY RESULTS
FIELD TRIAL SAMPLES

Transmission from:

ITAS - Cincinnati
11499 Chester Road
Cincinnati, Ohio 45246

FAX # (513) 782-4644

Voice # (513) 782-4600

From: PATRICK FARRELL

Department: GC/MS

To: CHARLENE KHAZAE / MARCA KUHEL

Company: DONAHUE & ASSOCIATES

Department: _____

FAX #: 1-414-458-0550

Voice #: _____

Special Instructions/Comments:

FORM 1A & 1E FOR SAS PROJECT #5798-E

FOR FURTHER INFO CONTACT PATRICK FARRELL

(C) 513-782-4805

Disposition of Original: ☐ Return to Originator ☐ Discard

Total Number of Pages including this cover sheet: 9 FAX Operator: PGH

VOLATILE ORGANICS ANALYSIS DATA SHEET

HDTT01-01

LAB NAME: PEI ASSOCIATESCONTRACT: SAS 5798-E5798E-1 / 5798E-2SAMPLE MATRIX: TENAXLAB SAMPLE ID: X0-11-064-01ASAMPLE WT/VOL: NALAB FILE ID: 5798-E1LEVEL: (low/med) LOWDATE RECEIVED: 11/8/90% MOISTURE: not dec. NADATE ANALYZED: 11/8/90DILUTION FACTOR: 1CONCENTRATION UNITS: NG/L

CAS NO.	COMPOUND	NG-SC-	Q
		DET. LIMIT	
74-87-3	CHLOROMETHANE	3.10	U
74-83-9	BROMOMETHANE	3.10	U
75-01-4	VINYL CHLORIDE	3.10	U
75-00-3	CHLOROETHANE	3.10	U
75-09-2	METHYLENE CHLORIDE	8.3	8 B
67-64-1	ACETONE	18.5	10
75-13-0	CARBON DISULFIDE	2.5	U
75-35-4	1,1-DICHLOROETHENE	2.5	U
75-34-3	1,1-DICHLOROETHANE	2.5	U
540-59-0	1,2-DICHLOROETHENE (TOTAL)	2.5	U
67-66-3	CHLOROFORM	2.5	U
107-06-2	1,2-DICHLOROETHANE	2.5	U
78-93-3	2-BUTANONE	3.10	U
71-55-6	1,1,1-TRICHLOROETHANE	2.5	U
56-23-5	CARBON TETRACHLORIDE	2.5	U
108-05-4	VINYL ACETATE	3.10	U
75-27-4	BROMODICHLOROMETHANE	2.5	U
78-87-5	1,2-DICHLOROPROPANE	2.5	U
10061-01-5	cis-1,3-DICHLOROPROPENE	2.5	U
79-01-6	TRICHLOROETHENE	2.5	U
124-48-1	DIBROMOCHLOROMETHANE	2.5	U
79-00-5	1,1,2-TRICHLOROETHANE	2.5	U
71-43-2	BENZENE	2.1	8 J
10061-02-6	trans-1,3-DICHLOROPROPENE	2.5	U
75-25-2	BROMOFORM	2.5	U
108-10-1	4-METHYL-2-PENTANONE	3.10	U
591-78-6	2-HEXANONE	3.10	U
127-18-4	TETRACHLOROETHENE	2.5	U
79-34-5	1,1,2,2-TETRACHLOROETHANE	2.5	U
108-88-3	TOLUENE	2.24	8
108-90-7	CHLOROBENZENE	2.5	U
100-41-4	ETHYL BENZENE	2.5	U
100-42-5	STYRENE	2.5	U
1330-20-7	XYLENE (TOTAL)	2.5	U

FORM 1A VOA

HDΠ01-01

CONTRACT: SAS 5798-E | 5798-E1 / 5798-E2

LAB SAMPLE ID: X0-11-064-01A

LAB FILE ID: 5798-E1

DATE RECEIVED: 11/8/90

DATE ANALYZED: 11/8/90

NUMBER OF TIC'S FOUND: 2

CONCENTRATION UNITS: NG/L
RET. TIME ~~NG-00~~ 0

FORM 1E VOA-TIC

VOLATILE ORGANICS ANALYSIS DATA SHEET

140TT02-01

LAB NAME: PEI ASSOCIATESCONTRACT: SAS 5798-E 5798E-3 / 5798E-4SAMPLE MATRIX: TENAXLAB SAMPLE ID: XD-11-064-02ASAMPLE WT/VOL: NALAB FILE ID: 5798-E3LEVEL (low/med) LOWDATE RECEIVED: 11/8/90% MOISTURE: not dec. NADATE ANALYZED: 11/8/90DILUTION FACTOR: 1CONCENTRATION UNITS: NG/L

CAS NO.	COMPOUND	NG-DE	DET. LIMIT	Q
74-87-3	CHLOROMETHANE		5 10	U
74-83-9	BROMOMETHANE		5 10	U
75-01-4	VINYL CHLORIDE		5 10	U
75-00-3	CHLOROETHANE		5 10	U
75-09-2	METHYLENE CHLORIDE	17 8	8	8
67-64-1	ACETONE	18 8	10	
75-15-0	CARBON DISULFIDE	7 3	8	
75-35-4	1,1-DICHLOROETHENE		2 8	U
75-34-3	1,1-DICHLOROETHANE		2 8	U
540-59-0	1,2-DICHLOROETHENE (TOTAL)		2 8	U
67-66-3	CHLOROFORM		2 8	U
107-06-2	1,2-DICHLOROETHANE		2 8	U
78-93-3	2-BUTANONE		5 10	U
71-55-6	1,1,1-TRICHLOROETHANE	8 2	8	
56-23-5	CARBON TETRACHLORIDE		2 8	U
108-05-4	VINYL ACETATE		5 10	U
75-27-4	BROMODICHLOROMETHANE		2 8	U
78-87-5	1,2-DICHLOROPROPANE		2 8	U
10061-01-5	cis-1,3-DICHLOROPROPENE		2 8	U
79-01-6	TRICHLOROETHENE		2 8	U
124-48-1	DIBROMOCHLOROMETHANE		2 8	U
79-00-5	1,1,2-TRICHLOROETHANE		2 8	U
71-43-2	BENZENE	8 2	8	J
10061-02-6	trans-1,3-DICHLOROPROPENE		2 8	U
75-25-2	BROMOFORM		2 8	U
108-10-1	4-METHYL-2-PENTANONE		5 10	U
591-78-6	2-HEXANONE		5 10	U
127-18-4	TETRACHLOROETHENE		2 8	U
79-34-5	1,1,2,2-TETRACHLOROETHANE		2 8	U
108-88-3	TOLUENE	67 31	8	
108-90-7	CHLOROBENZENE		2 8	U
100-41-4	ETHYL BENZENE		2 8	U
100-42-5	STYRENE		2 8	U
1330-20-7	XYLENE (TOTAL)		2 8	U

HD TT 02-01

CONTRACT: SAS 5798-E | 5798-E3 / 5798-E4

LAB SAMPLE ID: XO-11-064-02A

LAB FILE ID: 5798-E3

DATE RECEIVED: 11/8/90

DATE ANALYZED: 11/8/90

NUMBER OF TIC'S FOUND: 3

Q

[illegible]

VOLATILE ORGANICS ANALYSIS DATA SHEET

HDTT03-01

LAB NAME: PEI ASSOCIATESCONTRACT: SAS 5798-E 5798E-5 / 5798E-6SAMPLE MATRIX: TENAXLAB SAMPLE ID: X0-11-064-03ASAMPLE WT/VOL: NALAB FILE ID: 5798-E5LEVEL (low/med) LOWDATE RECEIVED: 11/8/90% MOISTURE: not dec. NADATE ANALYZED: 11/8/90DILUTION FACTOR: 1CONCENTRATION UNITS: NG/L

CAS NO.	COMPOUND	NG/CC	DET. LIMIT	Q
74-87-3	CHLOROMETHANE		11 10	U
74-83-9	BROMOMETHANE		11 10	U
75-01-4	VINYL CHLORIDE		11 10	U
75-00-3	CHLOROETHANE		11 10	U
75-09-2	METHYLENE CHLORIDE	18 15	8	B
67-64-1	ACETONE	18 18	10	
75-15-0	CARBON DISULFIDE		6 8	U
75-35-4	1,1-DICHLOROETHENE		6 8	U
75-34-3	1,1-DICHLOROETHANE		6 8	U
340-59-0	1,2-DICHLOROETHENE (TOTAL)		6 8	U
67-66-3	CHLOROFORM		6 8	U
107-06-2	1,2-DICHLOROETHANE		6 8	U
78-93-3	2-BUTANONE		11 10	U
71-55-6	1,1,1-TRICHLOROETHANE		6 8	U
56-23-5	CARBON TETRACHLORIDE		6 8	U
108-05-4	VINYL ACETATE		11 10	U
75-27-4	BROMODICHLOROMETHANE		6 8	U
78-87-5	1,2-DICHLOROPROPANE		6 8	U
10061-01-5	cis-1,3-DICHLOROPROPENE		6 8	U
79-01-6	TRICHLOROETHENE		6 8	U
124-48-1	DIBROMOCHLOROMETHANE		6 8	U
79-00-5	1,1,2-TRICHLOROETHANE		6 8	U
71-43-2	BENZENE	2	8	J
10061-02-6	trans-1,3-DICHLOROPROPENE		6 8	U
75-25-2	BROMOFORM		6 8	U
108-10-1	4-METHYL-2-PENTANONE		11 10	U
591-78-6	2-HEXANONE		11 10	U
127-18-4	TETRACHLOROETHENE		6 8	U
79-34-5	1,1,2,2-TETRACHLOROETHANE		6 8	U
108-88-3	TOLUENE	18 21	8	
108-90-7	CHLOROBENZENE		6 8	U
100-41-4	ETHYL BENZENE		6 8	U
100-42-5	STYRENE		6 8	U
1330-20-7	XYLENE (TOTAL)		6 8	U

HTT03-01

CONTRACT: SAS 5798-E | 5798-E5 / 5798-E6

LAB SAMPLE ID: X0-11-064-03A

LAB FILE ID: 5798-E5

DATE RECEIVED: 11/8/90

DATE ANALYZED: 11/8/90

NUMBER OF TIC'S FOUND: 1

CAS NUMBER

COMPOUND NAME

RET. TIME	MS-SC	0
-----------	-------	---

[illegible]

VOLATILE ORGANICS ANALYSIS DATA SHEET

LAB NAME: PEI ASSOCIATESCONTRACT: SAS 5798-EVELKACOSAMPLE MATRIX: TENAXLAB SAMPLE ID: VELKACOSAMPLE WT/VOL: NALAB FILE ID: VELKACOLEVEL (low/med) LOWDATE RECEIVED: 11/8/90% MOISTURE: not dec. NADATE ANALYZED: 11/8/90DILUTION FACTOR: 1

CONCENTRATION UNITS:

CAS NO.	COMPOUND	MG/DC	Q
		DET. LIMIT	
74-87-3	CHLOROMETHANE	10	U
74-83-9	BROMOMETHANE	10	U
75-01-4	VINYL CHLORIDE	10	U
75-00-3	CHLOROETHANE	10	U
75-09-2	METHYLENE CHLORIDE	10	5
67-64-1	ACETONE	10	U
75-13-0	CARBON DISULFIDE	5	U
75-35-4	1,1-DICHLOROETHENE	5	U
75-34-3	1,1-DICHLOROETHANE	5	U
540-59-0	1,2-DICHLOROETHENE (TOTAL)	5	U
67-66-3	CHLOROFORM	5	U
107-06-2	1,2-DICHLOROETHANE	5	U
78-93-3	2-BUTANONE	13	10
71-55-6	1,1,1-TRICHLOROETHANE	5	U
56-23-5	CARBON TETRACHLORIDE	5	U
108-05-4	VINYL ACETATE	10	U
75-27-4	BROMODICHLOROMETHANE	5	U
78-87-5	1,2-DICHLOROPROPANE	5	U
10061-01-5	cis-1,3-DICHLOROPROPENE	5	U
79-01-6	TRICHLOROETHENE	5	U
124-48-1	DIBROMOCHLOROMETHANE	5	U
79-00-5	1,1,2-TRICHLOROETHANE	5	U
71-43-2	BENZENE	5	U
10061-02-6	trans-1,3-DICHLOROPROPENE	5	U
75-25-2	BROMOFORM	5	U
108-10-1	4-METHYL-2-PENTANONE	17	10
591-78-6	2-HEXANONE	39	10
127-18-4	TETRACHLOROETHENE	5	U
79-34-5	1,1,2,2-TETRACHLOROETHANE	5	U
108-88-3	TOLUENE	5	U
108-90-7	CHLOROBENZENE	5	U
100-41-4	ETHYL BENZENE	5	U
100-42-5	STYRENE	5	U
1330-20-7	XYLENE (TOTAL)	5	U

FORM 1A VOA

TENTATIVELY IDENTIFIED COMPOUNDS

LAB NAME: PEI ASSOCIATES

CONTRACT: SAS 5798-E

VBKACO

SAMPLE MATRIX: TENAX

LAB SAMPLE ID: YBLKACO

SAMPLE WT/VOL: NA

LAB FILE ID: YBLKACO

LEVEL (low/med) LOW

DATE RECEIVED: 11/8/90

% MOISTURE: not dec. NA

DATE ANALYZED: 11/8/90

DILUTION FACTOR: 1

NUMBER OF TIC'S FOUND: 0

CONCENTRATION UNITS:

CAS NUMBER

COMPOUND NAME

RET. TIME

NG DC

Q

[illegible]

ORIGINAL

TECHNICAL MEMORANDUM NUMBER 13

DATE: December 10, 1990

TO: Vanessa Harris
Project Files, Himco Dump Site

CC: M. Kuehl - RI Lead
R. Gau - Project Manager
M. Crosser - TSQAM

FROM: Rob Cannestra, Hydrogeologist

SUBJECT: EPA ARCS Region V Contract No. 68-W8-0093
EPA Work Assignment No. 17-5L4J
Donohue Project No. 20026.024
Himco Dump RI/FS Phase I

INSTALLATION OF WATER TABLE WELLS AND LANDFILL CAP SAMPLING

Introduction

Six shallow observations wells were installed on or adjacent to the Himco Dump site between the dates of November 5, 1990, and November 14, 1990. Water table observation wells were installed to obtain water elevation information and to allow for groundwater sampling. Tasks associated with the installation of these wells included logging and classification of continuously sampled soils, field screening of soil samples, collection of soil samples for chemical and geotechnical analysis, and well installation. In addition, geotechnical samples were taken from five locations on the landfill cap. Landfill cap samples were collected for testing to determine the engineering properties of the cap. The following text summarizes the methods and procedures used to complete these tasks and point out deviations from procedures written in the Field Sampling Plan (FSP) or drilling specifications.

Drilling and Sampling

Soil borings BRG-1 through BRG-6 were advanced using hollow stem auger techniques. The subcontractor, John Mathes and Associates (Mathes), used a Central Mine Equipment (CME) 550 ATV rig equipped with 4.25-inch ID (8.0-inch OD) hollow stem augers to complete these borings. All borings were continuously sampled from ground surface to total depth using a 3-inch OD stainless steel split spoon sampler. Two stainless steel split spoon samplers were used. Split spoon samplers were decontaminated between sampling intervals according to the following steps: (1) tap water rinse, (2)alconox wash, (3) tap water rinse, (4) isopropanol rinse, (5) two deionized water rinses.

At each location, borings were drilled and sampled to a depth of 16.0 feet to allow the well screen to be installed intersecting the water table. All borings were extended a nominal one foot by blind drilling with the hollow stem augers. The extension of borings was completed to accommodate any formation collapse during monitoring well installation. After completing a well installation, the drill rig and drilling tools were steam cleaned before proceeding to the next installation.

Field Screening and Logging of Soil Samples

After recovering the split spoon and immediately upon opening the sampler barrel, soil samples were field screened by slowly running an HNu photoionization detector (PID) over the length of the sample. The highest PID reading observed for each sample interval was recorded on the boring log.

After field screening, samples were collected for volatile organic compound (VOC) and other chemical analyses. Samples were logged by recording the attempted sample interval, sample length recovered, blow counts, and providing a visual description of the soil. Sample descriptions included the sample color (reference Munsell color chart), relative density, major and minor soil components, general engineering properties and references to the depositional environment. Based on these observations, soils were classified according to the Unified Soil Classification System (USCS). Completed soil boring logs are attached in Appendix A.

Sample Collection

Samples were collected for chemical and geotechnical analysis. Chemical sampling included samples for VOC, base neutrals (BNA), polychlorinated biphenyls (PCBs), cyanide and metals analysis. Geotechnical sampling included samples for Total Organic Carbon (TOC), Atterberg limits and grain size analyses. Samples collected during the completion of borings for water table well installations are summarized in Table 1.

Chemical Sampling

VOC samples were collected immediately after field screening the split spoon. Two 120 ml jars were filled with soil taken over the entire length of the recovered sample for VOC analysis. After filling the VOC sample jars, the remaining soil was emptied into a stainless steel mixing bowl and mixed with a stainless steel spoon. After mixing, two 8 oz. composite samples were taken of the homogenous soil mixture for BNA, PCB, and metals analyses. The sample mixing bowl and spoon were decontaminated between samples by the same method as the split spoon samplers.

According to the Work Plan, chemical samples were to be taken from the first five split spoons (upper 10 feet) at each shallow well location. However, elevated PID readings, peculiar odors or visual signs of contaminations required the collection of samples at depths below 10 feet. In these cases, the additional deeper samples were substituted for shallower samples displaying no signs of contamination. Potentially contaminated samples were collected below 10-foot depths in borings BRG-03, BRG-05, and BRG-06.

TABLE 1

RECORD OF COLLECTED SOIL SAMPLES
 WATER TABLE WELL BORINGS
 Himco Dump Site
 December, 1990

<u>Boring</u>	<u>Depth Interval (Feet)</u>	<u>VOCs</u>	<u>CHEMICAL SAMPLING</u>		<u>Duplicate</u>	<u>GEOTECHNICAL SAMPLING</u>		
			<u>BNA/PCB Pesticides</u>	<u>Metals Cyanide</u>		<u>TOC</u>	<u>Atterberg Limits</u>	<u>Grain Size</u>
BRG-01	0-2	X	X	X		X		
	2-4	X	X	X				
	4-6	X	X	X				
	6-8	X	X	X	X			
	10-12	X	X	X				
	14-16						X	X
BRG-02	0-2	X	X	X				
	2-4	X	X	X		X		
	4-6	X	X	X				
	6-8	X	X	X				
	8-10	X	X	X				
	14-16						X	X
BRG-03	0-2	X	X	X				
	2-4	X	X	X				
	4-6	X	X	X	X			
	6-8	X	X	X				
	8-10					X		
	14-16	X	X	X			X	X
BRG-04	0-2	X	X	X				
	2-4	X	X					
	4-6	X	X	X				
	6-8	X	X	X				
	8-10	X	X	X				
	14-16						X	X

TABLE 1

RECORD OF COLLECTED SOIL SAMPLES
 WATER TABLE WELL BORINGS
 Himco Dump Site
 December, 1990
 (continued)

<u>Boring</u>	<u>Depth Interval</u> <u>(Feet)</u>	<u>VOCs</u>	<u>CHEMICAL SAMPLING</u>		<u>Duplicate</u>	<u>GEOTECHNICAL SAMPLING</u>		
			<u>BNA/PCB</u> <u>Pesticides</u>	<u>Metals</u> <u>Cyanide</u>		<u>TOC</u>	<u>Atterberg</u> <u>Limits</u>	<u>Grain Size</u>
BRG-05	2-4	X	X	X	X			
	8-10	X	X	X				
	10-12	X	X	X				
	12-14	X	X	X				
	14-16	X	X	X		X	X	X
BRG-06	0-2	X	X	X				
	4-6	X	X	X				
	6-8					X	X	X
	8-10	X	X	X				
	12-14	X	X	X				
	14-16	X	X	X				

W/A/AG7

Geotechnical Samples

Geotechnical samples were collected randomly from borings completed for the installation of shallow observation wells. With the exception of boring BRG-06, samples for Atterberg limits and grain size analysis were taken in the interval to be screened during the well installation. Samples for Total Organic Carbon (TOC) analysis were not collected from every boring completed for the installation of shallow observation wells.

Geotechnical samples were collected after retrieval of chemical samples from the remaining composited soil. One 8 oz. jar was collected for Atterberg limit and grain size analysis. An additional 8 oz. jar sample was taken for TOC analysis when applicable.

All samples were labelled, packaged, and shipped according to the details of the field sampling plan. The site sample custodian completed the appropriate chain-of-custody documentation. Samples were shipped to the appropriate labs by Federal Express.

Well Installations

Shallow observation wells W-101A through W-106A were installed to intersect the water table. Observations made during the drilling and sampling of borings completed for the installation of the wells were used to determine the depth of the water table. Because of the shallow water table encountered, modifications were made to the general well specifications to ensure that the well screens intersected the water table. Table 2 summarizes well construction information and general well information for water table observation wells at the Himco Dump site. Well construction diagrams are included in Appendix B.

Wells were constructed using Schedule 5, Type 304, flush threaded stainless steel riser attached to 10-foot, continuous wire wrap, 0.010-inch slot, stainless steel screens. Stainless steel screens and riser were manufactured by Diedrich. Well screens and riser were steam cleaned immediately preceding installation, handled only while wearing clean latex gloves, and wrapped in protective plastic during transport. All flush threaded joints were wrapped with teflon tape to provide a tight seal. A concentrated effort was made to assure that well construction materials were not contaminated during handling or installation.

In general, observation wells were installed to depths of approximately 16 feet rather than the anticipated 20 feet. To allow for the installation of a 10-foot screen in these shallower borings, the thickness of the filter pack overlying the screen, bentonite seal, and concrete cap were decreased. In the modified well installations, filter packs were extended from 0.3 (WT-105A) to 1.2 (WT-101A) feet above the top of the well screen. Bentonite pellet seals were cut to a nominal 1.0-foot thickness rather than the specified 2.0 feet. The accuracy of measured depths was assured by the shallowness of these installations.

TABLE 2

WATER TABLE OBSERVATION WELL INFORMATION
Himco Dump Site
December 1990

<u>Well Number</u>	<u>State Plane Coordinates</u>		<u>Top of Pipe Elevation</u>	<u>Screen Length (Feet)</u>	<u>Depth to Bottom of Well (Feet)</u>	<u>Depth to Bottom of boring (Feet)</u>	<u>Depth to Bottom of Bentonite Seal (Feet)</u>
	<u>North</u>	<u>East</u>					
WT-101A	1,531,617.69	407,617.00	764.35	10	16.3	17.5	4.2
WT-102A	1,534,861.43	405,928.37	769.08	10	16.0	16.8	4.5
WT-103A	1,532,537.90	405,532.73	760.59	10	16.0	17.0	4.0
WT-104A	1,531,496.08	406,013.86	765.57	10	16.3	17.6	4.3
WT-105A	1,531,174.04	407,105.64	762.94	10	16.0	16.8	4.9
WT-106A	1,530,932.11	407,806.75	761.47	10	16.2	17.0	5.0

A/R/HIMCO/AH1

In addition, to facilitate the timely completion of wells, hydration times at several locations were shortened to approximately one-half hour. The integrity of these seals was visually checked prior to the installation of a concrete cap. Finally, concrete cap thickness was reduced from a specified 5.0 feet to a nominal 3.0-foot thickness to accommodate the shallow installation. None of these modifications is expected to adversely affect the performance of these wells.

Despite efforts made to ensure that well screens intersected the water table, the extremely shallow water table at the location of WT-103A made this impossible. During installation, depth to water in WT-103A was approximately 4.0 feet, placing the water level above the interval to be screened. Temporal fluctuations may cause water levels to decrease, potentially lowering the water level into the screened interval at this location.

Landfill Cap Geotechnical Samples

Geotechnical samples, including jar samples for grain size and Atterberg limit testing, and shelly tube samples for consolidation undrained triaxial shear were recovered from five locations on the landfill cap. Landfill cap sample locations varied slightly from those originally specified because they were located at points on the geophysical survey grid rather than the proposed site survey grid. The site survey grid was not completed at the time landfill cap samples were taken. Rather than sample at random or approximate locations on the cap, samples referenced geophysical survey grid points. Landfill cap geotechnical sample locations are included in the site location map (Figure 1).

Landfill cap samples were recovered by digging through the topsoil cover (average thickness approximately 0.5 feet) to the calcium sulfate cap. Once the cap was encountered, excavations were extended by hand to a depth of approximately 1.5 feet. At this depth, two pint size jar samples were collected for grain size and Atterberg limit testing. After collecting jar samples, the CME 550 drill rig was used to push 24-inch shelly tubes. The dense nature of the calcium sulfate cap made pushing the tubes difficult. At several locations, shelly tubes appeared to penetrate through the cap material into waste. If shelly tubes potentially encountered waste, they were marked as containing potential waste on the tube exterior. Additional shelly tube samples were attempted at two locations for one-dimensional consolidation testing, however, no sample was recovered at one location (adjacent to GE-01). Geotechnical sample holes were backfilled with spoils and hand compacted.

Atmospheric Monitoring

Air quality monitoring within the breathing zone and at the borehole was completed after recovery of the samples. A PID was used to monitor for volatile organic compounds. A GasTech® meter was used to monitor the levels of hydrogen sulfide (H₂S), oxygen, and indicate the percent of the Lower Explosive Limit (LEL) for methane. A miniRAD radiation detector was used to monitor for radioactivity. The highest readings produced by each instrument were recorded in the sections provided on the boring log. During the drilling and sampling of BRG-06, one sampling team member became physically ill while jarring samples from the 12 to 14-foot depth interval. However, atmospheric monitoring of

the borehole and recovered sample did not show any elevated readings at this depth. Atmospheric monitoring results recorded during the completion of borings is included in the completed soil boring logs attached in Appendix A.

Atmospheric monitoring was completed periodically during well installations. Efforts were made to take readings at the beginning of the installation procedure and during the installation as sections of auger were removed from the boring. Atmospheric monitoring during well installations was generally terminated after the installation of the bentonite seal as the boring was then considered effectively plugged off. Results of atmospheric monitoring during well installations were recorded on daily atmospheric monitoring logs attached in Appendix B.

During the recovery of geotechnical samples from the landfill cap, atmospheric monitoring was complete as shallow excavations were completed and as shelly tubes were withdrawn. Atmospheric readings taken during geotechnical sampling of the landfill cap were recorded on daily atmospheric monitoring logs attached in Appendix C.

No elevated levels were recorded during atmospheric monitoring conducted during the completion of shallow wells and landfill cap geotechnical sampling.

SUMMARY

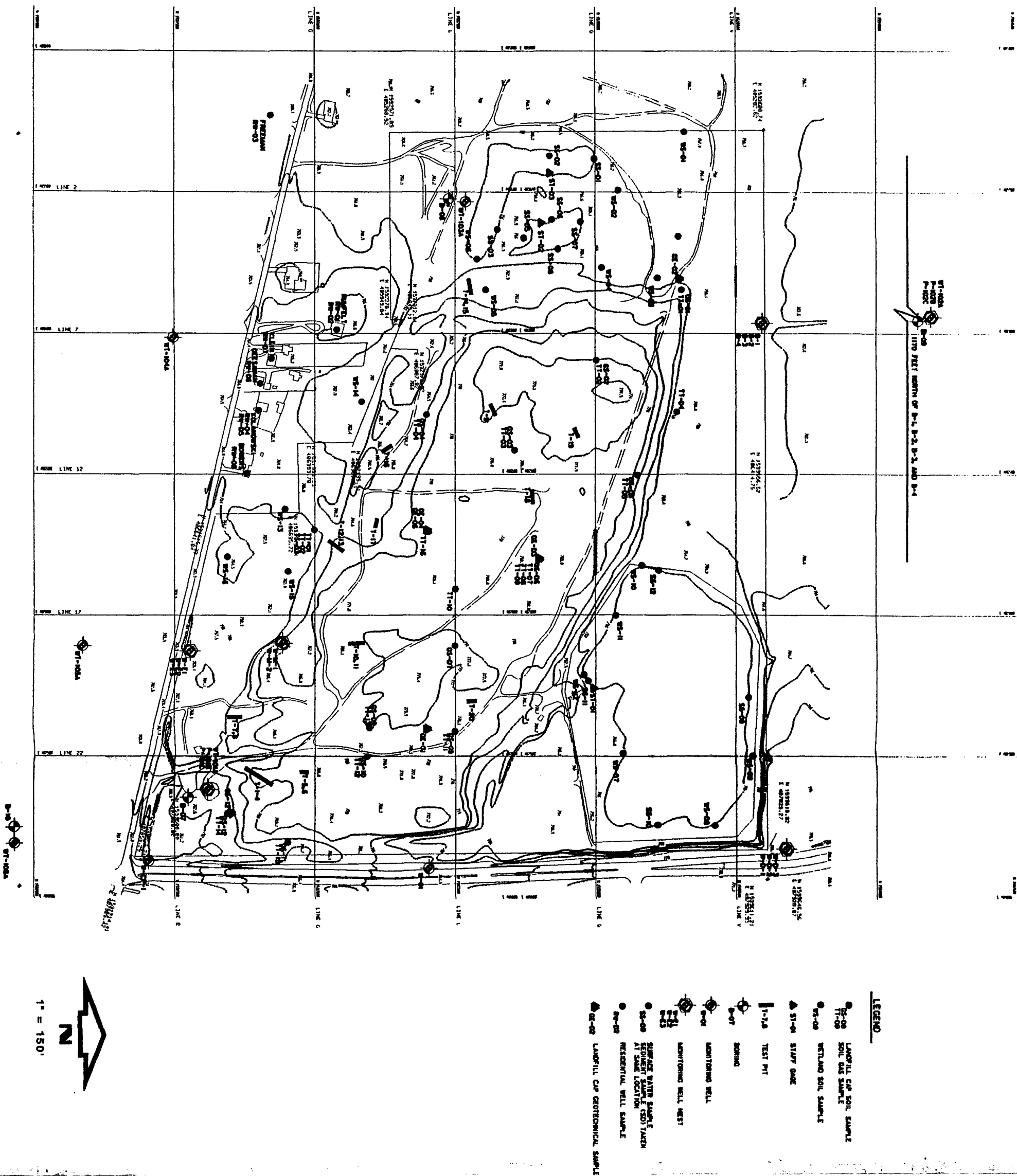
Six shallow soil borings were completed for the installation of water table observation wells. Soil samples were recovered for chemical analysis from the 0 to 10-foot depth interval or if contamination was indicated or observed, from intervals below 10 feet. Contamination was observed at depths below 10 feet in borings BRG-01, BRG-03, BRG-05, and BRG-06. Soil samples were submitted for VOC, BNA, PCB, pesticides, metals and cyanide analyses. Select soil samples were submitted for geotechnical analyses including TOC, grain size, and Atterberg limits.

Six water table observation wells were installed to intersect the water table. These wells were constructed to provide groundwater elevation information and to facilitate groundwater sampling. Concrete cap and bentonite seal thicknesses were modified to accommodate proper screening due to the shallow water table. Despite these efforts, the water level in WT-103A is above the well screen.

Geotechnical samples of the landfill cap below the surface cover were collected to determine the engineering properties of the cap. Jar and shelly tube samples of the landfill cap were collected and submitted for grain size, Atterberg limit, consolidation undrained triaxial shear, and non-dimensional consolidation testing. Shelly tube samples were potentially pushed into waste material and were appropriately labeled. At one shelly tube sample location, no sample was recovered.

A/R/HIMCO/AG8

FIGURE 1
SAMPLE LOCATION MAP



MAY 1991

FIGURE 1 SITE LOCATION MAP (TECHNICAL MEMO)

**HIMCO DUMP
SUPERFUND SITE
ELKHART, INDIANA**

20026

Donohue ENGINEERS
ARCHITECTS
SCIENTISTS

APPENDIX A
SOIL BORING LOGS

Donohue

BORING LOG

SOIL BORING NO.

Engineers & Architects
COMPUTER AIDED DESIGN/DRAFTINGSITE: HIMCO DUMP PROJECT NO. 20023 023

BRG-01

DRILLING METHOD: CME SSC

WATER LEVEL READINGS

GROUND SURFACE ELEV.: _____

4 1/4" I.D. HOLLOW STEMDATE 11/12/90 TIME 12:00 DEPTH 10.4 CASING 17.0

COORDINATES: _____

Augers 10 & 5' I.D.

NORTH: _____

LOG BY: R. CANESTRA

EAST: _____

DRILLER: D. ELLISDATE START: 11/12/90WEATHER: PLY CLOUD, 45°, NW WINDPHYSICAL SETTING: TO LANDFILL WELL INSTALLATION: WT-101A

GRASS ADJACENT DATE COMPLETE: _____

DEPTH IN FEET	SOIL DEPOSITIONAL ENVIRONMENT	USCS	SOIL DESCRIPTION AND DRILLING COMMENTS	BKGRND H _{Nu} 0.2	SAMPLING DATA				AIR MONITORING					
					B	N	A	R	SAMPLE TYPE / INTERVAL	TIME	PIO	O ₂ LEL	H ₂ S ₂ / RAD	
	OUTWASH	SP	MED DENSE, 10YR 2/1 BLACK SILTY SAND, TOP 2"		22				SS-1 0-2' 3" 0.2	13:51	0.2	21.2	0	0
1	OUTWASH	SP	MED. DENSE 10YK 5/6 YELLOWISH BROWN SAND / MEDIUM SUBANG. FROSTED QUARTZITE GRAINS) TO FINE SAND, TO 5M GRAVEL (SUBANG. ANG. QUARTZITE CLASTS). NON-PLAS. NON COHESIVE, TO SILT, DAMP						IN SPOON					
2	OUTWASH	SP	MED. DENSE, 10YR 5/8, YELLOWISH BROWN SAND (F.M. SUBANG. ANG. FROSTED, QUARTZITE GRAINS) NON PLASTIC, NON COHESIVE, SOME FeO ₂ STAINING, SOME LIME IN LOWER 6-8" OF SPOON, DAMP.		16				SS-2 2'-4' 3" 0.2	13:57	0.2	21.1	0	0
3									IN SPOON					
4														
5	OUTWASH	SP	MED DENSE, MOTTLED 10YR 7/4 & 10YR 4/2 VERY PALE BROWN / DARK YELLOWISH BROWN SAND (MEDIUM SUBANG. SUBANG. FROSTED QUARTZITE GRAINS) TO 2 CM GRAVEL (F.M. FINE, DOL. TO 2 CM). NON PLASTIC, NON COHESIVE, DAMP		17				SS-3 4'-6' 3" 0.2	14:24	0.2	21.1	0	0
6									IN SPOON					
7	OUTWASH	SP	MED DENSE 10YR 5/6 YELLOWISH BROWN SAND (MEDIUM SUBANG. SUBANG. FROSTED, QUARTZITE GRAINS) TRACE OF SAND, TO 5M GRAVEL (F.M. FINE, DOL. TO 2 CM). NON PLASTIC, NON COHESIVE, DAMP - WET		13				SS-4 6'-8' 3" 0.2	14:29	0.2	21.1	0	0
8									IN SPOON					
9	OUTWASH	SP	LOOSE, 10YR 5/4 YELLOWISH BROWN SAND (MEDIUM SUBANG. SUBANG. FROSTED QUARTZITE GRAINS) TO 2 CM SAND, NON PLASTIC, SLIGHT COHESION, SATURATED		10				SS-5 8'-10' 3" 0.2	14:46	0.2	21.2	0	0
10									IN SPOON					
11	OUTWASH	SP	VERY LOOSE 10YR 5/4 YELLOWISH BROWN SAND (MEDIUM SUBANG. SUBANG. FROSTED, QUARTZITE GRAINS) NON PLAS. NON COHESIVE, (C) 10.7 COLOR CHANGE TO 7.5 YR 7/1		3				SS-6 10'-12' 3" 0.2	15:00	0.2	21.1	0	0
12		BROWN BLACK	BLACK SAND (M.F.A. SUBANG. SUBANG. FROSTED, QUARTZITE GRAINS, TO GRAVEL SUBANG. SUBANG. FROSTED, QUARTZITE CLASTS NON PLASTIC, SLIGHT COHESION, SATURATED, NO OIL						IN SPOON					
13	OUTWASH	SP	VERY DENSE, 10YR 4/1 DARK GRAY SAND (MEDIUM SUBANG. SUBANG. FROSTED, QUARTZITE GRAINS) TO 5M GRAVEL (SUBANG. SUBANG. FROSTED, QUARTZITE CLASTS) NON PLASTIC, NON COHESIVE, FETTERED OIL, AT LEVEL		52				SS-7 12'-14' 3" 0.2	15:15	0.2	21.1	0	0
14									IN SPOON					
			DENSE 10YR 4/1 DARK GRAY SAND (MEDIUM, SUBANG. SUBANG. FROSTED, QUARTZITE GRAINS, TO 5M GRAVEL (SUBANG. SUBANG. FROSTED, QUARTZITE CLASTS) NON PLASTIC, NON COHESIVE, FETTERED OIL, AT LEVEL		47				SS-8 14'-16' 3" 0.2	15:27	0.2	21.1	0	0

Donohue

BORING LOG

SOIL BORING NO.

Engineers & Architects

SITE: ^{HIMCO} DUMP PROJECT NO. 20026.023

BRG-01

DRILLING METHOD: TIME 550
5 1/4 IN. ID HOLLOW STEM
AUGERS (Ø.65" ID)

WATER LEVEL READINGS			
DATE	TIME	DEPTH	CASING
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____

GROUND SURFACE ELEV.: _____
COORDINATES: _____
NORTH: _____
EAST: _____
DATE START: 11/12/90
DATE COMPLETE: 11/12/90
WELL INSTALLATION: WT-101A

LOG BY: R. CANESTRA
DRILLER: D. ELIS
WEATHER: _____

PHYSICAL SETTING:

[illegible]

Donohue

BORING LOG

SOIL BORING NO.

Engineers & Architects

SITE: HIMCO DUMP PROJECT NO. 20026

BRG-2

COMPUTER AIDED DESIGN/DRAFTING

DRILLING METHOD: 0.65" OD
(1/4" IN ID) HOLLOW STEM AUGER

WATER LEVEL READINGS

GROUND SURFACE ELEV.: _____

DATE 11/10 TIME 10:20 DEPTH 0.4 CASING ALUMINUM

COORDINATES: _____

WITH CME SSO

NORTH: _____

LOG BY: R. CANNESTA

EAST: _____

DRILLER: D. ELLISDATE START: 11/10/90WEATHER: CLEAR, LT BREEZE, 40°-48° BACKGROUND PID 0.2

DATE COMPLETE: _____

PHYSICAL SETTING: _____

WELL INSTALLATION: _____

DEPTH IN FEET	SOIL DEPOSITIONAL ENVIRONMENT	USCS	SOIL DESCRIPTION AND DRILLING COMMENTS	SAMPLING DATA				AIR MONITORING						
				B	N	A	R	SAMPLE		TIME	PID	O ₂	LEL	RAD
								TYPE	INTERVAL					
	EOLIAN	OL-SM	MD, 10YR 3/3, DK BROWN SILTY ORGANIC SAND SAND F.M., TC 2.2, SAND, GRAV (SPAND) ONLY COHESIVE, NONPLASTIC, MOIST	11				SS-1	0-2	13:35	0.2	20.5%	0	
1.0								3"	0.2					
2	OUTWASH	SP-SM	MD, 10YR 3/4, DK YELLOWISH BROWN SILTY SAND SAND (M-F), TC 2.2, SAND, GRAV (SPAND) SLIGHT COHESIVE, NON PLASTIC, MOIST				20							
3		SP	MD, 10YR 4/6, DK YELLOWISH BROWN, SAND F.M., SUB-SATURATED, FROSTED QUARTZITE GRAINS, TC (7-8%) 1m - 1m, SUE ANGLE TO SUBEND, DOL, GRAV, NON PLASTIC, NON COHESIVE, MOIST - DAMP	13				SS-2	2-4	13:45	0.2	20.5%	0	
4								3"	0.2					
5							17							
6		SP	D 10YR 10/3, PALE BROWN SAND, FM QUARTZITE FROSTED, SUB-SATURATED, GRAINS, NON PLASTIC, NON COHESIVE, MOIST, 3"	22				SS-3	4-6	14:20	0.2	20.5%	0	
7			MOTTLED W/ DK YELLOWISH BROWN @ 5:5											
8	OUTWASH	SP	MD, 10YR 10/3, PALE BROWN MOTTLED W/ 10YR 5/8 SAND, F.M., SUB-SATURATED, FROSTED, SUB-SATURATED, GRAINS, TC SILT NON PLASTIC, SLIGHT COHESION, TC ORGANIC FRAGMENTS, MOIST	27				SS-4	6-8	14:26	0.2	20.4%	0	
9								3"	0.2					
10		SP	MD, 10YR 6/4, LT YELLOWISH BROWN, SAND F.M. SUBEND, FROSTED, QUARTZITE GRAINS, TC 1m - 1m, NON PLASTIC, SLIGHT COHESION, TC Co SAND, MOIST - WET	14				SS-5	8-10	14:58	0.2	20.5%	0	
11			(R) 2.0 FT SAND CHANGE TO											
12	OUTWASH	SP	MD, 10YR 4/4, DK YELLOWISH BROWN SAND, F.M., TC 2.2, SAND, GRAV (SPAND) SUBEND, FROSTED, PILE, NON PLASTIC NON COHESIVE, TC 2m GRAV, DOLASTIC, SATURATED.	20				SS-6	10-12	15:05	0.2	20.4%	0	
13								3"	0.2					
14		SP	DENSE 10YR 5/3 BROWN, SAND, MEDIUM TC 2.2, SAND, GRAV, NON PLASTIC 2m - 2m, 3" LAYER OF SILTY FINE SAND @ 12.1, 1m - 1m COHESIVE, NON PLASTIC, SATURATED.	20				SS-7	12-14	15:35	0.2	20.4%	0	
15								3"	0.2					
16							16							
17			VD, 10YR 5/4 YELLOWISH - BROWN SAND F.M. TC 2.2, SAND, GRAV, NON PLASTIC 2m - 2m, 3" LAYER OF SILTY FINE SAND @ 12.1, 1m - 1m COHESIVE, NON PLASTIC, SATURATED.	16				SS-8	14-16	15:42	0.2	20.4%	0	
18														

Donohue

BORING LOG

SOIL BORING NO.

Engineers & Architects

SITE: HIMCO DUMP PROJECT NO. 20026

ପି.ସି.ଏ. - ୧୨

DRILLING METHOD: 4.65' CD
(444 IN I.D.) HOLLOW STEM

[illegible]

GROUND SURFACE ELEV.: _____
COORDINATES: _____

AUGERS w/ CME 550

LOG BY: R. CANNESTRO

DRILLER: D. ELLIS

WEATHER: CLEAR LT BZEEZE 40-48°

PHYSICAL SETTING:

WELL INSTALLATION: _____

[illegible]

Donohue

BORING LOG

SOIL BORING NO.

Engineers & Architects
COMPUTER AIDED DESIGN/DRAFTINGSITE: KIMCO DUMPPROJECT NO. 20026

B26-03

DRILLING METHOD: 4 1/4" ID
HOLLOW STEM AUGERS
(0.65' O.D.)

WATER LEVEL READINGS

DATE: 11/11/90 TIME: 11:30 DEPTH: 4.1 CASING: 17.0

GROUND SURFACE ELEV.: _____

COORDINATES: _____

NORTH: _____

EAST: _____

LOG BY: R. CANNESTRADRILLER: D. ELLISWEATHER: FLY CLDY

ADJ TO POND

DATE START: 11/11/90DATE COMPLETE: 11/11/90PHYSICAL SETTING: BRUSH FIELDWELL INSTALLATION: WT-103A

DEPTH IN FEET	SOIL DEPOSITIONAL ENVIRONMENT	USCS	SOIL DESCRIPTION AND DRILLING COMMENTS	BACKGROUND HNA 0.1 PPM	SAMPLING DATA				AIR MONITORING						
					B	N	A	R	SAMPLE TYPE / INTERVAL		TIME	PID	O ₂ LEL	H ₂ %	CO ₂ %
0	OUTWASH	OL	LOOSE, 2.5 V 4/2, DK GRAYISH BROWN SAND (M-C), GRAINS QUARTZITIC, SUBANG TO SUBORD, PITER, 10% SM - L GRAV. (SUBORD, DOLOMITIC,) DAMP		9				SS-1	0-2	9:22	0.1	20.6	0	0
1	OUTWASH		(3" BROWN SILTY SAND, SOME ORGANICS, TOPSOIL)						3"	0.1					
2	OUTWASH	SP	MD, 10YR 5/3, BROWN, SAND, (MEDIUM, PITER SILTY AND SHEPPIC, QUARTZITIC GRAINS) TO FCA SAND TO SM - M GRAV. (SUBANG - SUBORD DOLOMITIC) NON PLASTIC, NON COHESIVE, DAMP - MOIST		15				SS-2	2-4	9:35	0.1	20.6	0	0
3			(22-28 GRAV. 5 H-2 @ 4 POOL - P)						3"	0.1					
4	OUTWASH	SP	DENSE, 10YR 5/3, BROWN, SAND, (MEDIUM SUBORD, PITER, FROSTED, QUARTZITIC GRAINS) TO FCA SAND, TO SILT, NON PLASTIC SLIGHT COHESION, SATURATED		45				SS-3	4-6	9:47	0.1	20.9	0	0
5									3"	0.1			DUPLICATE TAKEN		
6	OUTWASH	SP	DENSE, 10YR 5/3, BROWN, SAND, (MEDIUM SUBORD - BND, PITER, FROSTED, QUARTZITIC GRAINS) TO FCA SAND, TO SM GRAV. (DK BLACK SUBANG DOLOMITIC CLASTS) NON PLASTIC, NON COHESIVE, SATURATED		45				SS-4	6-8	9:57	0.1	20.9	0	0
7									3"	0.1					
8										IN SPOON					
9		SP	DENSE, 10YR 5/3, BROWN, SAND, (MEDIUM SUBANG - BND, PITER, FROSTED, QUARTZITIC GRAINS) TO FCA SAND, NON PLASTIC SLIGHT COHESION, SATURATED.		45				SS-5	8-10	10:20	0.1	20.5	0	0
10	OUTWASH	SW	AT 9.5, 10YR 5/3, BROWN SAND FCA LAYER, TO 10% GRAV. DOLOMITIC SOME FCA STAINING IN THIS LAYER						3"	0.1					
11		SW	DENSE, 10YR 5/3, GRAYISH BROWN, SAND FCA, 12-15% GRAVEL (BROWN, BLACK SUBANG, DOLOMITIC, CLASTS) NON- PLASTIC, NON COHESIVE, SATURATED		25				SS-6	10-12	10:33	0.1	20.9	0	0
12									3"	0.1					
13	OUTWASH	SW-GW	DENSE, 10YR 5/1, GRAY, SAND & GRAVEL SAND, FCA, SUBANG - SUBORD, FROSTED DOLOMITIC GRAINS, GRAVEL (SM - M SUBANG, DOLOMITIC, CLASTS) NON- PLASTIC, NON COHESIVE, SATURATED		25				SS-7	12-14	10:50	0.1	20.9	0	0
14									3"	0.1					
15										IN SPOON					
16			VERY DENSE, 10YR 5/1, GRAY, SAND & GRAVEL (SAND, FCA, SUBANG - SUBANG, FROSTED,		75				SS-8	14-16	11:00	0.1	20.6	0	0

Donohue

BORING LOG

SOIL BORING NO.

Engineers & Architects

SITE: HIMCO
DUMP

PROJECT NO. 20026

B26-03

DRILLING METHOD:
4 1/4" ID HC. & O.V. STEM
AUGER

[illegible]

GROUND SURFACE ELEV.: _____
COORDINATES: _____

LOG BY: R. CANNESTRA

DRILLER: D. ELLIS

WEATHER: OVERCAST, NW BREEZE

PHYSICAL SETTING: ADJACENT TO POND

NORTH: _____
EAST: _____

DATE START: 11/1/90

DATE COMPLETE: 11/11/90

WELL INSTALLATION: WT-103A

[illegible]

Donohue

BORING LOG

SOIL BORING NO.

Engineers & Architects
COMPUTER AIDED DESIGN/DRAFTINGSITE: WIMCO DUMP PROJECT NO. 20026

BRG-04

DRILLING METHOD: UME 550
4 1/4" ID HO-LAW STEM ALKESWATER LEVEL READINGS
DATE _____ TIME _____ DEPTH _____ CASING _____GROUND SURFACE ELEV.: _____
COORDINATES: _____LOG BY: Z CANVESTRA
DRILLER: D. ELLIS
WEATHER: OVERCASTDATE START: 11/11/90
DATE COMPLETE: 11/11/90
WELL INSTALLATION: WT-104A
PHYSICAL SETTING: GRASS

DEPTH IN FEET	SOIL DEPOSITIONAL ENVIRONMENT	USCS	SOIL DESCRIPTION AND DRILLING COMMENTS	SAMPLING DATA				AIR MONITORING					
				B	N	A	R	SAMPLE TYPE INTERVAL	TIME	PIO	O ₂ LEL	CO ₂ RAD H ₂ S	
	EOLIAN	OL-SM	LOOSE, 2.5Y 3/2 V. DARK REDDISH BROWN, SILTY SAND, F-M, ORGANIC, MOIST	9				SS-1	0'-2'	16:00	0.2	20.9%	0%
1	OUTWASH	SP	10YR 4/4 SAND (MEDIUM GRAIN) - SPOON GRAVEL MOIST					3"	0.2 ppm				
									IN SPOON				
2								18					
3		SP	MEDIUM DENSE, 10YR 4/6, DARK YELLOWISH BROWN SAND (MEDIUM GRAIN) - SPOON F-M, QUARTZITIC GRAIN - F-SOME SILT TO F-FINE SAND - GRAVEL (S-M) GRANULOMETERIC, PLASTIC, MOIST	10				SS-2	2'-4'	16:07	0.2	20.9%	0%
								3"	0.2 ppm				
									IN SPOON				
4	OUTWASH	SP	MEDIUM DENSE, MOTTLED 10YR 4/6 (DK YEL BROWN) & 10YR 7/3 VERY PALE BROWN SAND (F-M, SUBANG - SUBANG GRAINED QUARTZITIC GRAIN) TO CO SAND TO F-M DOLOMITIC GRAVEL (DK BROWN & TAN SUBANG CLASTS) TO SILT, NON PLASTIC, SLIGHT COHESION DAMP	15				SS-3	4'-6'	16:26	0.2	20.9%	0%
										3"	0.2 ppm		
									IN SPOON				
6	OUTWASH	SP	MEDIUM DENSE, 10YR 6/2 PALE BROWN SAND, (F-M, SUBANG - ANG, FINE-SS, QUARTZITIC GRAIN) TO CO SAND, TO SILT TO ORGANIC FRAGMENTS TO CO GRAVEL (SUBANG TO CO CLASTS) NON- PLASTIC, NON COHESIVE, DAMP-MOIST	12				SS-4	6'-8'	16:36	0.2	20.9%	0%
										3"	0.2 ppm		
									IN SPOON				
8								18					
9		SP	LOOSE, 10YR 4/4 DARK YELLOWISH BROWN, SAND (F-M, SUBANG - ANG, FINE-SS, QUARTZITIC GRAIN) TO CO SAND, OCC. SS. DK DOLOMITIC GRAVEL (SUBANG - SUBANG) NON PLASTIC, NON COHESIVE, MOIST (WATER TABLE APPEARS TO BE 8 FEET)	5				SS-5	8'-10'	16:57	0.2	20.9%	0%
								3"	0.2 ppm				
									IN SPOON				
10	OUTWASH	SP	MEDIUM DENSE, 10YR 5/3 BROWN SAND (F-M GRAINED, FINE TO MEDIUM GRAINED, QUARTZITIC GRAIN) TO CO SAND, OCC. SS. GRAVEL (DOLOMITIC GRAIN, SUBANG) NON PLASTIC, NON- COHESIVE, SATURATED	25				SS-6	10'-12'	17:08	0.2	20.9%	0%
										3"	0.2 ppm		
									IN SPOON				
12	OUTWASH	SP	MED. DENSE - DENSE, 10YR 5/3 BROWN SAND (F-M, SUBANG - ANG, QUARTZITIC GRAIN) TO CO SAND, 2" SAND OF F-M STAINING & 12.5" NON PLASTIC NON COHESIVE, SATURATED	20				SS-7	12'-14'	17:28	0.2	20.9%	0%
										3"	0.2 ppm		
									IN SPOON				
14								15					
								SS-8	14'-16'	17:37	0.2	20.9%	0%

Donohue

BORING LOG

SOIL BORING NO.

Engineers & Architects

SITE: HIMCO DUMP PROJECT NO. 20026

BRG - 04

COMPUTER AIDED DESIGN/DRAFTING

DRILLING METHOD:

WATER LEVEL READINGS

GROUND SURFACE ELEV.: _____

4 1/4" ID HOLLOW STEM

DATE	TIME	DEPTH	CASING
------	------	-------	--------

COORDINATES: _____

AUGERS

NORTH: _____

LOG BY: R. CANNESTA

EAST: _____

DRILLER: D. ELLIS

DATE START: 11/1/90

WEATHER: OVERCAST, NW WIND, 45

PHYSICAL SETTING: ~~GLASS~~ ^{LEVEL}

DATE COMPLETE: 11/1/90

WELL INSTALLATION: WT-104A

[illegible]

Donohue

HIMCO DUMP

BORING LOG

SOIL BORING NO.

Engineers & Architects
COMPUTER AIDED DESIGN/DRAFTING

SITE: SUPERFUND PROJECT NO. 20026

BRG-05

DRILLING METHOD: CME 550

WATER LEVEL READINGS

GROUND SURFACE ELEV.: _____

4 1/4 IN ID (8 1/2 IN OD)

DATE TIME DEPTH CASING

COORDINATES: _____

HOLLOW STEM AUGER

NORTH: _____

LOG BY: R. CANNESTRA

EAST: _____

DRILLER: DAVE ELLIS

DATE START: 11-9-90

WEATHER: OVERCAST

ADJACENT
PHYSICAL SETTING: FILLED FIELD

DATE COMPLETE: _____

WELL INSTALLATION: _____

DEPTH IN FEET	SOIL DEPOSITIONAL ENVIRONMENT	USCS	SOIL DESCRIPTION AND DRILLING COMMENTS	SAMPLING DATA				BACKGROUND P10 0.4 AIR MONITORING			
				B	N	A	R	TIME	PID	O ₂ LEL	GEOR
1	ID	OL	MD, 10YR 3/2 VL GRAYISH BROWN SILTY CLAY SAND, 2% SILT, 1% GRAVEL, 2% SAND, 1% SUPERFUND, DOLOMITIC GRAVEL, MOIST	13				SS-10-2	15:03	0.4	20.6/0
								3" 0.5	0.5		
2	OUTWASH	SP	MD, 10YR 4/6 DK YELLOWISH BROWN SAND, F-M, 1% SILT, 1% GRAVEL, 1% SAND, 1% SUPERFUND, DOLOMITIC GRAVEL, MOIST	14							
3	OUTWASH	SP	MD, 10YR 4/6 DK YELLOWISH BROWN SAND, F-M, 1% SILT, 1% GRAVEL, 1% SAND, 1% SUPERFUND, DOLOMITIC GRAVEL, MOIST	18				SS-2 2-4	15:25	0.4	20.6/0
								3" 0.6	0.6		
4											
5	SP		MD, 10YR 4/6 DK YELLOWISH BROWN SAND, F-M, 1% SILT, 1% GRAVEL, 1% SAND, 1% SUPERFUND, DOLOMITIC GRAVEL, MOIST	21				SS-3 4-6	15:35	0.5	20.6/0
								3" 0.7	0.7		
6											
7	SP		MD, 10YR 4/6 DK YELLOWISH BROWN SAND, F-M, 1% SILT, 1% GRAVEL, 1% SAND, 1% SUPERFUND, DOLOMITIC GRAVEL, MOIST	21				SS-4 6-8	15:45	0.4	20.6/0
								3" 1.6	1.6		
8											
9	SWASH		MD, 10YR 5/2 BROWN SAND, F-M, 1% SILT, 1% GRAVEL, 1% SAND, 1% SUPERFUND, DOLOMITIC GRAVEL, MOIST	25				SS-5 8-10	16:00	0.6	20.6/0
								3" 2.0		4.6	PREHOLE
10	OUTWASH	SP	MD, 10YR 5/2 BROWN SAND, MEDIUM TO SILT, 1% GRAVEL, 1% SAND, 1% SUPERFUND, DOLOMITIC GRAVEL, MOIST	25				SS-6 10-12	16:25	0.8	20.6/0
								3" 3.4		5.0	
11											
12	OUTWASH	SP	MD, 10YR 5/2 BROWN SAND, MEDIUM TO SILT, 1% GRAVEL, 1% SAND, 1% SUPERFUND, DOLOMITIC GRAVEL, MOIST	25				SS-7 12-14	16:45	0.8	20.6/0
								3" 20.0+		34.4	
13											
14	OUTWASH	SP	MD, 10YR 5/2 BROWN SAND, MEDIUM TO SILT, 1% GRAVEL, 1% SAND, 1% SUPERFUND, DOLOMITIC GRAVEL, MOIST	25				SS-8 14-16	17:10	0.8	20.6/0

BEMF

Donohue

BORING LOG

SOIL BORING NO.

Engineers & Architects

SITE: HIMCO DUMP
SUPER FUND PROJECT NO. 20026

BRG-65

DRILLING METHOD: CME 550
4 1/4 IN ID (8 1/2 IN OD)
HOLLOW STEM AUGER

WATER LEVEL READINGS			
DATE	TIME	DEPTH	CASING
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____

GROUND SURFACE ELEV.: _____

COORDINATES: _____

NORTH: _____

EAST: _____

DATE START: 11-

DATE COMPLETE: _____

WELL INSTALLATION:_____

LOG BY: R. CANNESTRA
DRILLER: D. ELLIS (MATHES)
WEATHER: OVERCAST

PHYSICAL SETTING:_____

[illegible]

Donohue

BOREING LOG

SOIL BORING NO.

Engineers & Architects

SITE: FIELD
DUMP

PROJECT NO. 20026

BRG-6

DRILLING METHOD: FOLLOW STEIN AUGER

WATER LEVEL READINGS			
DATE	TIME	DEPTH	CASING
11-9	9:40	7.0'	16.0'

GROUND SURFACE ELEV.: _____
COORDINATES: _____

LOG BY: R. ANNE-FA

DRILLER: 1) ELLIS

WEATHER: OVERCAST

PHYSICAL SETTING: CLASS

NORTH: _____

EAST: _____

DATE START: 11-08-90

DATE COMPLETE: 11-08-90

WELL INSTALLATION: YES

DEPTH IN FEET	SOIL DEPOSITIONAL ENVIRONMENT	USCS	SOIL DESCRIPTION AND DRILLING COMMENTS	SAMPLING DATA				AIR MONITORING						
				B	N	A	R	SAMPLE		TIME	PID	O ₂	LEL	GIEGA
								TYPE	INTERVAL					
		OL	LOOSE, 10YR 4/2, DARK GRAYISH BROWN SILTY SAND F-M, QUARTZITIC, TR. ORGANICS, RE. GRAY	6				SS-1	0-2'	15:25	0.2	20.4%	0	
								3"	0.2 ppm					
	OUTWASH	SP-SW	LOOSE 10YR 5/6, YELLOWISH BROWN SAND M-C, MOSTLY MEDIUM, TR. SM-L SUB. END GRAVEL, MOIST	11										
			DENSE, 10YR 5/1, YELLOWISH BROWN SAND M-C, TR. SP. M. SUBANG. TR. SUB. END SOME LIMONITE STAINING, MOIST CHANGE COLOR @ 2.2 FT TO 10YR 4/2 LT BROWNISH GRAY SOME MOTTLING	14				SS-2	2-4	15:38	0.3	20.9%	0	
								3"	0.2 ppm					
		SP												
	OUTWASH		DENSE, 10YR 4/6, BROWNISH YELLOW, SAND MEDIUM, TR. F.F.C. SAND, OCC. SM-M SUB. END DOLO. GRAVEL, OCC. 1-2 mm LAMINATIONS, MOIST	20				SS-3	4-6	15:53	0.2	20.9%	0	
								3"	0.3 ppm					
		SP	DENSE 10YR 5/4 YELLOWISH BROWN, SAND MEDIUM, TR. F-C. SAND, OCCASIONAL END-SUB. END DOLO. GRAVEL SM-M, MOIST WE @ 7.3'	10				SS-4	6-8	16:18	0.2	20.9%	0	
								3"	0.8 ppm					
	OUTWASH	SP	DENSE, 10YR 5/2, BROWN, SAND, M-C CA. SAND SEAM, 1-3" @ 8.4 FT, TR. SILT OCC. SM DOLO. GRAVEL (SUB. END - SUBANG) WET & SATURATED	28				SS-5	8-10	16:38	0.2	20.9%	0	
								3"	0.2 ppm					
10	OUT WASH	SP-SW	DENSE, 10YR 5/2 BROWN, SAND, F-C GRAV. SEAM, 2" @ 10.9', TR. SILT SAND TURNING FINER NEAR TOP GRAV. SM-L SUBANG. - SUB. END DOLOMITE	44				SS-6	10-12	16:54	0.2	20.9%	0	
								3"	0.2 ppm					
			GRAY											
		SP-CP	LENS-VD, 10YR 5/1, V.M. SAND & GRAVEL SM-M, FINE GRAV. TR. L. GRAV. TR. SUB. TR. FER. SAND, TR. SUB. SOLVENT ODOR SATURATED, OCC. BLACK GRAV. CL.	50				SS-7	12-14	17:20	0.2	20.9%	0	
								3"	0.2 ppm					
		SP	DENSE 10-6.5/1, GRAY SAND (CA. 5 SM) SUB. END - SUB. END F.F.C. SAND, GRAV. SUBANG. - SUB. END, SOLVENT ODOR SAT	58				SS-8	14-16	17:30	0.2	20.9%	0	
								3"	0.2 ppm					

Donohue

BORING LOG

SOIL BORING NO.

Engineers & Architects

SITE: 5-MED PROJECT NO. 200

BRG-6

DRILLING METHOD: HOLLOW STEM AUGER

[illegible]

GROUND SURFACE ELEV.: _____
COORDINATES: _____

NORTH: _____

EAST: _____

LOG BY: R. CANNES-4A

DRILLER: D. ELLIS

WEATHER: CLEAR & COOL

PHYSICAL SETTING: _____ WELL INSTALLATION: _____

WELL INSTALLATION: _____

[illegible]

APPENDIX B
WELL CONSTRUCTION DIAGRAMS

Donohue

Water Table Well Installation Diagram

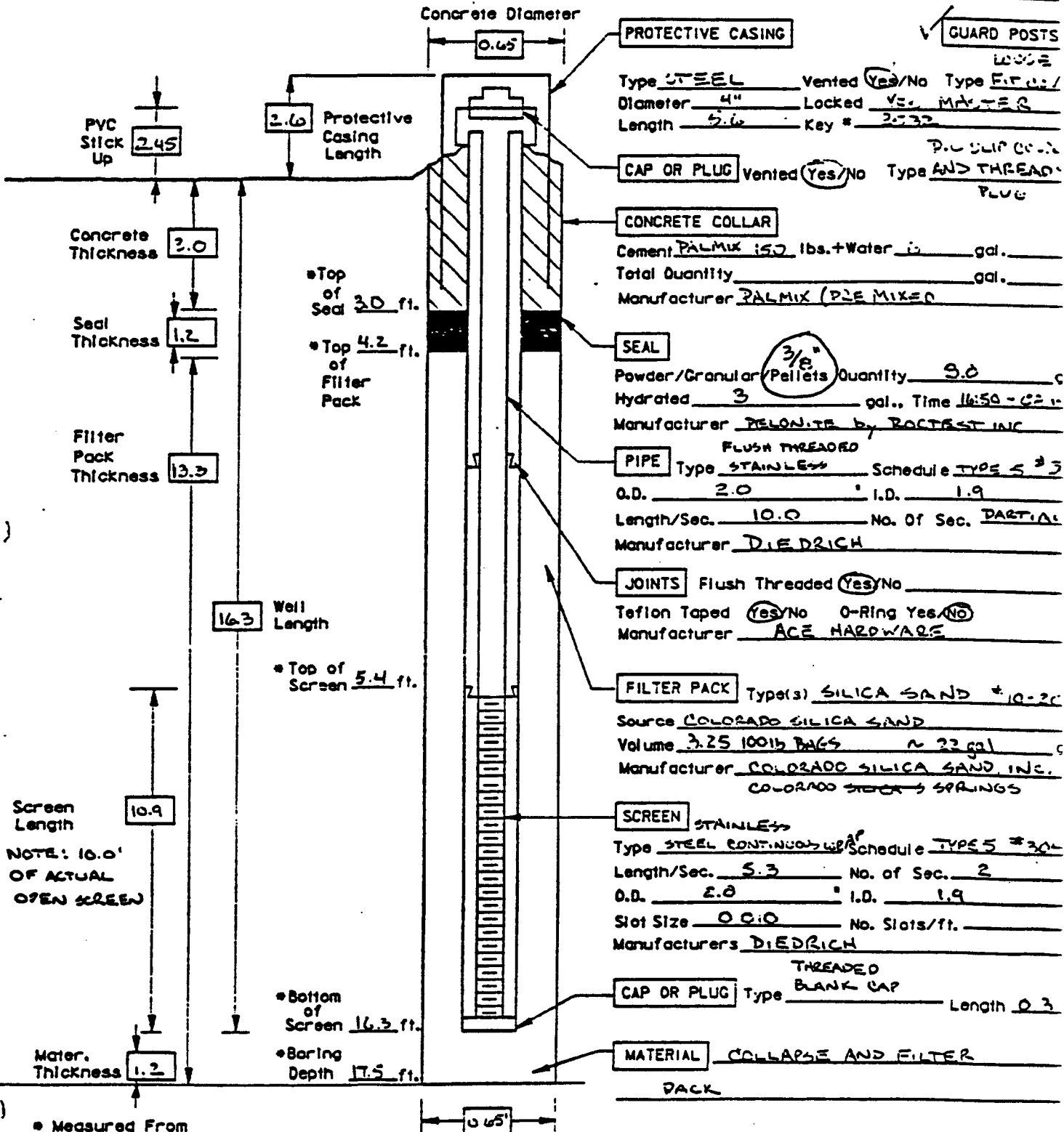
Form

Site: WIMCO DUMPDate: NOVEMBER 17, 1990

Inspected By: _____

Project No. 20026, C-63Well No. WT-101AEngineers & Architects
COMPUTER AIDED DESIGN/DRAFTING

Driller/Contractor _____



NOTE: 10.0'
OF ACTUAL
OPEN SCREEN

• Measured From
Ground Surface

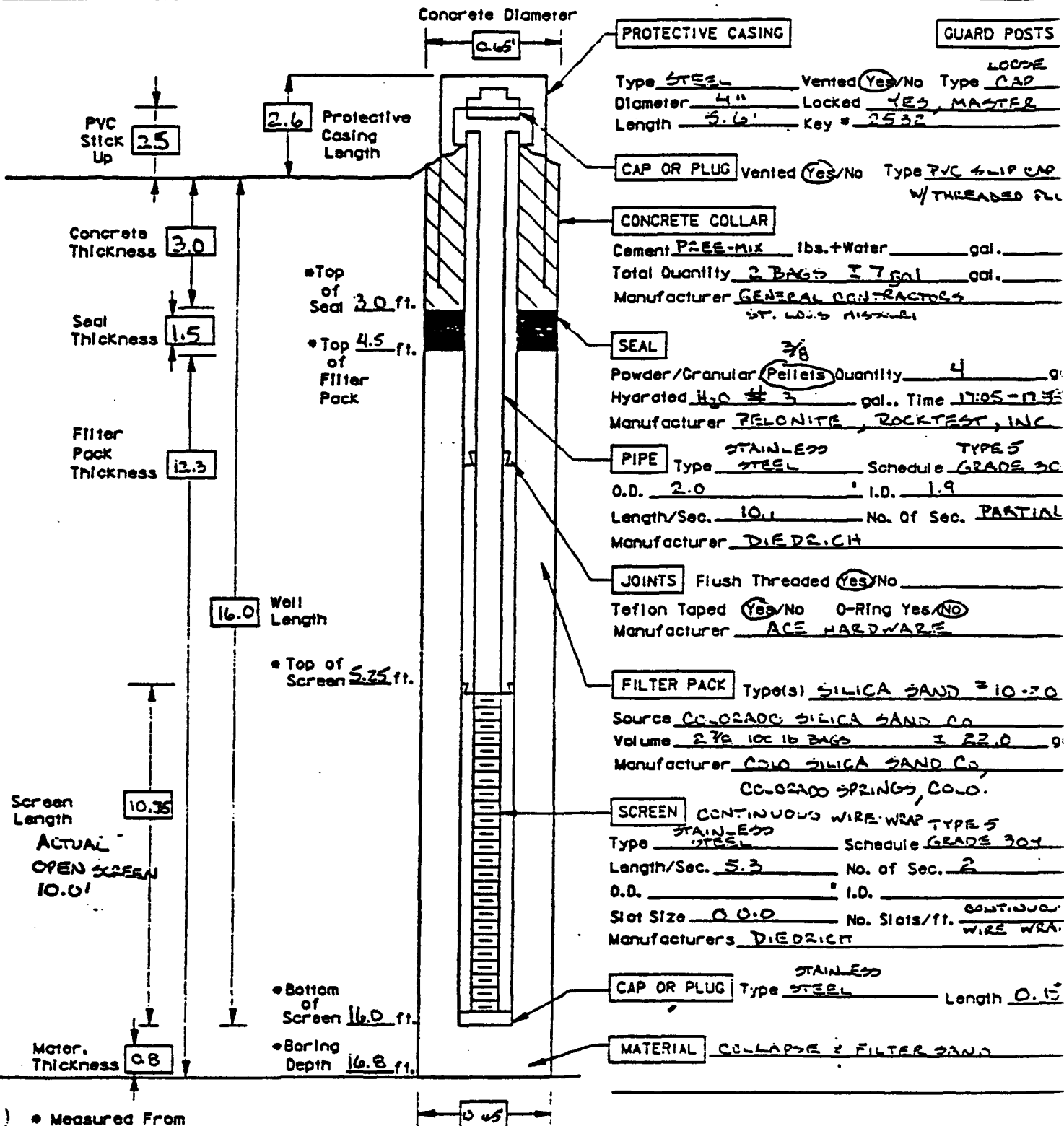
WATER SOURCE ELKHART MUNICIPAL WATER SUPPLY

Notes: _____

Donohue

Water Table Well Installation Diagram

Form

Site: HIMCO PUMP SITE Date: 11 -Inspected By: R. CANNESTRA Project No. 20026 Well No. WT-102AEngineers & Architects
COMPUTER AIDED DESIGN/DRAFTINGR. CannestraDriller/Contractor D. ELLIS / MATHES

Donohue

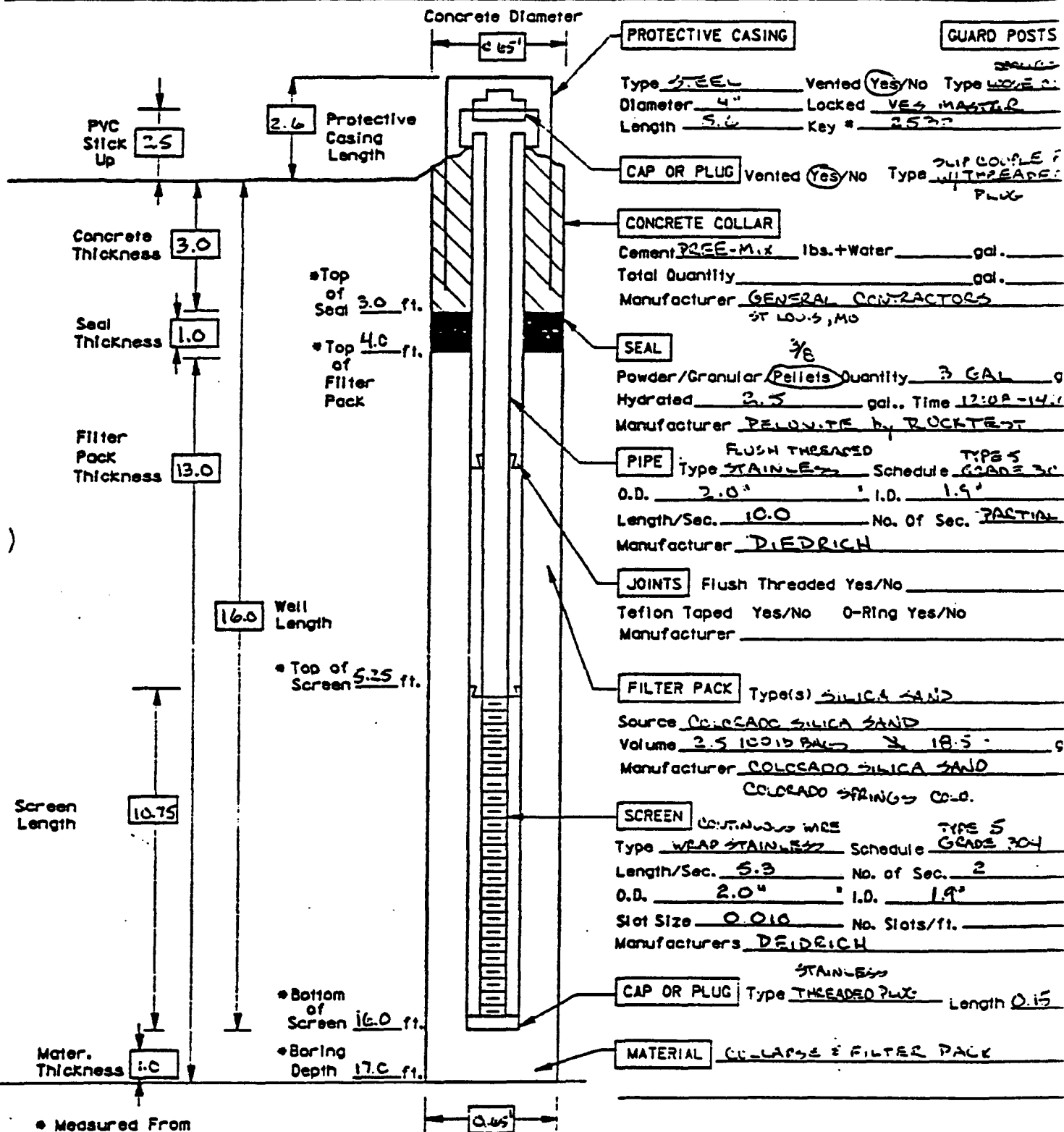
Water Table Well Installation Diagram

Form

Site: HIMCO DUMPDate: 11/11/90Inspected By: R. CANESTRAProject No. 260212Well No. WT-103A

Engineers & Architects

COMPUTER AIDED DESIGN/DRAFTING

Driller/Contractor D. ELLIS / MATHEIS

• Measured From Ground Surface

WATER SOURCE ELKHART MUNICIPAL WATER PLANT

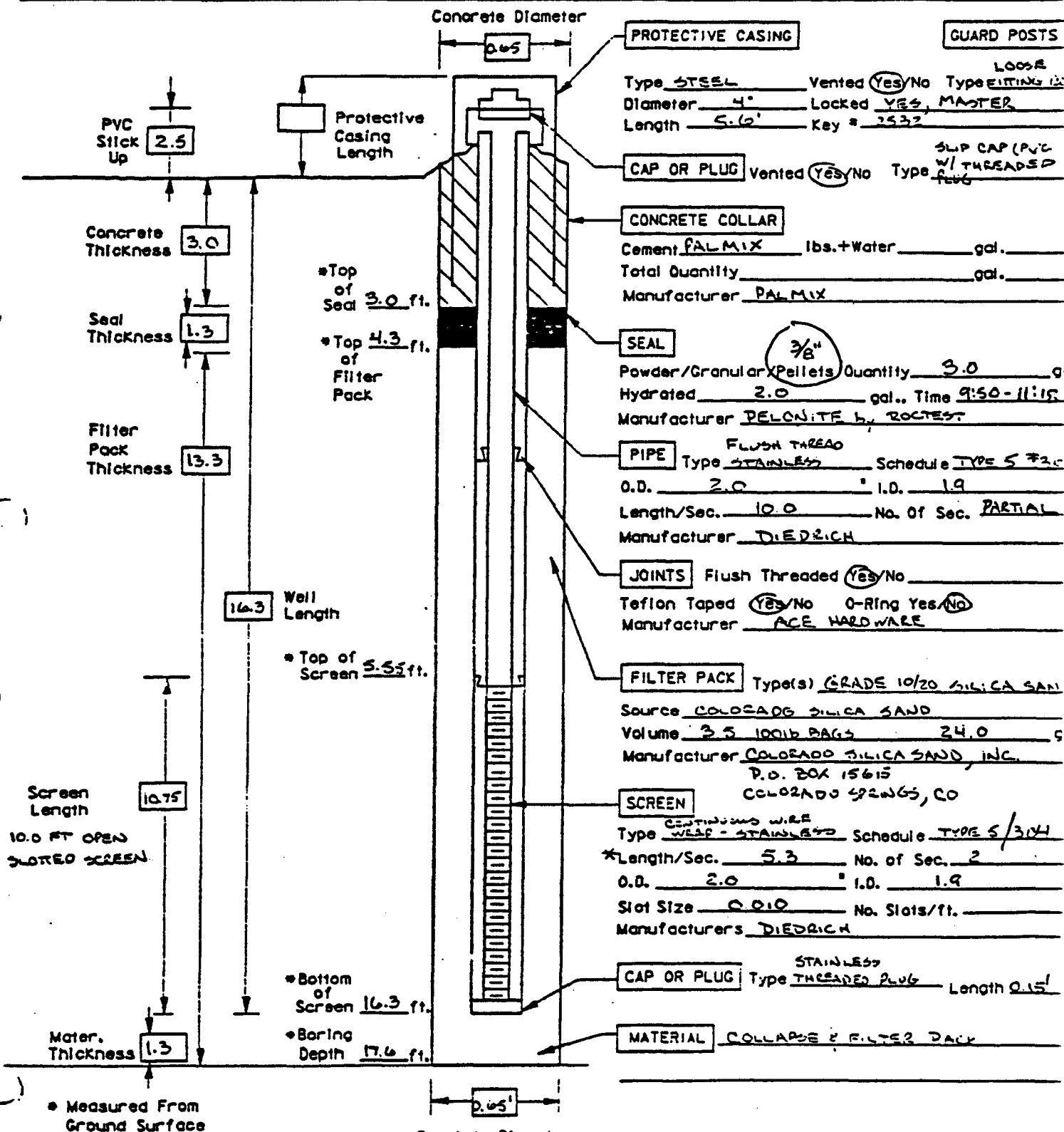
Notes:

Donohue

Water Table Well Installation Diagram

Form

Site: HIMCO DUMP SITE Date: 11/12/82
Inspected By: R. CANESTRA Project No. 20024-023 Well No. WT-104A
Engineers & Architects
COMPUTER AIDED DESIGN/DRAFTING
Driller/Contractor D. ELLIS / MATHE

WATER SOURCE ELKHART MUNICIPAL WATER PLANTNotes: WATER LEVEL 9.9 F FROM 65 TOWN HALL ADDRESS

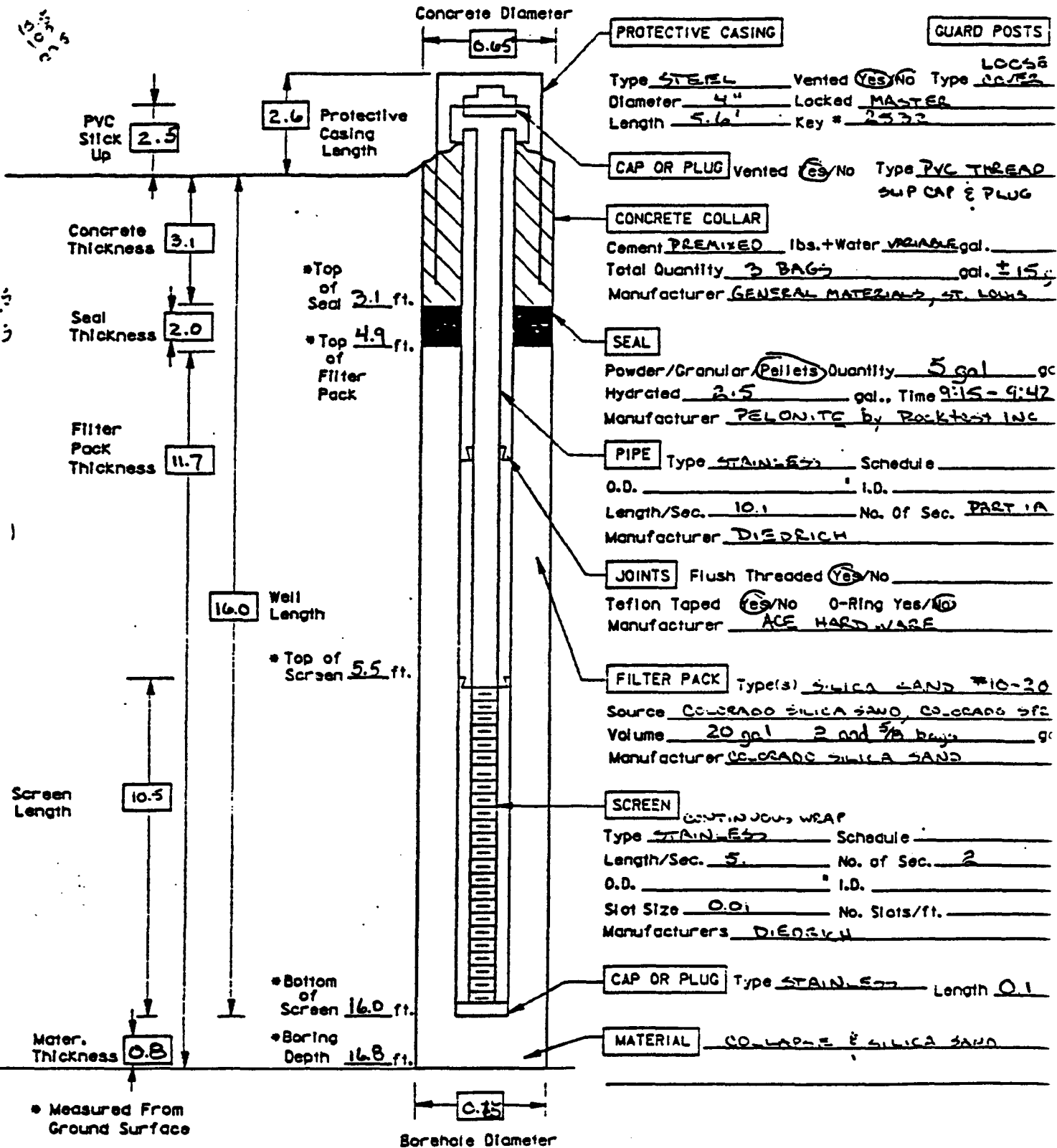
* 10.0 FT OPEN SLOTTED SCREEN

© COMPLETION 11/12/82 2:00 PM 1982

Donohue

Water Table Well Installation Diagram

Form 10

Site: HIMCO DUMPDate: 11/10/90Inspected By: R. CANNESTRAProject No. 20026Well No. WT-103AEngineers & Architects
COMPUTER AIDED DESIGN/DRAFTINGDriller/Contractor D. ELLIS/MATHES

WATER SOURCE

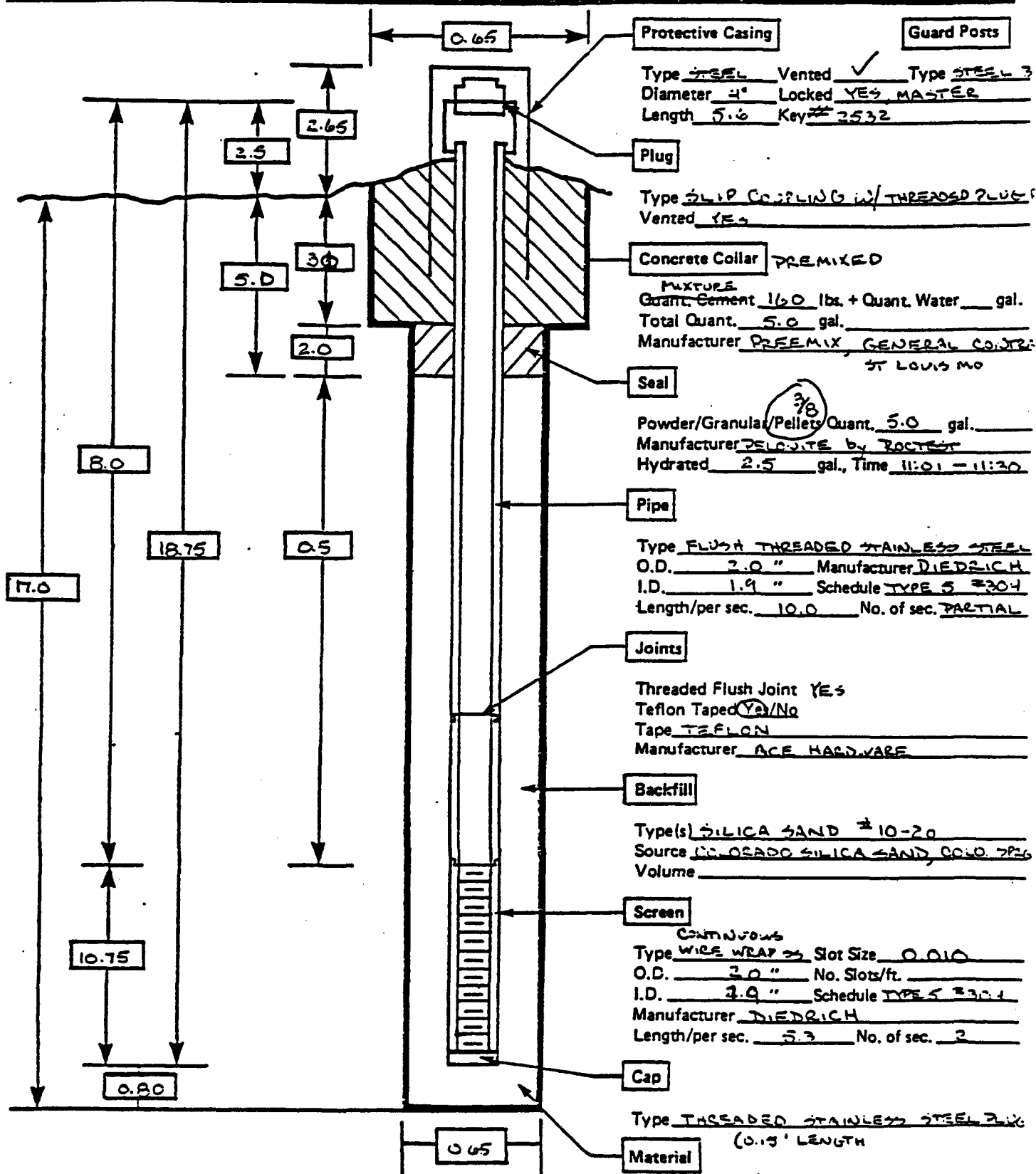
Notes: WATER @ 7.5' TWO AUGERSSEAL HYDRATED 25-30 MIN BEFORE PLACING CONCRETE CAP

Donohue

OBSERVATION WELL INSTALLATION DIAGRAM

Well No. WT 106A

Site: HIMCO DUMP, ELKHART, IN Date: NOVEMBER 9, 1990

By: R. CANESTRA/MATHES Project No. 20026.023

Notes: Water Source ELKHART MUNICIPAL WATER WORKS

WATER LEVEL IN BOREHOLE PRIOR TO INSTALLATION ~7.0 FEELING

APPENDIX C
DAILY ATMOSPHERIC MONITORING LOGS

Engineers & Architects

Atmospheric Monitoring Log

Field Safety

Project Site HIMCO DUMP Health & Safety Officer A. KIRYKOW.CZ

Health & Safety Officer A. KIRYKOW.CZ

Project Number 200216

Level of Protection

Level of Action

Description of site (weather, temp, soil conditions) Ptly CLDY, LT BREEZE

[illegible]

Additional Notes:

Signature Robert Connors

Date 11/11/90

Engineers & Architects

Atmospheric Monitoring Log

Field Safety

Project Site HIMCO DUMP SITE Health & Safety Officer A. KIRYKOWICZ

Project Number 20026 Level of Protection D

Level of Action _____

Description of site (weather, temp, soil conditions) CLEAR, 35-45, SOILS MOIST-SATURATED
HN-2 BKGD O.W. GASTECK

[illegible]

Additional Notes: _____

Signature R. Connors Date 11/10/96

Date 11/10/96

Engineers & Architects

Atmospheric Monitoring Log

Field Safety

Project Site HIMCO DUMP SUPERFUND SITE Health & Safety Officer ANYA KIRYKOWICZ

Project Number 20026 Level of Protection C

Level of Action C (DURING WELL INSTALLATION @ WT-106A)

Description of site (weather, temp, soil conditions) OVERCAST, 35-46°

[illegible]

Additional Notes: _____

Signature Robert B. Cannestra Date 11-9-90

Date 11-9-90

~~71~~ ~~71~~ ~~71~~ x 2

Date Nov 13, 1990

ORIGINAL

TECHNICAL MEMORANDUM NUMBER 14

DATE: May 1, 1991

TO: Vanessa Harris, Site Manager

CC: Marcia Kuehl, RI Lead
Roman Gau, Project Manager
Mike Crosser, TSQAM

FROM: Anya Kirykowicz
Dave Richardson

SUBJECT: EPA ARCS Region V Contract No. 68-W8-0093
EPA Work Assignment No. 17-5L4J
Himco Dump RI/FS
Donohue Project No. 20026.024

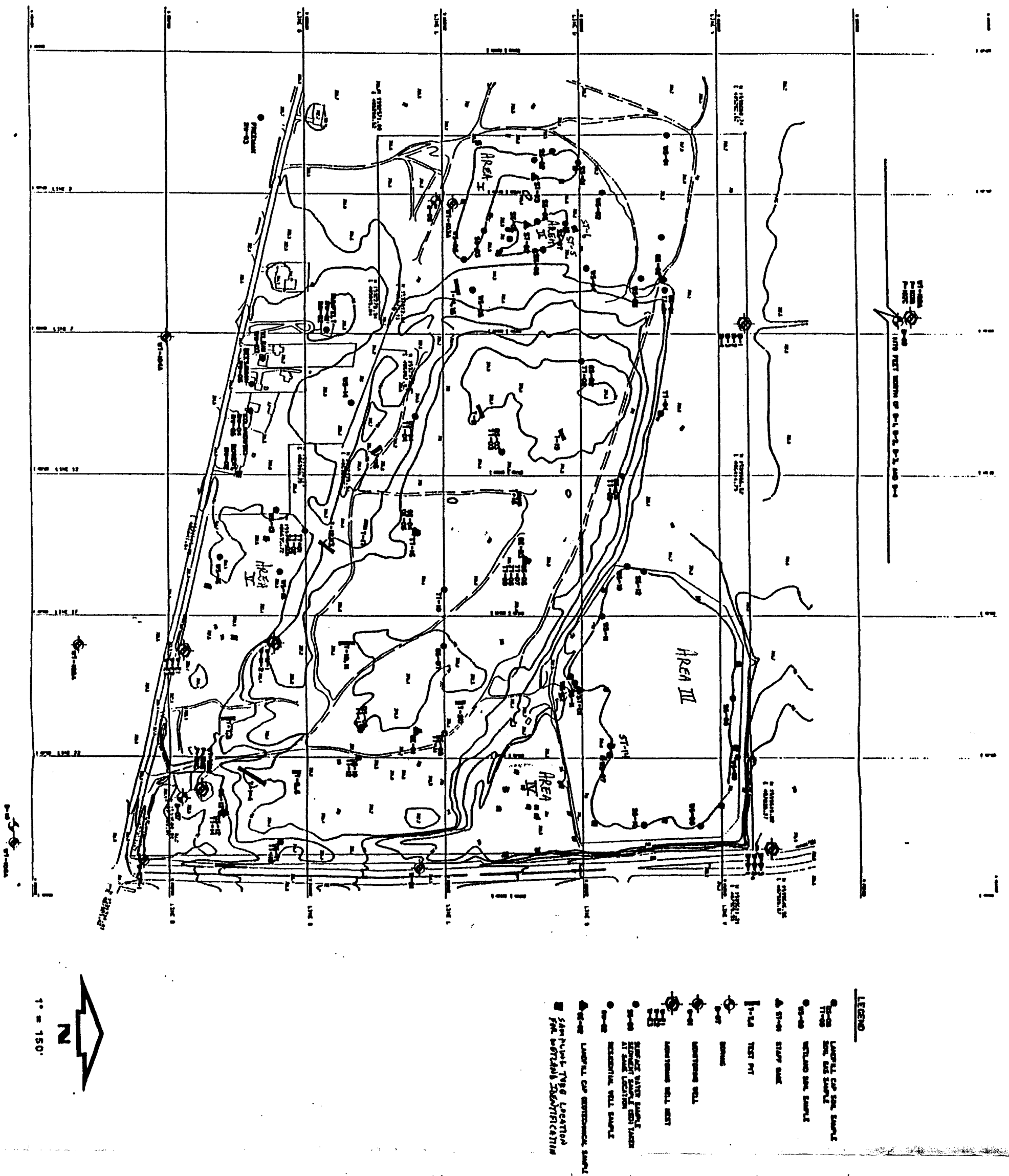
WETLANDS ASSESSMENT AND IDENTIFICATION

Introduction

On October 22, 23, and 24, 1990 Donohue & Associates, Inc. conducted an on-site wetlands assessment and identification at the Himco Dump Superfund Site as part of the RI Work Plan. The delineation was conducted by Dave Richardson and Anya Kirykowicz. Three suspected wetland areas were designated as Northwest Wetland Area, Wetland Remnant, and Gravel Pit Wetland Area. The location of these areas is presented in Figure 1.

Methods

As outlined in Section 4.6.1 of the Final Field Sampling Plan, Himco Dump RI/FS Elkhart, Indiana, three essential characteristics were used to identify wetland areas. These characteristics are: hydric soils, wetland hydrology, and hydrophytic vegetation. These characteristics and their technical criteria are described below. The approximate boundaries between wetland and upland areas were identified using methods prescribed in the "Federal Manual for Identifying and Delineating Jurisdictional Wetlands" (Federal Interagency Committee for Wetland Delineation, 1989). The Disturbed Area Wetland Determination Method was used, with the hydrophytic vegetation assessment taking the lead. Sampling tube cores were used to examine the soil profile for hydric soils and wetland hydrology. An assessment of hydrophytic vegetation was made at each sampling tube core. The following equipment was used: soil sampling tube, dead blow hammer, site map, field notebook, Munsell Soil Color Charts, flagging tape, wooden lathe, camera, plastic bags, field guides for plant identification, USGS topographic map, Hydric Soils of the United States List, and an aerial photograph.



Wetland Hydrology

Wetland hydrology is defined as permanent or periodic inundation or prolonged soil saturation sufficient to create anaerobic conditions in the soil. The wetland hydrology criterion is met if a site is inundated or saturated to within 1.5 feet below the surface, based on the soil drainage characteristics, for at least one consecutive week during the growing season in an average rainfall year (Federal Interagency Committee for Wetland Delineation, 1989). This criterion is the least exact and the most difficult to assess in the field.

Hydric Soil

Hydric soils are defined as soils that are saturated, flooded or ponded long enough during the growing season to develop anaerobic conditions in the upper part (U.S.D.A. Soil Conservation Service, 1987). An area has hydric soils when the National Technical Committee for Hydric Soils criteria are met. These criteria relate to soil types, soil drainage characteristics, water table levels and frequency of flooding or ponding.

Hydrophytic Vegetation

Hydrophytic, or wetland, vegetation is defined as macrophytic plant life growing in water, soil or on a substrate that is at least periodically deficient in oxygen as a result of excessive water content (Federal Interagency Committee for Wetland Delineation, 1989). The U.S. Fish and Wildlife Service publishes a list of plant species that occur in wetlands by region. Each species in the list is given an indicator status reflecting the range of estimated probability that it may occur in a wetland versus non-wetland area across its entire distribution. These indicator categories are listed below:

- o Obligate Wetland (OBL). Occur almost always (estimated probability >99%) under natural conditions in wetlands.
- o Facultative Wetland (FACW). Usually occur in wetlands (estimated probability 67%-99%), but occasionally found in non-wetlands.
- o Facultative (FAC). Equally likely to occur in wetlands or non-wetlands (estimated probability 34%-66%).
- o Facultative Upland (FACU). Usually occur in non-wetlands (estimated probability 67%-99%), but occasionally found in wetlands (estimated probability 1%-33%).
- o Obligate Upland (UPL). Occur in wetlands in another region, but occur almost always (estimated probability >99%) under natural conditions in non-wetlands in the region specified. If a species does not occur in wetlands in any region, it is not on the National List.

The hydrophytic vegetation criterion for wetland identification is met when more than 50 percent of the dominant species at a given site are obligate, facultative wetland or facultative species.

Deviations

The three suspected wetland areas were renamed in the field. The Northwest Wetland Area was divided into Area I and Area II. The Gravel Pit Wetland was designated Area III. The Wetland Remnant was designated Area V. An area immediately south of the gravel pit was designated Area IV. This area was added to the field investigation based on visual observations. The study areas are shown on Figure 1.

Summary of Results

Sampling tube cores were used to examine the soil profile for hydric soils and wetland hydrology. A total of thirty-nine sites were chosen for soil sampling, representing the various conditions on the site. The vegetation was sampled at these 39 sites. Some of the plant species were not identified in the field but were collected, tagged, and identified off-site. Field work was conducted in late autumn, making identification difficult. The locations for the 39 sites are shown on Figure 1.

The only area identified as a wetland was Area IV. All of the other locations were non-wetland based on existing normal conditions or due to fill materials that were placed in close proximity to open water.

Hydrophytic vegetation identified in these wetland areas included: *Typha angustifolia* (Narrow-leaf Cattail-OBL), *Carex* sp. (Sedge sp.), *Equisetum hyemale* (Rough Horesetail-FACW), *Solidago gigantea* (Giant Goldenrod-FACW), *Salix* sp. (Willow sp.), *Aster novae-angliae* (New England Aster-FACW), and other *Solidago* sp. and *Aster* sp.

AK:llw

A/R/HIMCO/AB9

TECHNICAL MEMORANDUM - NO 15

ORIGINAL

DATE: January 25, 1991

TO: Vanessa Harris - Site Manager

CC: Marcia Kuehl - RI Lead
Roman Gau - Project Manager
Mike Crosser - TSQAM

FROM: Tom Puchalski
Anya Kirykowicz

SUBJECT: EPA ARCS Region V Contract No. 68-W8-0093
EPA Work Assignment No. 17-5L4J
Donohue Project No. 20026.024
Himco Dump RI/FS

WETLAND SOIL SAMPLING

Introduction

Sixteen soil samples were collected from three suspected wetland areas at the Himco Dump Site on October 21, 22, 23, and November 7, 1990; six from the Northwest Wetland Area, four from the Wetland Remnant, and six from the Gravel Pit Wetland Area (Figure 1). These soil samples were collected to investigate for possible soil contamination associated within these possible wetland areas. Sampling locations were selected to include what were suspected to be areas of most likely contamination. These areas included suspected wetland areas receiving drainage from the landfill cover as determined by aerial photography and field observations, and areas of apparent stressed vegetation. Soil samples were composited at each location from 0 to 18 inches or shallower where the auger met with refusal. Wetland soil sampling for chemical analysis was performed by Eric Slusser and Tom Puchalski of Donohue & Associates, Inc.

Methods

Section 4.6.4 of the Final Field Sampling Plan, Himco Dump RI/FS, Elkhart, Indiana, describes the wetlands soil sampling procedures. A hand auger was used to collect the sample at each location. After gathering soil to the required 18-inch depth, grab samples were retrieved from the sample bowl and put in 4-oz. glass jars for volatile analysis. These jars were filled with no head space remaining. The remaining soil was classified (USCS), the color identified using a Munsell Color Chart, and examined for obvious signs of contamination. This information was recorded on a soils data form (Appendix A). A stainless steel spoon was used to stir the remaining soil until a homogeneous mixture was obtained. The mixture was divided into four equal size quadrants. Portions were taken from each of the four quadrants to fill the remaining sample jars.

The hand auger, mixing spoon, and composite bowl were decontaminated between sampling points using an alconox and tap water wash, a tap water rinse, an isopropanol rinse, and two deionized or distilled water rinses. Isopropanol rinses were captured in a 5-gallon bucket and covered for eventual discharge into the on-site frac tank. A photograph was taken of each wetland soil sampling location.

Deviations

The sixteen sampling locations were selected prior to the wetland assessment and identification. Only one of the locations designated as a wetland sample (WS-#) was from a wetland location. WS-07 was located near ST-14 (sampling tube-14) of the wetland identification procedures. ST-14 met all three of the wetland criteria - hydric soil, hydrology and hydrophytic vegetation.

A stainless steel hand auger was used to collect the soil sample rather than a sampling tube as was described in the sampling plan. Besides being more labor intensive, a sampling tube does not collect sufficient soil volume to fill the required sample jars. Several pushes of the tubes would have been required at each sampling location. With the hand auger, sufficient sample volume was collected with one run from 0 to 18 inches.

Summary of Results

Sixteen soil samples for chemical analysis were collected in suspected wetland areas. Sample locations are provided in Figure 1. Wetland Soil Data forms are provided in Appendix A. A summary of wetland soil sampling locations, suspected wetland area, and materials encountered is provided in Appendix B.

TP:AK:ds

A/R/HIMCO/AB3

APPENDIX A
SOILS DATA FORMS

Donohue

Soils Data Form

Soil Sample Area Northwest RemrSoil Subsample WS-1

Engineers & Architects & Scientists

Site Himco DumpProject No. 20026.023DATE 10/21/90TIME 1625COLLECTOR TOM PUCHALSKI
ERIC SLOSSERSAMPLE DEPTH 0-18"PHYSICAL DESCRIPTION OF SUBSAMPLING LOCATION: North end of
Northwest wetland remnant in grassy area.DESCRIPTION OF SUBSAMPLE: 10 YR 4/1 Dark grey silty sand (SM), low
col, moistANY OTHER CHARACTERISTICS OF NOTE: 1" of moss at surface; roots to
3"

Donohue

Soils Data Form

Soil Sample Area Northwest RemnantSoil Subsample WS-2

Engineers & Architects & Scientists

Site Himco DumpProject No. 20026.023DATE 10/21/90TIME 1645COLLECTOR TOM DUCHALSKI
ERIC SLUSSERSAMPLE DEPTH 0-18"

_____PHYSICAL DESCRIPTION OF SUBSAMPLING LOCATION: South end of
Northwest Remnant in prairie.

_____DESCRIPTION OF SUBSAMPLE: 10YR 6/1 Light gray silty sand (3M)
low coh, moist

_____ANY OTHER CHARACTERISTICS OF NOTE: _____

Donohue

Soils Data Form

Soil Sample Area Northwest CornerSoil Subsample US-03

Engineers & Architects & Scientists

Site Hinco DumpProject No. 20026.025DATE 10/22/90TIME 857COLLECTOR ERIC SLUSSER
DOROTHEA DOWNS
TOM PUCHALSKISAMPLE DEPTH 0-6"PHYSICAL DESCRIPTION OF SUBSAMPLING LOCATION: Low area 40 yards
south of tree line & 50 yards west of landfill filled & capped
area.DESCRIPTION OF SUBSAMPLE: 10 YR 3/1 Very dark grey, Silty Sand (sml
fine grained 60% sand 40% silt, moist, low coh, roots.ANY OTHER CHARACTERISTICS OF NOTE: Refusal at gravel layer
6" below surface.

Donohue

Soils Data Form

Soil Sample Area Northwest RemnSoil Subsample WS-04

Engineers & Architects & Scientists

Site Himco DumpProject No. 20026.023DATE 10/22/90TIME 9:40COLLECTOR Eric Slusser
Dorothea DownsSAMPLE DEPTH 0-18"PHYSICAL DESCRIPTION OF SUBSAMPLING LOCATION: Flat^{low} area30 yds yards ^{east} of tree line and 60 yards west of landfill fill
and capped are.DESCRIPTION OF SUBSAMPLE: 7.5 YR 5/4 Brown silty sand 0-10"
(SM) fine grained. 65% sand 35% silt moist, low coh roots upper
0.5' 10-18" grey 7.5 YR 5/0 Grey silty sand (SM) fine grained
65% sand, 35% silt low coh, moist - ^{sat} H₂S smellANY OTHER CHARACTERISTICS OF NOTE: H₂S smell in grey silty
sand

Donohue

Soils Data Form

Soil Sample Area Northwest RemSoil Subsample WS-05

Engineers & Architects & Scientists

Site Himes DumpProject No. 29026.023DATE 10/22/93TIME 10:16COLLECTOR Eric Slusser
Dorothea DownsSAMPLE DEPTH 0-18"PHYSICAL DESCRIPTION OF SUBSAMPLING LOCATION: Flat area in
40 yard east of pond 50 yards west of landfill filled and capped
area. large hardy cattails presentDESCRIPTION OF SUBSAMPLE: 0-12" 7.5 YR S/4 Brown silty sand (SM)
Fine grain 65% sand 35% silt moist low coh roots approx 2-3"
12-18 10 YR 3/4 V. Dark Gray silty sand (SM) 65% sand 35% silt.
Wet low cohANY OTHER CHARACTERISTICS OF NOTE: H₂S smell from V. Dark Gray silty
refused refusal between 19-20"

Donohue

Soils Data Form

Soil Sample Area Northwest DamSoil Subsample WS-06

Engineers & Architects & Scientists

Site Himco DumpProject No. 20026-023DATE 10/23/90TIME 825COLLECTOR TOM PUCHALSKI
ERIC GLUSSERSAMPLE DEPTH 0-12"PHYSICAL DESCRIPTION OF SUBSAMPLING LOCATION: East shore of
6 sided pond at southeast end of pond at midpoint, 6" from
water edge.DESCRIPTION OF SUBSAMPLE: 10 54R 5/4 Yellowish Brown, fine grained
silty sand (SM).

ANY OTHER CHARACTERISTICS OF NOTE: _____

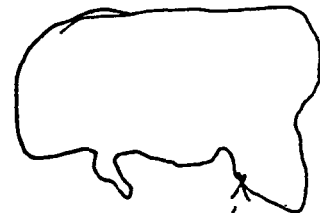
Donohue

Soils Data Form

Soil Sample Area QuarrySoil Subsample WS-07

Engineers & Architects & Scientists

Site Himco DumpProject No. 20026-02DATE 10/21/90TIME 955 AMCOLLECTOR TOM PUCHALSKI
ERIC SLUSSERSAMPLE DEPTH 0-14"

_____

WS-07

PHYSICAL DESCRIPTION OF SUBSAMPLING LOCATION: Southeast corner
of quarry pond in 4" of clear water in cattails

_____DESCRIPTION OF SUBSAMPLE: 5Y, 3/1 Very dark grey fine grained silty
sand (SM), very green, trace small shells.

_____ANY OTHER CHARACTERISTICS OF NOTE: Slight H₂S odor

Donohue

Soils Data Form

Soil Sample Area QuarrySoil Subsample WS-08

Engineers & Architects & Scientists

Site Himco DumpProject No. 20026-023DATE 10/21/90TIME 1051 AMCOLLECTOR TOM PUCHALSKI
ERIC SLUSSERSAMPLE DEPTH 0-18"PHYSICAL DESCRIPTION OF SUBSAMPLING LOCATION: Northeast corner
of quarry pond in 8" of clear water in cattail area.DESCRIPTION OF SUBSAMPLE: 54, 3/1 very dark grey fine grained silty
sand (SM), angular grains, trace of small shellsANY OTHER CHARACTERISTICS OF NOTE: H₂S odor.

Donohue

Soils Data Form

Soil Sample Area QuarrySoil Subsample WS-09

Engineers & Architects & Scientists

Site Himco DumpProject No. 20026.02EDATE 10/21/90TIME 1122 AMCOLLECTOR TOM DUCHALSKI
ERIC SLUSSERSAMPLE DEPTH 0-18"

_____PHYSICAL DESCRIPTION OF SUBSAMPLING LOCATION: On north shore of
quarry 5 feet north of water edge in horse tails 0-4" gravel \approx $\frac{1}{4}$ - $\frac{1}{2}$ " s
sand grading to gravelly sand 4"-18"

_____DESCRIPTION OF SUBSAMPLE: 10 YR 5/3 Brown ^{sep 10/21/90} sandy gravelly sand (SW)
20% $\frac{1}{8}$ " sharp grl, sand-angular fn to md grained

_____ANY OTHER CHARACTERISTICS OF NOTE: _____

Donohue Soils Data Form Soil Sample Area Quarry
Soil Subsample WS-10

Engineers & Architects & Scientists Site Himco Dump Project No. 20026.033

DATE 10/21/90

TIME 1412 PM

COLLECTOR TOM PUCHALSKI
ERIC SLUSSER

SAMPLE DEPTH 0-18"

PHYSICAL DESCRIPTION OF SUBSAMPLING LOCATION: Middle of west
bank in 8" water. Edge of cattails. 1 foot off shore

DESCRIPTION OF SUBSAMPLE: ^{SEP}54 10YR 5/3 Brown fine grained sand
(SP)

ANY OTHER CHARACTERISTICS OF NOTE: _____

Donohue

Soils Data Form

Soil Sample Area QuarrySoil Subsample WS-116 Dup

Engineers & Architects & Scientists

Site Himlo DumpProject No. 20026.02

DATE

10/21/98

TIME

1438

COLLECTOR

TOM DUCHALSKI
ERIC SLOSSER

SAMPLE DEPTH

0-18"PHYSICAL DESCRIPTION OF SUBSAMPLING LOCATION: South shore of
quarry 70 yards east of west shore 1' off shore.DESCRIPTION OF SUBSAMPLE: 10YR 5/3 Brown mixed with 5Y 3/1
very dark grey finegrained sand-silty (SM) with trace 1/2" shrd gnlANY OTHER CHARACTERISTICS OF NOTE: H₂S odor in grey areas. Roots
inter-twining to form a cluster at surface to 3".

Donohue Soils Data Form Soil Sample Area Quarry
Soil Subsample WS-12

Engineers & Architects & Scientists Site Himco Dump Project No. 20026023

DATE 10/21/90

TIME 1550

COLLECTOR TOM PUCHALSKI
ERIC SLIKER

SAMPLE DEPTH 0-18"

PHYSICAL DESCRIPTION OF SUBSAMPLING LOCATION: South shore of
quarry towards south edge of bay at base of steep bank
in 6" of water.

DESCRIPTION OF SUBSAMPLE: Multi-colored gravel $\approx 1/2$ " diam. 10%
fine sand

ANY OTHER CHARACTERISTICS OF NOTE: _____

Donohue

Soils Data Form

Soil Sample Area South Wetland AreaSoil Subsample WS-13

Engineers & Architects & Scientists

Site Himco DumpProject No. 20026.025

DATE

10/23/90

TIME

1355

COLLECTOR

TOM PUCHALSKI
ERIC SLUSSER

SAMPLE DEPTH

0-18"PHYSICAL DESCRIPTION OF SUBSAMPLING LOCATION: Southwest corner
of wetland remnant near Klein property 100' north in grassy areaDESCRIPTION OF SUBSAMPLE: 10 yr 3/2 Very Dark Greyish Brown Silty
Soil (SM) 30% silt 70% fine grained angular sand, roots to 3"
low oak, moist, grass at surface

ANY OTHER CHARACTERISTICS OF NOTE:

Donohue

Soils Data Form

Soil Sample Area South Wetland

Soil Subsample WS-14

Engineers & Architects & Scientists

Site Himco Dump

Project No. 20026.023

DATE 10/23/90

TIME 1418

COLLECTOR TOM PUCHALSKI
ERIC SLUSSER

SAMPLE DEPTH 0-8" - Refusal
at gravel layer

PHYSICAL DESCRIPTION OF SUBSAMPLING LOCATION: West edge of
South wetland remnant 15 yards south of old rail road
grade in low grassy area.

DESCRIPTION OF SUBSAMPLE: 10YR 4/4 Dark Yl.ish Brown silty sand
(SM) 70% fine grained angular sand 30% silt, low coh,
moist

ANY OTHER CHARACTERISTICS OF NOTE: _____

Donohue

Soils Data Form

Soil Sample Area San Hill Wetland
Soil Subsample US-15 Remn

Engineers & Architects & Scientists

Site Hinco DumpProject No. 20026-02DATE 10/23/96TIME 1431COLLECTOR TOM PUCHALSKI
ERIC SLUSSERSAMPLE DEPTH 0-6" - Refusal at
gravel layer 2" strongPHYSICAL DESCRIPTION OF SUBSAMPLING LOCATION: 40 yards south of
old railroad grade in open grassy area near east edge of remnant - 100
yards ~~from~~ west of east border
getDESCRIPTION OF SUBSAMPLE: 1042 3/2 Very Dark Grayish Brown
silty sand (SM) 70% fn grn ang sld, 30% silt, low coh,
moistANY OTHER CHARACTERISTICS OF NOTE: Methane odor in air

Donohue

Soils Data Form

Soil Sample Area South Wetland RdSoil Subsample WS-16

Engineers & Architects & Scientists

Site Himco DumpProject No. 20026.023DATE 10/23/90TIME 1455COLLECTOR TON PUCHARSKI
ERIC SLUSSEKSAMPLE DEPTH 0-8"

_____PHYSICAL DESCRIPTION OF SUBSAMPLING LOCATION: 40 yards north
of road in brushy grassy area of southeast portion of
southeast wetland remnant.

_____DESCRIPTION OF SUBSAMPLE: 10 YR 3/1 Very dark grayish brown
silty sand (SM) 70% fr fine gray sand, 30% silt, low clay
moist, roots to 2".

_____ANY OTHER CHARACTERISTICS OF NOTE: _____

APPENDIX B

APPENDIX B

<u>WETLAND SOIL SAMPLE NUMBER</u>	<u>SUSPECTED WETLAND AREA LOCATION</u>	<u>SAMPLE CHARACTERISTICS</u>
01	*	Dark grey silty sand. Moss at surface, roots to 3".
02	*	Light grey silty sand
03	*	Very dark grey silty sand. Refusal at gravel layer (6" below surface).
04	*	Grey silty sand; H ₂ S odor.
05	*	Dark grey silty sand; H ₂ S odor (refusal at 20").
06	I	Yellowish brown silty sand.
07	III	Very dark grey silty sand. Trace small shells; H ₂ S odor.
08	III	Very dark grey silty sand. Trace small shells; H ₂ S odor.
09	III	Brown gravelly sand.
10	III	brown fine grained sand.
11	III	Brown mixed with very dark grey silty sand H ₂ S odor in grey areas.
12	III	Multi-colored gravel and fine sand.
13	V	Very dark greyish brown silty sand.
14	*	Dark yellowish brown silty sand.
15	V	Very dark greyish brown silty sand.
16	V	Very dark greyish brown silty sand.

* Located outside of suspected wetland area

A/R/HIMCO/AB3

ORIGINAL

TECHNICAL MEMORANDUM NUMBER 16

DATE: May 1, 1991

TO: Vanessa Harris, Site Manager

CC: Marcia Kuehl - RI Lead
Roman Gau - Project Manager
Mike Crosser - TSQAM

FROM: Anya Kirykowicz

SUBJECT: EPA ARCS Region V Contract No. 68-W8-0093
EPA Work Assignment No. 17-5L4J
Donohue Project No. 20026.024
Himco Dump RI/FS

WATER LEVEL MEASUREMENTS

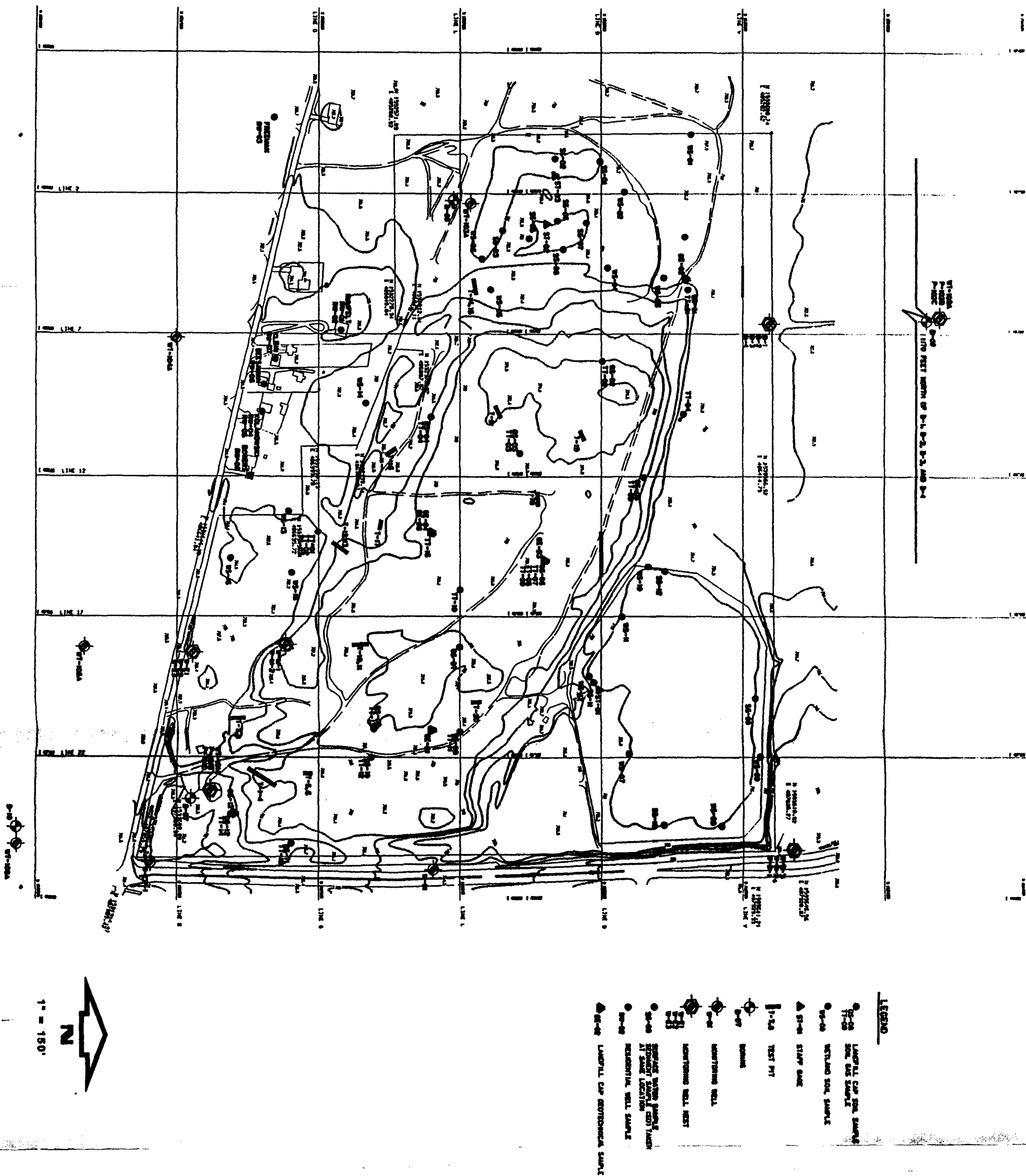
Introduction

Water level and well depth measurements were taken at the Himco Dump Site on November 6, 1990, February 1, 1991 and February 2, 1991. Static water levels were measured and recorded to determine groundwater flow directions and gradients at the site (water table elevations map). Water level and well depth measurements were also taken after installation of new wells, before and after well development and during scheduled groundwater sampling. Information concerning those measurements may be found in the respective technical memorandums. Water level and well depth measurements were conducted by Rob Cannestra, Anya Kirykowicz and Tracey Koach of Donohue & Associates, Inc. Well locations are shown in Figure 1.

Methods

Section 4.2.3.3 and Section 4.2.3.4 of the Final Field Sampling Plan, Himco Dump RI/FS, Elkhart, Indiana, described water level, well depth measurements and decontamination procedures. The water level surface was measured using poppers and electronic water level indicators. Each well had a reference point on top of the PVC well casing, from which water level measurements were taken. Measurements were noted to the nearest 0.01 feet. Each well was surveyed with respect to mean sea level elevation with an accuracy of 0.01 feet. Water level, well depth and staff gauge measurements were made within a 24-hour period.

The poppers and electric water level indicators were decontaminated between wells using an Alconox soap and tap water wash, tap water rinse, isopropanol rinse and two deionized or distilled water rinses. The isopropanol rinses were captured in a 5-gallon bucket and covered for discharge into the on-site frac tank.



MAY 1991

FIGURE 1 SITE LOCATION MAP (TECHNICAL MEMO)

HIMCO DUMP
SUPERFUND SITE
ELKHART, INDIANA

20026

Donohue ENGINEERS
ARCHITECTS
SCIENTISTS

APPENDIX A
WATER LEVEL MEASUREMENT AND ELEVATIONS

Deviations

Distilled water rinses were used during decontamination procedures in addition to deionized water.

Summary of Results

Water level measurement forms are attached in Appendix A.

AK:lh

A/R/HIMCO/AC0

DONOHUE

WATER ELEVATION

PROJECT NO. 20026

SITE HIMCO DUMP - INITIAL WELL INVENTORY

WELL NUMBER	ELEVATION OF TOP OF PIPE	DEPTH TO WATER	WATER ELEVATION	DEPTH TO BOTTOM	WELL INTEGRITY				COMMENTS
					LOCKED	CAPPED	CRACKED	OBSTRUCT	
E-1	77.11	15.15'		81.32	X	X			11/6/90 - 11/6/90 - 11/6/90
E-2		11.62'		17.93		X			11/6/90 - 11/6/90 - 11/6/90
E-3		12.99'		17.55	X	X			11/6/90 - 11/6/90 - 11/6/90
N-1		9.04'		22.85		X			11/6/90 - 11/6/90 - 11/6/90
B-4		7.55'		175.12	X	X			11/6/90 - 11/6/90 - 11/6/90
E-3		7.34'		130.23	X	X			11/6/90 - 11/6/90 - 11/6/90
B-2		7.04'		12.91'		X			11/6/90 - 11/6/90 - 11/6/90
B-1		7.33'			X	X			11/6/90 - 11/6/90 - 11/6/90
LP-1	UNABLE TO OPEN					X			11/6/90 - 11/6/90 - 11/6/90
M-1		7.12'		103.34'		X			11/6/90 - 11/6/90 - 11/6/90
M-2		10.35		7.68'		X			11/6/90 - 11/6/90 - 11/6/90
L-1		12.58		62.53	X	X			11/6/90 - 11/6/90 - 11/6/90
L-2		10.46		186.0	X	X			11/6/90 - 11/6/90 - 11/6/90
L-4		11.73		19.91		X			11/6/90 - 11/6/90 - 11/6/90
I-3		9.28		22.20	X	X			11/6/90 - 11/6/90 - 11/6/90
I-1		10.67		172.82	X	X			11/6/90 - 11/6/90 - 11/6/90
I-2		9.05		15.64	NO	X			11/6/90 - 11/6/90 - 11/6/90
Q-1		5.87		23.69	NO	X			11/6/90 - 11/6/90 - 11/6/90
Q-1		11.65		42.70	X	X	X		11/6/90 - 11/6/90 - 11/6/90
Q-3		22.18		153.62	X	X			11/6/90 - 11/6/90 - 11/6/90
Q-2		9.76		17.80	NO	X			11/6/90 - 11/6/90 - 11/6/90
F-2		17.06		147.85	X	X			11/6/90 - 11/6/90 - 11/6/90
F-3		20.34		180.23	X	X			11/6/90 - 11/6/90 - 11/6/90
F-1		9.05		31.25	NO	X			11/6/90 - 11/6/90 - 11/6/90
G-1		13.75		46.27	X	X			11/6/90 - 11/6/90 - 11/6/90
G-3		27.62		—	X	X			11/6/90 - 11/6/90 - 11/6/90
P-1		8.90		25.24	NO	NO			11/6/90 - 11/6/90 - 11/6/90
O-1		10.19		29.77	X	X			11/6/90 - 11/6/90 - 11/6/90

DESCRIPTION OF SITE

SOIL CONDITIONS

WEATHER

TEMPERATURE

ENTERED ON COMPUTER

SIGNATURE

DATE

DONOHUE

WATER ELEVATION

Feb. 1, 1991

PROJECT NO. 20026

SITE Himco Dump

WELL NUMBER	ELEVATION OF TOP OF PIPE	DEPTH TO WATER	WATER ELEVATION	DEPTH TO BOTTOM	WELL INTEGRITY				COMMENTS
					LOCKED	CAPPED	CRACKED	OBSTRUCT	
B-1		6.25			X	X			1052 No protective casing
B-2		6.15		13.88		X			1055
B-3		7.44		130.34	X	X			1059
B-4		6.45		175.16	X	X			1110
CP-1		3.82		20.19		X			1013 2/2/91 NO protective casing
E-2		9.82		16.54		X			1612
E-3		11.11		175.65	X	X			1614
F-1		7.67		31.28		X			1755
F-2		14.08		147.83	X	X			1438
F-3		16.98			X	X			1453
G-1		12.48		52.02	X	X			1413
G-3		22.08		169.89	X	X			1434
I-1		9.48		172.92	X	X			1540
I-2		8.78		15.67		X			1544
I-3		9.14		32.15	X	X			1872
J-1		12.03		42.64	X	X			1574
J-2		10.29		17.81		X	X		1524 2/2/91 SP2491
J-3		18.63		153.39	X	X			1520
M-1		15.61		103.24		X			10452 2/91
M-2		14.84		24.76		X			1050
N-1		8.81		29.22		X			0947 Flush
O-1		5.0		23.47		X			1820
O-1		8.34		29.77		X			1931
WT101A		9.96		18.70	X	X			1145
P101B		9.89		100.47	X	X			1152
P101C		9.78		106.53	X	X			1159
WT106A		2.87		18.50	X	X			1558
WT105A		9.0		18.56	X	X			1625
WT104A		8.02		18.69	X	X			1635
WT103A		5.28		18.47	X	X			1001 2/2/91
WT102A		10.17		18.18	X	X			0851 2/2/91

DESCRIPTION OF SITE

E 11.17 DTW = 11.38 NTR = 71.75

SOIL CONDITIONS

O-1: Flush w/ground water mē ten rever to side resing fill w/

WEATHER

hion. ice, water ran no snow on

TEMPERATURE

ENTERED ON COMPUTER

SIGNATURE

DATE

WATER ELEVATION

PROJECT NO. 10076

SITE

Hume Dump

[illegible]

DESCRIPTION OF SITE

SOIL CONDITIONS

WEATHER _____ TEMPERATURE _____

ENTERED ON COMPUTER _____ SIGNATURE _____ DATE _____

TECHNICAL MEMORANDUM - NO. 17

ORIGINAL

DATE: November 1, 1991

TO: Vanessa Harris, Site Manager

CC: Mansour Ghiasi, RI Lead
Roman Gau, Project Manager
Mike Crosser, TSQAM

FROM: Anya Kirykowicz

SUBJECT: EPA ARCS Region V Contract No. 68-W8-0093
EPA Work Assignment No. 17-5L4J
Himco Dump RI/FS
Donohue Project No. 20026.024

HEALTH AND SAFETY

Introduction

Donohue & Associates, Inc., conducted field work from October 1990 to January 1991 and from September 1991 to October 1991 at the Himco Dump Superfund site in accordance with the Final Field Sampling Plan, Himco Dump RI/FS, Elkhart, Indiana - 1990 and the Addendum I, Phase II Work Plan, Himco Dump Remedial Investigation/ Feasibility Study - August 1991, respectively. Personnel entering the site followed the protocols established in the Health and Safety Plan, Himco Dump Remedial Investigation/Feasibility Study, Elkhart, Indiana, Final July 1990 (HASP, 1990) and the Final Addendum I Health and Safety Plan, Himco Dump Remedial Investigation/Feasibility Study, Phase II, Elkhart, Indiana - August 1991 (Addendum I, 1991).

Methods

As outlined in Section 1.0 of the HASP, 1990, the plan was prepared in accordance with the ARCS V Program Health and Safety Guideline HAS-1 and the regulatory requirement of 29 CFR 1910.120, "Hazardous Waste Operations and Emergency Response." The HASP, 1990 was implemented during Phase I activities. The following tasks were completed during Phase I: sediment and surface water sampling, trenching, soil boring/monitoring well installation, soil sampling, staff gauge installation, waste mass gas sampling, wetland identification, monitoring well development, slug tests, groundwater sampling, survey, and geophysical survey.

During Phase II activities, the HASP, 1990 and Addendum I, 1991 were implemented. Tasks completed during Phase II were: trenching, soil boring/monitoring well installation, wetland delineation, soil sampling, groundwater sampling, leachate sampling, sediment and surface water sampling. Addendum I, 1991 addresses safe boating practices for the collection of sediment and surface water samples.

Deviations

There were no deviations from the HASP, 1990 and the Addendum I, 1991, except for reassignment of staff listed in the project organization.

Summary Results

The HASP, 1990 and Addendum I, 1991 were adhered to by staff from the following: Donohue and Associates, Inc.; John Mathes & Associates; Life Systems, Inc.; Lang, Feeney & Associates, Inc.; Engineering-Science, Inc.; STS Consultants, Ltd.; United States Environmental Protection Agency; and the Indiana Department of Environmental Management.

A/R/HIMCO/AH7